

Fission product yield evaluation

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Abstract

A new evaluation has been made of the independent and cumulative yields of fission products for a selection of fissioning systems, including fission of nuclides important for reactor design and operation, and for fuel and waste management. The evaluation, which has been given the reference name UKFY3, used a new database of measurements and is considered complete up to early 1993. This database considerably extends and updates the database used for the previous UKFY2 evaluation.

The measurement database was analysed to produce a “best estimate” set of fission product yields. Careful study has been made of experimental uncertainties and discrepancies in the data. As some discrepancies could not be resolved the normalised residual technique was used to down-weight discrepant values. Relative and ratio-of-ratio measurements were included in the analysis by an iterative procedure. The measured data, results of the analysis and discrepancies in the data are shown in extensive tables included as appendices to this thesis.

The “best estimates” of fission product yields generated by the analysis were then studied to improve the understanding of the systematics of the yield distribution in mass, charge and isomeric state. Models describing these distributions were investigated and fitted. The effects of the fissioning nucleus mass and charge were examined, as well as the effect of neutron energy on the distributions from neutron-induced fission.

The results of these studies were then combined with the “best estimates” to generate complete independent and cumulative yields sets for a list of fissioning systems considered important for applications. This set consists of the neutron-induced fission of ^{232}Th , $^{233,234,235,236,238}\text{U}$, $^{237,238}\text{Np}$, $^{238,239,240,241,242}\text{Pu}$, $^{241,242\text{m},243}\text{Am}$, and $^{243,244,245}\text{Cm}$, plus the spontaneous fission of $^{242,244}\text{Cm}$ and ^{252}Cf . These complete yield sets were subsequently adjusted to fit the physical constraints of the fissioning process. The new adjusted library produced by the analysis of the UKFY3 database, provisionally called UKFY3.0 has been produced as a computer file in the ENDF-6 format.

The new UKFY3.0 file and the UKFY2 file, which has been revised for use in JEF2.2 during this work, were then tested against integral experimental results for delayed neutron and decay heat production respectively.

Finally, results of this work are summarized, remaining problems discussed and areas for future work highlighted.

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1. Introduction

1.1 Requirement for fission product yield data

In this first chapter I shall address the importance of fission products and their quantification. It is also necessary to describe the nomenclature used in the study of fission product yields and their evaluation.

The main need for fission product yield data comes from any type of modelling associated with situations where actinides are being, or have been, fissioned. The primary uses of these data are within the nuclear industry for nuclear reactor and fuel cycle calculations, although these data can be used in the study of naturally occurring geological formations such as the Oklo “natural” reactors^[1.1]. At Oklo, many millions of years ago, the uranium rich rock was shattered by earthquakes. This allowed water to percolate through the rock which formed regions where self-sustaining fission reactions were started. These reactions later ceased when the ^{235}U content of the rock was depleted by the nuclear reactions.

In the nuclear industry fission product yields are used in many different reactor and spent fuel calculations, including those on decay heat, shielding, dosimetry, burn-up, fuel handling, waste disposal and safety. In such calculations the fission product yields that are significant to the individual task are required. The number may vary from a single yield for a destructive burnup assay to around a thousand yields for decay heat calculations. If more than one fissioning system is present then the yields will be required for each of these. The number of yields needed to be considered will therefore depend upon the task and its desired level of modelling accuracy.

All such fission product calculations are ultimately calculations of nuclide inventory. These inventories are usually calculated by starting with the initial inventory of the fuel, typically the uranium content and its isotopic abundances, along with any impurities (e.g. lithium, nitrogen etc.) and other nuclei present (e.g. oxygen in uranium dioxide fuels). Changes to the initial inventory are then modelled during periods of neutron irradiation or

[1.1] Nuclear Engineering International, February 1994, p30 “Gabon’s natural reactors”, B.Nagy (1993).

cooling. The inventory changes are governed by differential equations which include terms for both destruction and production of each nuclide. The destruction terms are the decay of the nuclide, and neutron reactions which transmute the nuclide (e.g. capture, fission, (n,p) , (n,α) , $(n,2n)$ etc.). The production terms are decay of direct precursors to the nuclide, the independent fission product yields produced by fission of actinides and the neutron transmutation of other nuclides into this nuclide. Obviously the differential equation governing the change of any one nuclide is linked to those describing changes in all of its precursors. Thus the solution of these equations, without making simplifying assumptions, is not trivial and is usually carried out on computers using numerical solution techniques. The inventories calculated can then be processed using half-lives, branching fractions and average decay energies to calculate the heat output of the irradiated fuel. Similarly the total emission and spectra of α , β , γ and neutron emissions can be calculated using half-lives, branching fractions, (α,n) cross-sections and the characteristic particle spectra of each nuclide present.

Such calculations can describe the chemistry, heating and radiative emission of the fuel as functions of time. These parameters have many uses for the storage and transport of spent fuel, and for chemical or mechanical processing of the fuel. The heat output of the fuel or separated components can be used to calculate the cooling that must be applied to safely store the material. If fuel is stored at too high a temperature the thermal stress may damage the cladding and release volatile fission products. Also at high temperature some fission product compounds and fuel components such as magnesium alloys may combust in air. A tragic example of this occurred at TOMSK-7 in the Soviet Union where concentrated fission product waste was stored as nitrates in solution. The fission product decay heat dried up the solution; the residue was chemically unstable and exploded releasing radio-nuclides into the atmosphere.

The calculated emission and spectra of various radiations are used as source terms in calculations to determine the shielding necessary around fuel while it is either being transported or processed so that workers and members of the public are not exposed to radiation doses above internationally agreed limits.

The fuel chemistry and its variation with time are important in determining the paths that

radio-nuclides will take in chemical processing. Also, when radio-nuclides are released into the environment by accidents, like Chernobyl, their chemical behaviour will determine their spread within the ecosystem and their uptake into plants and animals. The effect of release of radio-nuclides into the environment are determined by both their uptake by and excretion by organisms, and the radiation dose to the organism whilst present. An interesting example of this is the cycling of caesium in mountainous pastures and in the arctic tundra. The mosses which grow in these places require trace elements which are in short supply in the soil of these areas. The radio-caesium is chemically similar to the required trace elements and is thus strongly absorbed by the moss. When the moss is eaten the caesium either enters the animal or is excreted and re-absorbed by the moss. Thus the moss fixes the caesium into the environment stopping rain from washing the contamination away.

Calculations of radio-nuclide uptake are used to estimate the radiation dose to the population from both accidents and, also the processing and disposal of nuclear waste. As well as doses to the general population specific groups at greater risk of exposure are studied in detail. An example of this are those who survive on a diet of shellfish picked from the seashore near nuclear installations. Shellfish feed on the small particles of food caught from tidal currents and thus easily absorb many radio-nuclides.

Apart from the safety related calculations described above the nuclide inventories can be used in metrology of spent fuel. The percentage burnup of heavy atoms in the fuel and the cooling time since the irradiation are important parameters for fuel handling which can be determined by examining the fission product inventories. The burnup of fuel can be estimated using the stable nuclide ^{148}Nd which is determined by destructive assay. The precursors of ^{148}Nd are all short lived and have small cross-sections and thus the cumulative yield can be used to determine the number of fissions that has taken place in the fuel. In this technique a further simplification applies as the cumulative yields of ^{148}Nd for both thermal and fast fission of ^{235}U and ^{239}Pu are very similar. Thus, as these are the major isotopes undergoing fission in thermal reactor fuel, it is possible to determine the number of fissions, and thus the loss of heavy elements. This can be calculated simply by dividing the number of the stable ^{148}Nd nuclei present by the

cumulative fission yield of 1.68 ± 0.01 per one hundred fissions.

Another method of determining fuel burnup is non-destructive gamma-ray spectrometry. The simplest method involves measuring the ratio of ^{134}Cs to ^{137}Cs which is directly proportional to the burnup. However this method is highly dependent on the initial ^{235}U enrichment of the fuel and on the reactor rating. An improved technique uses the Fox ratio^[1.2]. The activities of ^{106}Ru , ^{137}Cs and ^{134}Cs within the fuel are measured by gamma-ray spectrometry, the Fox ratio is defined by the following expression;

$$^{106}\text{Ru} \times ^{137}\text{Cs} / (^{134}\text{Cs})^2 \quad \text{Eqn (1.1)}$$

where the terms refer to the activity of the nuclides. This ratio is directly proportional to the burnup of the fuel, but has little dependence on the initial ^{235}U enrichment of the fuel or on the reactor rating. However, the short half-life of ^{106}Ru (1.0228 ± 0.0004 years) restricts the use of this ratio to fuel cooled for less than seven years.

Similarly, the cooling time of the fuel can be determined by examining activity ratios such as $^{106}\text{Ru}/^{137}\text{Cs}$ and $^{134}\text{Cs}/^{154}\text{Eu}$. These ratios have characteristic values with cooling time and thus by measuring the ratios the cooling time can be estimated. The short lived ^{140}La (half-life of 1.6781 ± 0.0003 days), with no long lived precursors, can similarly be used to detect fuel that has been cooled for very short times. This is used in reprocessing plants to avoid dissolving short-cooled fuel rods whose radio-iodine content could dramatically increase the radiation dose to workers. In reactor experiments the short-lived ^{140}La can also be used to determine the fission rate in a sample as this nuclide quickly forms an equilibrium number density dependent on the fission rate and the decay constant.

In most applications the fission product radiation makes the handling of fuel more difficult. However many fission products are neutron absorbers and thus their presence reduces the neutron multiplication in transport flasks and cooling ponds. This reduces

[1.2] The fourth International conference on nuclear fuel reprocessing and waste management RECOD94, 24-28th April 1994, London, UK. "Special Instrumentation development at Sellafield" by G.H.Fox, N.Gardner and C.H.Zimmerman.

the risk of criticality accidents. Including the fission products in calculations of neutron multiplication, provided the calculations can be experimentally validated, will allow more fuel to be packed in shipping flasks and cooling ponds. This would reduce the cost of transporting and storing spent nuclear fuel. However, in the UK, it is currently not permitted to take credit for fuel burnup in criticality calculations. However, in Germany, if the burnup of the fuel is confirmed by measurement some credit can be taken for the stable and very long-lived fission products.

All the calculations above are dependent on the nuclear data used. To estimate these data most accurately all available experimental measurements must be taken into account. However, for fission product yields, even the most measured fissioning system, thermal neutron-induced fission of ^{235}U , does not have experimental data for all significant yields. It is thus necessary to generate values using empirical or theoretical models for those yields for which measured data are unavailable.

1.2 The history of UK and international evaluations of fission product yields

The evaluation of yields for computer libraries in the UK was pioneered by E.A.C. Crouch at Harwell^[1.3] during the 1960's and 70's. This work led to the production of computer libraries called Crouch 1, 2 and 3. After his retirement in 1981 the work was continued by M.F.James and J.Banai at Winfrith. This led to the production of an interim library, largely based on the Crouch experimental measurement database and was thus known as Crouch4 (as Crouch had previously produced three files); this was then followed by an improved file which was called UKFY1. The UKFY1 file was adopted by the Nuclear Energy Agency in 1986 for the fission product yield sections of the first version of an evaluated nuclear data file called the Joint Evaluated File, or JEF.

M.F.James and this author then produced a new evaluation called UKFY2. This work was funded jointly by British Nuclear Fuels plc, the Central Electricity Generating Board and the United Kingdom Atomic Energy Authority. The resulting file was adopted for inclusion in the preliminary release of the second Joint Evaluated File (JEF-2.1). Following this

[1.3] E.A.C. Crouch, Atomic and Nuclear Data Tables, 19, 417 (1977) and earlier references therein.

work, in June 1990, I began a studentship sponsored by BNF plc. At the beginning of this period the UKFY2 work was completed and written up as three United Kingdom Atomic Energy Authority reports^{[1.4][1.5][1.6]}. Comments from the UK Chemical Nuclear Data Committee and the JEF committees high-lighted two areas for further study. Firstly, for UKFY2 mass yields were approximated by chain yield. This approximation ignores neutron emission and thus would lead to incorrect calculation of nuclide inventories. Secondly the UKFY2 file had yields for nuclides that were not stable or included in the JEF decay data. This will lead to loss of these yields in calculations. Thus a revised processing technique was used to correct for these problems. Ultimately in 1993 the final JEF2.2 decay data became available and this was used to create a new version of UKFY2 which was submitted to the Nuclear Energy Agency Databank's JEF project in July 1993 and this became part of the JEF2.2 file release later that year. The work reported in this thesis is a continuation of the original UKFY2 work, although carried out in parallel with the final modifications to UKFY2, but leading to a new evaluation UKFY3.

Internationally there exist several other evaluation efforts each generating their own files. These are in China (CENDL, Chinese Evaluated Nuclear Data Library), Japan (JENDL, Japanese Evaluated Nuclear Data Library), Russia (BROND) and the United States of America (ENDF, Evaluated Nuclear Data File). These separate projects have developed in parallel with the work of the UK and there have been detailed communication between the evaluators and intercomparisons of the different datasets over the decades, especially between the U.K. and U.S.A. In the past other groups in France and Austria have also produced evaluations. However only the UK and US evaluations have developed evaluated files completely independently of the other evaluations. In addition

[1.4] Report AEA-TRS-1015 "A new evaluation of fission product yields and the production of a new library (UKFY2) of independent and cumulative yields. Part I. Methods and outline of the evaluation" by M.F. James, R.W. Mills and D.R.Weaver (1991).

[1.5] Report AEA-TRS-1018 "A new evaluation of fission product yields and the production of a new library (UKFY2) of independent and cumulative yields. Part II. Tables of measured and recommended fission yield" by M.F. James, R.W. Mills and D.R.Weaver (1991).

[1.6] Report AEA-TRS-1019 "A new evaluation of fission product yields and the production of a new library (UKFY2) of independent and cumulative yields. Part III. Tables of fission yields with discrepant or sparse data" by M.F. James, R.W. Mills and D.R.Weaver (1991)

to the communication between the evaluators contact has also been maintained with the measurers of fission yield data.

1.3 Brief overview of the physical processes relating to the formation and properties of fission products

The process of fission, the splitting of a heavy nucleus into two or more light nuclei, was first suggested by Meitner and Frisch in 1938 who drew conclusions from the work of Curie and Savitch, and Hahn and Strassmann who had observed barium as a product of the neutron bombardment of uranium^[1.7].

It is energetically possible for actinides to split into two lighter fragments and release a relatively large amount of energy, around 200 MeV per fission; however it is first necessary for the nucleus to overcome a potential energy barrier called the fission barrier. This can occur in several ways. Energy to overcome the barrier can come from either transferring sufficient energy to the nucleus from outside, or the internal release of energy due to rearrangement of the nucleus after the absorption of a particle, or even through both of these two effects combined. A third process involves quantum mechanical tunnelling through the barrier, this occurs for both spontaneous and sub-threshold fission.

Once the barrier is overcome the fission process proceeds very rapidly. The nucleus splits into two fragments which are rapidly accelerated apart by Coulomb repulsion. As the fragments are accelerated prompt neutrons are emitted. Around 10^{-14} seconds after passing the fission barrier prompt gamma rays are emitted as the fragments de-excite. After 10^{-10} seconds the fragments are left in states that begin to undergo gamma cascade to longer-lived states which then decay by gamma or particle emission.

Because the precursor actinide has a high neutron to proton ratio, from its position on the line of stability, the main fission products are neutron rich nuclides. These products mostly undergo beta decay towards the line of stability. A small percentage of these beta decaying nuclides leave their daughter nuclei with sufficient energy to throw off a neutron

[1.7] "Elements of Nuclear Physics", W.E. Burcham first published by Longman in 1979, reprinted 1985. ISBN 0-582-46027-1

before emitting a gamma cascade. As this neutron emission occurs at the same time as the radioactive decay of the fission products which itself is delayed from the fission event this process is called delayed neutron emission. The delayed component of neutron production when averaged per fission is of the order of one percent of the prompt neutron production. Although this is a small component of the total the existence of this delayed fraction allows the design of reactors that reach criticality only because of delayed neutrons and which can thus be safely controlled with feedback controllers with characteristic cycle times of the order of tens of seconds rather than milliseconds.

At this point it is interesting to note that the half-lives of fission products range from fractions of a millisecond to many millions of years. However the longest lived fission product which emits delayed neutrons in its decay is Rb-91 with a reported half-life of 58.4 ± 0.4 seconds reported in the JEF2.2 decay data file^[1.8]. This leads to the interesting observation that delayed neutron emission is dominated by short lived products, most of which are at the neutron rich extremes of the fission product yield distribution.

1.4 Definitions relevant to fission product yields

The nomenclature for fission products yields used in this thesis is that described by James et al^[1.4], a report which was produced as part of the work associated with this thesis.

The atomic number and mass number of the fissioning compound nucleus are denoted by Z_f and A_f respectively. For the neutron-induced fission of a nuclide of mass number A_{target} , $A_f = A_{\text{target}} + 1$, while for spontaneous fission, A_f is the mass number of the fissioning nuclide.

A fission product nuclide is specified symbolically by the triplet (A,Z,I), where A and Z are respectively the mass number and atomic number, and I indicates the isomeric state (I=0

[1.8] JEF2.2 radioactive decay data file maintained and distributed from the NEA Data-bank, Le Seine St-Germain, 12 boulevard des îles, 92130 Issy-les-Moulineaux, Paris, France.

for the ground state, $l=1,2,\dots$ for the 1st, 2nd,... excited states). If a fission product has no isomers, or if we are referring to the sum of yields for all its isomers, we use the doublet (A,Z) .

The **independent yield** $y(A,Z,l)$ is the number of atoms of (A,Z,l) produced directly from one fission, but after the emission of prompt neutrons (but before any radioactive decay and hence the emission of delayed neutrons). It can be written as the product of 3 factors:

$$y(A, Z, l) = Y(A) \times f(A, Z) \times R(A, Z, l) \quad \text{Eqn (1.2)}$$

where the **sum yield** or **mass yield** $Y(A)$ is the total of the independent yields (before delayed neutron emission) of all fission products of mass number A ; $f(A,Z)$ is the **fractional independent yield** of all isomers of (A,Z) ; and $R(A,Z,l)$, the **isomeric yield ratio**, is the fraction of (A,Z) produced directly as isomer l .

From the definition Eqn (1.2), it follows that:

$$\sum_Z f(A, Z) = 1 \quad \text{for all } A \quad \text{Eqn (1.3)}$$

and

$$\sum_l R(A, Z, l) = 1 \quad \text{for all } (A,Z) \quad \text{Eqn (1.4)}$$

so that:

$$Y(A) = \sum_{Z,l} y(A, Z, l) \quad \text{for all } A \quad \text{Eqn (1.5)}$$

The usefulness of these formulae derives from the fact that, with the exception of delayed neutron (β^- , n) emission and the few very long-lived alpha decays, all the radioactive decays of fission products are β^- or β^+ , or isomeric transitions, and in none of these is the mass number A altered. Thus, to a very good approximation, the fission products can

be considered as belonging to distinct decay chains of constant mass.

In a similar way to the sum yield it is possible to define a **charge yield** $g(Z)$ such that:

$$g(Z) = \sum_{A, I} y(A, Z, I) \quad \text{for all } Z \quad \text{Eqn (1.6)}$$

This has only become useful since mass separators such as LOHENGRIN^[1.9] have allowed the rapid determination of the number of fission fragments with a given charge before beta decay can occur. It should be noted that the mass separators measure the yield of a specific mass, ionic charge and energy. To produce fission product yields requires many summations and normalizations of different experimental runs and thus care must be taken in using these data to ensure the yields are representative of typical fission events and not subsets for specific parameters.

The **cumulative yield** $c(A, Z, I)$ of nuclide (A, Z, I) is the total number of atoms of that nuclide produced over all time after one fission. If the nuclide is stable the cumulative yield is the total number of atoms of that nuclide remaining per fission after all precursor decays (ignoring the effects of other nuclear reactions e.g. neutron capture). Similarly, for a nuclide with a much longer half-life than any of its precursors, $c(A, Z, I)$ is very nearly equal to the amount of it produced at a time short compared to its half-life but long compared to those of its precursors. However, for a radioactive nuclide for which this is not the case, some atoms will have decayed before all have been produced, so that at no time will there actually be $c(A, Z, I)$ atoms per fission present. The **chain yield** $Ch(A)$ is equal to the sum of all stable or long-lived cumulative yields for a given mass chain.

An equivalent definition that is more useful is the following: immediately at the end of an “infinite” irradiation at the rate of 1 fission per second, $c(A, Z, I)$ is the rate of decay of (A, Z, I) if that nuclide is radioactive, or its rate of production if it is stable. In the case of a

[1.9] “Mass and nuclear charge yields for $^{237}\text{Np}(2n\text{-th}, f)$ at different fission fragment kinetic energies”, G.Martinez, G.Barreau, A.Sicre, T.P.Doan, P.Audouard, B.Leroux, W.Arafa, R.Brisot, J.P.Bocquet, H.Faust, P.Koczon, M.Mutterer, F.Gonnenwein, M.Asghar, U.Quade, K.Rudolph, D.Engelhardt and E.Piasecki, Nucl. Phys.A, 515, 433 (1990).

radioactive product an equilibrium concentration is formed by such an “infinite” irradiation and thus the production is equal to the decay. As a consequence of this property cumulative yields are useful in computing parameters summed over all time such as total fission product decay energies and delayed neutron emission probabilities.

It should be noted that the chain yield, $Ch(A)$, and the sum or mass yield, $Y(A)$, for a mass chain A may differ by a few per cent because the former applies after, and the latter before, delayed neutron emission.

In practical measurements the number density of a particular (A,Z,I) present or the number of decays of that nuclide will be determined at some time after fission. Thus to determine the independent, cumulative or chain yields it is necessary to correct for the decay into and out of the measured nuclide if any has occurred. The timing of an experiment will thus determine the yields and type of yield that can be measured. To measure the independent yields of short lived nuclides or those which are quickly swamped by precursors it is necessary to make rapid measurements or to be able to correct accurately for the decays.

Fissions can generate two or more fragments, ignoring for the moment the neutrons emitted. If only two fragments are produced then the fission is referred to as a **binary** fission. If three fragments it is termed **ternary** fission. The third, and possibly fourth, fragments are always light compared to the other two. The most common light fragment is a helium nucleus, followed by a triton. Measurements have been made down to extremely low yields, below 1 in 10^{10} , of nuclides up to a mass of 39 a.m.u. These light fragments are sometimes called **light charged particle** emissions.

1.5 Summary of contents

The concern of this work is four fold. Firstly, to extend and improve the experimental database used in the UKFY2 evaluation. Secondly, to study various aspects of fission product yield distributions using a new and expanded database of fission product yield measurements. Thirdly, to generate a new and complete yield dataset, UKFY3.0, using this set of experimental data together with models from the literature or developed during this work. Fourthly, to compare calculational results for decay heat and delayed neutron

emission derived from fission product yields and decay data using this new dataset and to compare these results with the other evaluations available.

To generate a complete dataset it is necessary to model the mass, fractional independent and the light charged particle yields, plus the isomeric splitting ratios. It is also necessary to consider how these distributions and the model parameters vary with incident neutron energy based upon the experimental data and to provide an appropriate way to describe these variations.

The experimental data must be analyzed to produce a set of “best estimates” of the yields from the measurements. The measurements will all have their own uncertainties and some may be inconsistent.

Earlier work^[1.4] has shown that the chain yield distributions can be modelled effectively by sums of gaussians, fractional independent yields by the A_p and Z_p models developed by A.C.Wahl^[1.10], isomeric splitting by the Madland and England model^[1.11], and light charged particles by various empirical relationships between yields and compound nucleus mass and charge.

This whole process of collating the measurements, analyzing these published results to determine the “best estimate” recommendations, testing published models and also novel ideas against the analyzed data to determine the “best” models, and then generating a final physically consistent dataset for use in subsequent calculations is referred to by the nuclear data community as “evaluation”.

[1.10] “Nuclear-charge distribution and delayed-neutron yields for thermal-neutron fission of ^{235}U , ^{233}U and ^{239}Pu and for the spontaneous fission of ^{252}Cf ”, A.C.Wahl, Atomic and Nuclear Data Tables 39, 1-156 (1988).

[1.11] “The influence of Isomeric states on independent fission product yields”, D.G.Madland and T.R.England, Nucl. Sci. Eng. 64, 859 (1977).

2. Experimental Database

2.1 Introduction

The purpose of Fission Product Yield Evaluation is to generate a set of data that can be used to estimate, together with other nuclear data such as cross-sections and half-lives, the fission product nuclide inventories following fission. These inventories can then be used with decay data to calculate integral properties such as decay heat and radiation emission for applications like transport, reprocessing and waste management.

All evaluations are dependent upon the experimentally measured data and that must be any evaluation's starting point, and its sole factual foundation. To go beyond these experimental data is to rely upon empirical or theoretical models to interpolate or extrapolate the data. Thus the experimental database must contain all relevant measurements over as wide a range of experimental parameters as possible. The literature must be searched for every obtainable item of data or constraint upon data. These data should then be summarized in a standard format to facilitate analysis of the data.

In the collection of fission yield data there are three important considerations. Firstly, the large number of possible fissioning systems (i.e. target nuclide, the cause of fissioning - whether by an incident particle of certain energy and type, or spontaneously). Secondly the large number of fission products produced during fission (around a thousand). And finally, the many thousands of reported measurements.

The many parameters of each measurement and large number of measurements direct the evaluator towards computer storage and analysis of the data.

2.2 Database Format

2.2.1 Initial comments

The format must store all the relevant information that can be obtained from the reference. The database must include for each measurement the nuclide fissioning (the "target nucleus"), the incident particle causing fission together with its energy or a note that fission is spontaneous, the product, the yield type, the yield and its uncertainty, and

an identifier for the original reference.

2.2.2 Measurement methods

It should be noted that fission yield measurements can be made by three basic methods.

In the first, the nuclide production and the number of fissions are determined which allows the yield (probability of producing the nuclide per fission) to be determined directly. This is often referred to as an **absolute measurement**.

In the second the yield of the nuclide of interest can be measured relative to that of a “standard” nuclide; this gives rise to the ratio of the nuclide’s yield to the “standard” yield. This technique is referred to as a **relative measurement**. It should be noted that this does not require the determination of the number of fissions but does require a procedure to measure the “standard” and “unknown” nuclides’ number densities present in the irradiated sample.

The third method is the “ratio of ratio” technique; here neither the number of fissions nor the nuclides’ number densities need to be determined. The ratio of activities or, more commonly, the ratio of specific fission product decay gammas for the “standard” and the “unknown” nuclides are determined in two different irradiations. These irradiations can, for example, be for different neutron energies (e.g. thermal and fast) or be for differing sample materials (e.g. thermal fission of ^{235}U and ^{239}Pu). This **“ratio of ratio” measurement** or R-value shows the ratio between the two different ratio measurements.

The properties of ratio of ratio measurements are best illustrated by an simplified example.

First consider the general case of rate of change of the number density of a nuclide, i , in a sample being irradiated with a neutron flux ϕ . There are five routes of destruction and production of the nuclide i ; the decay of the nuclide, the destruction of the nuclide by neutron reactions, the production of the nuclide by decay of precursors, the production by neutron reactions on other nuclides present and the production from fission of fissile materials present.

This can be written as a differential equation, for example from Burstall^[2.1],

$$\frac{dN_i}{dt} = -N_i(\lambda_i + \sigma_i\phi) + \sum_j N_j(\lambda_{ij} + \sigma_{ij}\phi) + \sum_k N_k\sigma_k^f\phi Y_k^i \quad \text{Eqn (2.1)}$$

where N_x is the number density of x , λ_x is decay constant of x , λ_{xy} is the decay constant of decay of y producing x , σ_x is the sum of cross-sections destroying x , σ_{xy} is the cross-section of the reaction on y leading to the production of x , σ_k^f is the fission cross-section of k and Y_x^k is the independent fission yield of x from the fission of nuclide k .

If we consider a nuclide i whose half-life is very much longer than the time-scale of any measurement and whose destruction cross-sections are very small then Eqn (2.1) approximates to:

$$\frac{dN_i}{dt} \approx \sum_j N_j(\lambda_{ij} + \sigma_{ij}\phi) + \sum_k N_k\sigma_k^f\phi Y_i^k \quad \text{Eqn (2.2)}$$

Also if we assume that nuclide i is produced only by fission reactions then:

$$\frac{dN_i}{dt} \approx \sum_j N_j\lambda_{ij} + \sum_k N_k\sigma_k^f\phi Y_i^k \quad \text{Eqn (2.3)}$$

Now if the precursors of i , j , and all the precursors of j decay to i very rapidly then Eqn (2.1) will contain no component for the precursor decay and thus if the destruction cross-sections of the precursors are negligible it simplifies to:

$$\frac{dN_i}{dt} \approx \sum_k N_k\sigma_k^f\phi c_i^k \quad \text{Eqn (2.4)}$$

[2.1] Report ND-R-328(R) "FISPIN- A computer code for nuclide inventory calculations", R.F.Burstall (1979).

where c is the cumulative yield as defined in chapter 1. Thus after an irradiation of a duration of $\Delta t_{\text{irradiation}}$, assuming none of i (or precursors) present before the irradiation and that negligible change occurs in the fissile nuclides number densities during the irradiation, then;

$$N_i \approx \sum_k N_k \sigma_k^f \phi c_k^i \Delta t_{\text{irradiation}} \quad \text{Eqn (2.5)}$$

Now if the above approximations apply for both samples and products in a ratio of ratio measurement, and also if each sample contains only one fissile nuclide then the number densities of the products are given by:

$$\begin{aligned} N_x^1 &\approx N_1 \sigma_1^f \phi_1 c_1^x \Delta t_{\text{irradiation1}} \\ N_s^1 &\approx N_1 \sigma_1^f \phi_1 c_1^s \Delta t_{\text{irradiation1}} \\ N_x^2 &\approx N_2 \sigma_2^f \phi_2 c_2^x \Delta t_{\text{irradiation2}} \\ N_s^2 &\approx N_2 \sigma_2^f \phi_2 c_2^s \Delta t_{\text{irradiation2}} \end{aligned} \quad \text{Eqn (2.6)}$$

Thus the activities per unit volume are:

$$\begin{aligned} A_x^1 &\approx \lambda_x N_1 \sigma_1^f \phi_1 c_1^x \Delta t_{\text{irradiation1}} \\ A_s^1 &\approx \lambda_s N_1 \sigma_1^f \phi_1 c_1^s \Delta t_{\text{irradiation1}} \\ A_x^2 &\approx \lambda_x N_2 \sigma_2^f \phi_2 c_2^x \Delta t_{\text{irradiation2}} \\ A_s^2 &\approx \lambda_s N_2 \sigma_2^f \phi_2 c_2^s \Delta t_{\text{irradiation2}} \end{aligned} \quad \text{Eqn (2.7)}$$

Now from the definition of R-value:

$$R = \frac{N_x^1}{N_s^1} / \frac{N_x^2}{N_s^2} \quad \text{Eqn (2.8)}$$

Thus:

$$R = \frac{N_1 \sigma_1^f \phi c_1^x \Delta t_{\text{irradiation1}}}{N_1 \sigma_1^f \phi c_1^s \Delta t_{\text{irradiation1}}} / \frac{N_2 \sigma_2^f \phi c_2^x \Delta t_{\text{irradiation2}}}{N_2 \sigma_2^f \phi c_2^s \Delta t_{\text{irradiation2}}} \quad \text{Eqn (2.9)}$$

This simplifies to:

$$R = \frac{c_1^x}{c_1^s} / \frac{c_2^x}{c_2^s} = \frac{c_1^x c_2^s}{c_2^x c_1^s} \quad \text{Eqn (2.10)}$$

From this it can be seen that if the approximations are valid then the R-value is independent of the irradiation conditions, the number of fissions and the number density of the sample, and thus solely dependent upon the fission yields. However if cross-section effects or decay data parameters significantly effect the results then the experimental analysis must involve the solution of the differential equation in Eqn (2.1).

As described above the R-value is usually determined from the activities, or gamma spectrometry of the samples. In this case a different simplification becomes important. As given above the activity per volume is determined by the number density and the decay constant. Also for gamma spectrometry the P_γ , the probability of emitting a gamma of a specific energy is involved, since from Eqn (2.8)

$$R = \frac{\lambda_x P_{\gamma, x} N_x^1}{\lambda_s P_{\gamma, s} N_s^1} \times \frac{\lambda_s P_{\gamma, s} N_s^2}{\lambda_x P_{\gamma, x} N_x^2} = \frac{A_{\gamma, x}^1}{A_{\gamma, s}^1} \times \frac{A_{\gamma, s}^2}{A_{\gamma, x}^2}, \quad \text{Eqn (2.11)}$$

where $A_{\gamma, x}^i$ is the gamma activity for a specific energy, of nuclide x after irradiation i.

Now consider the situation when the same measurements are made on the two samples with the same detector in the same geometry and that the self-absorption of the two samples is the same (i.e. the separated fission product is in the same chemical form and of the same thickness). Then, the ratio of the number densities, of the same nuclide in both samples, is directly related to the ratio of counts in the detector, C, thus Eqn (2.8) becomes:

$$R = \frac{C_x^1}{C_s^1} / \frac{C_x^2}{C_s^2} = \frac{C_s^2 C_x^1}{C_x^2 C_s^1} \quad \text{Eqn (2.12)}$$

Of data from these three measurement types the absolute values can be used directly; however the relationships in the other two measurements (relative and ratio of ratio) allow calculation of absolute yields if values for the one standard in relative measurements and the three standards in ratio of ratio measurements are available.

2.2.3 Database details

The fission yield databases for both UKFY2 and UKFY3 used four files; these contained the absolute data in a file called FYDB, the relative data in RFYDB, the ratio of ratio data in RVALFYDB and the references with comments in FYREFDB. For UKFY3 the format was extended to allow the inclusion of charged particle and photon induced fission reactions and the new yield type of “charge yield”, but this did not require change in any of the pre-existing UKFY2 database entries. Both the UKFY2 and UKFY3 databases have been released for distribution through the NEA Data Bank in Paris.

The format common to both UKFY2 and UKFY3 files is described below.

For the **FYDB** files the data format can be described by the FORTRAN77 specifier as: (a1,1x,e9.3,4i3,a1,a1),(1x,e9.3,1x,e9.3,i5,a1).

An example of this is:

```
B 0.000E+00 92235 88 35 M 0.342E+00 0.800E+01 920
B 0.000E+00 92235 88 35 N 0.111E+01 0.117E+0222003
B 0.000E+00 92235 88 35 U 0.192E+01 0.521E+0121743N
```

The record is split into two parts: the yield identifier and the yield data sections.

The yield identifier consists of the particle inducing fission and its energy (or spontaneous fission), the “target” nuclide, the fission product and its yield type. The first character and the first floating point number gives the fission inducing particle and energy as shown in Table 2.1 below.

Table 2.1: Fission inducing particle and its energy

Incident particle	Energy	First character	Value of first number
neutron	thermal spectrum	B	0.0
“	fast or fission spectrum	F	0.0
“	Epi-thermal	E	0.0
“	High Energy (~14MeV)	H	0.0
“	monoenergetic or average	S	Energy in eV
none	Spontaneous Fission	I	0.0
Gamma	monoenergetic or average	G	Energy in eV
Proton	monoenergetic or average	P	Energy in eV
Deuteron	monoenergetic or average	D	Energy in eV
Triton	monoenergetic or average	T	Energy in eV
Helium-3	monoenergetic or average	3	Energy in eV
Helium-4 (alpha particle)	monoenergetic or average	A	Energy in eV
Helium-6	monoenergetic or average	6	Energy in eV

These are then followed by four integers in “4I3” format (to use FORTRAN terminology); these give, in order, the target nuclide charge and mass, and the product’s mass and charge. The character following this gives the product’s isomeric state.

It should be noted that the sign of the product charge field for ternary fission products is used as a flag. If negative it denotes that the yield was measured using the number of fission fragments of a given mass and (where loss of energy of the fragment can be determined) charge, counted in a detector. Whereas a positive value denotes that the

yield was determined by a radiochemical technique, such as mass or gamma-ray spectrometry.

The last character in the yield identifier field describes the yield type as in Table 2.2.

Table 2.2: Yield type identifier

Yield Type	Identifier
Chain yield	H
Cumulative Yield	U
Independent yield	N
Fractional Cumulative Yield	I
Fractional Independent yield	M
Charge yield	G

The yield data consists of the following items in the given order: (i) the measured yield, (ii) the one standard deviation uncertainty given as a percentage of the yield value, (iii) a five digit integer to give the reference identifier and (iv) for cumulative and chain yields, a character flag to show whether the measurement should be used to estimate the weighted averaged chain yield ('Y' for yes and 'N' for no).

For chain, charge, cumulative and independent measurements the yields are given as percentage per fission, i.e. yield per 100 fissions, while for fractional yields the values are given as ratios.

For the **RFYDB** files the FORTRAN77 data format specifier is as follows: 2(a1,1x,e9.3,4i3,a1,a1),(1x,e9.3,1x,e9.3,i5,a1). This corresponds to 2 yield identifiers and a yield data section. The first identifier is for the "unknown" and the second for the "standard". The yield data section gives the ratio of the "unknown" to the "standard". Both of the identifiers have fields as described for FYDB as does the yield section apart from the first value which is the measured ratio.

An example is shown below:

```
B 0.000E+00 92235 88 37 NB 0.000E+00 92235 93 37 N 2.000E-03 1.000E+02 2008
```

For the **RVALFYDB** files the FORTRAN77 data format specifier is as follows: 2(a1,1x,e9.3,4i3,a1,a1),(1x,e9.3,1x,e9.3,i5,a1). This is the same format specifier as the RFYDB file. However, here the first yield identifier contains information on the first irradiation conditions and the “unknown” nuclide. The second identifier contains information on the second irradiation and the “standard” nuclide. The yield data section gives the R-value, the standard deviation as a percentage of the R-value, the reference identifier and, for chain and cumulative yields, whether to include the measurement in the estimation of the chain yield.

If the activity of a nuclide x in the nth sample is given by A_x^n , then the R-value for “unknown” x to “standard” s for the two irradiations is given by:

$$\frac{A_x^1}{A_x^2} \times \frac{A_s^2}{A_s^1} \quad \text{Eqn (2.13)}$$

If the measurement procedures for the two samples are the same it follows that the detector efficiencies, γ intensities per decay and the number of fissions will be the same. Thus these effects cancel and the activity, A_x^n , can be replaced by the yield, Y_x^n , in the above expression.

An example from the file is shown below:

```
B 0.000E+00 90229136 55 NB 0.000E+00 92235 99 42 U 2.567E+02 0.200E+02 300
```

2.3 Data sources

The sources of data for an evaluation are any relevant reported experimental results. The data are found by literature searches, studying other compilations and evaluations, or by searching specialist databases.

For UKFY2 and UKFY3 the main source of new data were the CINDA and EXFOR databases maintained by the Nuclear Data Centres’ “4 Centre Collaboration”. The other sources were obtained via literature searches using the INIS database.

During the production of UKFY3 CINDA and EXFOR were extended to include a

conversion of parts of the measurement database generated in 1980 by Meek and Rider^[2.2] for their fission product yield evaluation. These data were converted to EXFOR format and added to the EXFOR and CINDA databases by V.McLane of the Brookhaven National Laboratory. These new data increased the UKFY3 database's coverage of early U.S. measurements. The Meek and Rider evaluation became part of the ENDF/B-V evaluated file.

The UK evaluations started with the work of Cunningham and Crouch in the 1960's; this was continued with increasing links to the US evaluation effort (Meek and Rider) until 1981. After this the work was continued by M.F.James and J.Banai, who produced the UKFY1 evaluation, which was adopted for JEF1. Within the current project the UKFY1 experimental database was converted to the new format described above and considerably updated and checked. It was then used to produce UKFY2. Further extension of the database and re-evaluation within the studentship has led to UKFY3. The relative sizes of the recent databases are shown in Table 2.3 below:

Table 2.3: Number of data items in the UK experimental databases

Dataset	Absolute measurements	ratio measurements	ratio of ratio measurements	Total
UKFY1	7448	0	0	7448
UKFY2	10768	684	1506	12958
UKFY3	11887	1352	1471	14710

It should be noted that refined checking procedures for UKFY3 removed many duplicate reports of single measurements which had appeared in different references. This applied particularly for relative and ratio of ratio measurements which previously had been converted to absolute measurements on entry to the database using then current yield values. Thus these repeated measurements could have different values in the database making their discovery more difficult.

[2.2] Lab report from Vallecitos Nuclear Center, U.S.A. "Compilation of Fission Product Yields, 1980" by B.F.Rider. General Electric Company Report number NEDO-12154-3(C) (1981)

2.4 Experimental uncertainties

As will be come apparent in the next chapter the experimental uncertainty is a very important parameter in the analysis of data.

Experimentalists often report an uncertainty that is related to the random ('statistical') variation between the measurements that are analyzed to produce the value they quote; an example of this would be analysis based on the variation of counts in a detector during several runs. However, in any experiment there are many variations in the measurement system that may be important (i.e. pressure, temperature or even, as observed in high precision particle physics experiments at CERN, the phase of the moon^[2.3]). Each experiment will have a large number of system changes which should be considered, although few experiments involve apparatus large enough to be effected by the moon's tidal forces. A full study of all the uncertainties from the experiment and the data used in the analysis of the measurement must be included for the quoted uncertainty on the published result to be of practical use.

Both Crouch^[1.3] and Rider^[2.2] and [2.4] developed a list of minimum uncertainties that could be expected from different techniques, no result was allowed to be more accurate than these limits. Rider's criteria are give in Table 2.4.

Table 2.4: Rider's Guidelines for uncertainties

Method	Minimum uncertainty
mass spectrometric after 1965	0.5%
Ge(Li) and new techniques after 1965	5%
Sodium iodide and measurements 1955-1965	10%
Geiger counter and measurements pre-1955	20%
If no error given	add 10% to appropriate method uncertainty for other methods use 30%
For absolute measurements with only random errors quoted	combine error with 2% systematic error

[2.3] "Events spring surprises as Moon stretches LEP", David Miller, Physics World, January 1993.

[2.4] Private communication from T.R.England and B.F.Rider, Draft text of Los Alamos report on fission yield evaluation for ENDF/B-VI. (1988)

Crouch used the following, which although less specific kept all uncertainties above 5%.

Table 2.5: Crouch's Guidelines for uncertainties

Method	minimum uncertainty
No uncertainty data, mass spectrometric	10%
No uncertainty data, other	15%
All results	5%

In both the UKFY2 and UKFY3 evaluations Crouch's 5% minimum was relaxed to 1%, as it was observed that the difference between measurements were often less than 1% and it was felt that the best modern experiments could give results with accuracies better than 5%. Thus a 5% limit was no longer felt to be justifiable. In a study of analysis techniques by James et al^[2.5], described in chapter 3, it was observed that applying this new criteria to the database did not increase the discrepancies in the file and thus this 1% criterion was considered to be justifiable.

In a few cases new data were highly discrepant with old data. If these differences could not be resolved from the published reference the uncertainty on the new data were increased so that their weight in the analysis was no greater than any of the already present data. When this down-weighting was necessary this was noted in the database. The philosophy of this evaluation was to include all published data. However it should be emphasized that one set of data was removed from the database. This set of measurements of the tritium yield in a reactor showed differences of many orders of magnitude for almost identical samples and irradiations. As the technique employed in the measurements should have been accurate to 5% and the authors could not explain the differences in their work it was felt necessary to exclude this data from the database.

[2.5] M.F.James, R.W.Mills and D.R.Weaver "The use of the normalized residual in averaging experimental data and in treating outliers", Nuclear Instruments and Methods in Physics Research A313, 277 (1992).

2.5 The use of cumulative yields in the estimation of chain yields

Initially a definition was adopted that a cumulative yield was assumed equal to the chain yield if the fractional independent yield of the nuclide was less than 0.01 and the fractional cumulative yield was greater than 0.99. However, this was difficult to implement due to the experimental errors on the data. Thus cumulative yields of neutron rich nuclei within 2 atomic mass units of stable were flagged as appropriate for being used in the calculation of chain yields. The data were then scanned for discrepancies and any cases where the weighted mean cumulative yield was significantly different from its neighbours in the chain yield calculation had these yields flagged as “not to be included in the chain yield analysis”. Alternatively if precursors in the chain could not be distinguished from the chain yield they were flagged as “to be included in the chain yield analysis”.

2.6 Procedure for data entry and checking

The data for UKFY2 and UKFY3 came from two main sources: paper-based and computer readable.

For UKFY2 the Crouch (1981) database which had been computer based and had formed the main source for UKFY1 was converted into the new format, by a subsidiary computer program, and also checked extensively against the original papers. New references used by Banai and James in the production of UKFY1 were then inserted by hand. Next, EXFOR data was converted using a computer program that read the EXFOR data (extracted by the NEA Data Bank in 1988) and, by using user commands for each data section of each entry, converted this into the new format. Finally, the results of a literature search and new references from the evaluations of Rider and England (1988) and Wahl (1988) were added by hand.

After the data had been entered into the database a considerable amount of checking was undertaken before the evaluation process was undertaken. This included checking the range of Z and A for target and product, checking the format, checking the yield value and the accuracy, and checking for duplicated measurements (where a single measurement was reported in more than one reference). The data were then put through the initial stages of the evaluation process (as described in the next chapter) and any

major discrepancies examined to discover if typing or conversion errors had occurred; if this was the case the data were corrected and the analysis repeated.

For UKFY3 updated EXFOR database searches and an extensive literature search were employed in order to extend the database. In addition, the searches were extended to include charged particle and photon induced fission. All changes to the preliminary UKFY3 database were noted in a separate journal to allow a quality assurance audit trail. The last EXFOR search for UKFY3 was dated October 1992, and it is also known that up to June 1993 no further data were added to the EXFOR database at the Data Centres. The last entries and corrections were made to the UKFY3 database on the 29th March 1993.

In addition, the process of checking of the database was extended from that applied to UKFY2. The major extension was an improved search for duplicated measurements; this often occurred where a single experiment had been re-reported after a small correction. Unless the duplicates are removed this re-reporting effectively gives excessive weight to particular measurements in the analysis. This procedure removed a number of duplicated results from the database; thus the number of ratio of ratio measurements actually falls from 1506 to 1470 between UKFY2 and UKFY3, although this list now includes many new results.

2.7 Description of references to experimental data

The UKFY3 references in appendix 5 are given in a variety of formats; however, where possible, the CINDA/EXFOR format was used. In contrast the UKFY2 references did not use this unified system. The CINDA/EXFOR system gives the journal, proceedings or report as a standard set of abbreviations, which can be found in table 3 of the CINDA93 book published by the IAEA^[2.6]. Examples of this include “PR/C”, “JIN” and “NSE” which are the codes for “Physics Review part C”, “Journal of Inorganic Nuclear Chemistry” and

[2.6]CINDA93: The index to literature and computer files on microscopic neutron data” published on behalf of the US National Nuclear Data Centre, the Russian Nuclear Data Centre, the Nuclear Energy Data Bank and the International Atomic Energy Agency Nuclear Data Centre ISBN 92-0-102293-X.(August 1993)

“Nuclear Science and Engineering” respectively. The conference proceedings are abbreviated by the place and year such as “91Juelich” describing “The International Conference on Nuclear Data for Science and Technology, Jülich, Germany, 13-17 May 1991”.

The references in appendix 5 are given in chronologically ordered sections. The first being the 1981 Crouch references; these are followed by the Banai and James references (1986), those of James and Mills (1988), James and Mills (October 1992), the EXFOR references and finally a set of warnings. The warnings are given reference numbers of 90000 and above. These warn that either the data (although in the database) should not be used, the data are derived from a calculation or that extensive corrections were made to the data to make it of practical use.

3. Analysis Of Data

3.1 Introduction

Fission product yield evaluation has been defined above as a set of procedures. One of the steps required early in the process is the analysis of experimental data measurements to produce a set of “best estimate” recommended values. In all areas of practical, quantitative application of science it is necessary to provide scientists and engineers with physical or chemical constants to be used in calculations. These constants are usually obtained by the user community from standard references, such as the CRC Handbook of Chemistry and Physics, generally known as the “Rubber Bible”^[3.1], whose production involves the analysis of experimental measurements resulting in a recommended set of “best estimates”. These “best estimates” can then be combined with theoretical models, interpolation and extrapolation, depending upon currently accepted wisdom, to produce a complete set of data for the respective application.

Before describing the techniques used in the analysis of the UKFY3 experimental measurement database, and how these developed from those of UKFY2, it is useful to consider the fundamental basis of this type of analysis. Where a physical quantity x has been measured n times giving a set of results (x_1, x_2, \dots, x_n) and each measurement has an experimental standard deviation $(\sigma_1, \sigma_2, \dots, \sigma_n)$, what is required for practical use of these data is the “best estimate” of the parameter which can be defined as \bar{x} .

Measurements may vary widely in accuracy. Consider the commonly used statistic χ^2 defined ^[3.2] as

$$\chi^2 = \sum_{i=1}^n \frac{(x_i - \bar{x})^2}{\sigma_i^2} \quad \text{Eqn (3.1)}$$

[3.1] “CRC Handbook of Chemistry and Physics, 74th Edition” edited by D.R.Lide, CRC Press, ISBN-0-8493-0474-1 (1993)

[3.2] “Data Reduction and Error Analysis for the Physical Sciences” P.R.Bevington, McGraw-Hill Book Company (1969) Library of Congress catalog card number 69-16942

At a minimum χ^2 the partial differential with respect to \bar{x} must be zero.

$$\frac{d\chi^2}{d\bar{x}} = 0 \quad \text{Eqn (3.2)}$$

This gives;

$$\sum_{i=1}^n \frac{2}{\sigma_i^2} (\bar{x} - x_i) = 0 \quad \text{Eqn (3.3)}$$

Thus, separating the “best value” and measurement terms, gives:

$$\bar{x} \sum \frac{1}{\sigma_i^2} = \sum \frac{x_i}{\sigma_i^2} \quad \text{Eqn (3.4)}$$

If we define a weighting term for each measurement, w_i , with a value

$$w_i = \frac{1}{\sigma_i^2} \quad \text{Eqn (3.5)}$$

Then \bar{x} can be expressed as:

$$\bar{x} = \frac{\sum w_i x_i}{\sum w_i} \quad \text{Eqn (3.6)}$$

This is called the inverse variance weighted mean or, more commonly, the weighted mean, and it has the property that measurements with larger uncertainties are given less weight than those with smaller uncertainties.

To define any physical property, such as the parameter \bar{x} , in a meaningful way it is necessary to give an estimate of its uncertainty. The first method is to consider the mean as a function of the measurements, and thus making the standard statistical assumptions (each measurement is unbiased, the measurements are independent and uncorrelated and the standard deviations are known accurately) the random errors can

be propagated to give an estimate of the standard deviation of the mean. This is often called the “internal” standard deviation.

From Eqn (3.6) \bar{x} is calculated as

$$\bar{x} = \frac{w_1 x_1}{\sum w_i} + \frac{w_2 x_2}{\sum w_i} + \dots + \frac{w_n x_n}{\sum w_i} \quad \text{Eqn (3.7)}$$

Thus adding the errors in quadrature gives the variance of the mean, $\sigma_{\bar{x}}^2$,

$$\sigma_{\bar{x}}^2 = \sum_{i=1}^n \frac{w_i}{\sum w_j} \sigma_i^2 \quad \text{Eqn (3.8)}$$

and because of the definition of w_i , this simplifies to

$$\sigma_{\bar{x}}^2 = \frac{1}{\sum w_i} \quad \text{Eqn (3.9)}$$

This considers only the quoted experimental standard deviations, ignoring discrepancies in the data. As this is a least-squares fitting of the data, the technique of Birge can be applied^[3.2]. This states that the observed and predicted spread of the observations (variances) about the mean should be equal. Thus χ^2 per degree of freedom will, on average, be 1.0. Thus

$$\frac{\chi^2}{(n-1)} = 1 = \frac{\sigma_{\text{observed}}^2}{\sigma_{\text{predicted}}^2} \quad \text{Eqn (3.10)}$$

which expands to

$$\frac{\sum w_i (x_i - \bar{x})^2}{(n-1)} = 1 = \frac{\sigma_{\text{observed}}^2}{\sigma_{\text{predicted}}^2} \quad \text{Eqn (3.11)}$$

and then

$$\frac{\sum w_i(x_i - \bar{x})^2}{(n-1)\sum w_i} = \sigma_{\text{observed}}^2 \quad \text{Eqn (3.12)}$$

Thus the observed or external standard deviation is given by:

$$\sigma_{\text{external}} = \sqrt{\frac{\sum w_i(x_i - \bar{x})^2}{(n-1)\sum w_i}} \quad \text{Eqn (3.13)}$$

If χ^2 per degree of freedom is less than or equal to one, then the internal estimate of standard deviation is the larger and should be used. But if it is greater than one the external estimate of standard deviation should be used. It should be noted that

$$\sigma_{\text{external}} = \sigma_{\text{internal}} \sqrt{\frac{\chi^2}{(n-1)}} \quad \text{Eqn (3.14)}$$

The $\sqrt{\frac{\chi^2}{(n-1)}}$ term is referred to as the Birge factor and gives a guide to the “goodness of fit” of the data. It clearly relates to the standard statistical χ^2 test where the probability of a set of measurements having a certain χ^2 value can be derived from mathematical tables, for example in the Handbook of Chemistry and Physics^[3.1]. If the probability of a set of data having a χ^2 value is very small then the experimental data may contain erroneous entries and, by finding the entry with the largest contribution to χ^2 , it is possible to find the most discrepant data point.

3.2 Techniques for removing or down-weighting discrepancies

When any discrepancy is found the first attempt to resolve the problem must be to look at the original data reference. It may be that the data was incorrectly entered into the analysis, the experiment was incorrectly published or the technique used contained a bias that was not corrected for by the experimentalist. However, in most cases, a paper in a peer reviewed journal is unlikely to contain easily identifiable errors.

If this direct approach to resolve the discrepancy fails then the reported data must be the guide to the evaluator. There are three approaches to solving the problem. Firstly, the evaluator can ignore the problem, and rely on the fact that the discrepancy will increase the external estimate of error on the weighted mean. This however leaves a suspiciously large and possibly unjustifiably estimate of error, particularly if the discrepant datum is upsetting an otherwise reliable and accurate data set. This is clearly unreasonable when an evaluator's purpose is to produce the best estimate with the smallest justifiable uncertainty. Secondly, removing the discrepant datum from the analysis will remove the problem, however this may mask the fact that a measurement method or its implementation was wrong, or even that the apparently discrepant measurement was correct and the other measurements wrong. The third technique is to adjust the discrepant measurement. This can be either be by adjusting the measured value or its uncertainty. If no reason or theory for a bias can be found the value cannot justifiably be altered thus the uncertainty is the only parameter that can be adjusted. This adjustment should only occur **within the analysis** not by adjusting the database as that would lead to inconsistencies in any further or repeated analyses if these were subsequently carried out with the altered measurement database.

There are many techniques for adjusting the uncertainty to decreasing the weight of a data point in the analysis. Rajput and MacMahon^[3.3] have recently summarized several techniques and developed a new method. One of the techniques studied in their work was developed for use in the UKFY2 evaluation^[2.5] and is based upon the properties of the “normalized residual”, r_i , defined by

$$r_i = \sqrt{\frac{w_i W}{W - w_i}} (x_i - \bar{x}) \quad \text{Eqn (3.15)}$$

where W is the sum of the individual weights defined by $W = \sum_{i=1}^{i=n} w_i$.

This parameter allows the quantification of discrepancy of a measurement to the total dataset, the measurement i with the largest value of $|r_i|$ being the most discrepant. The

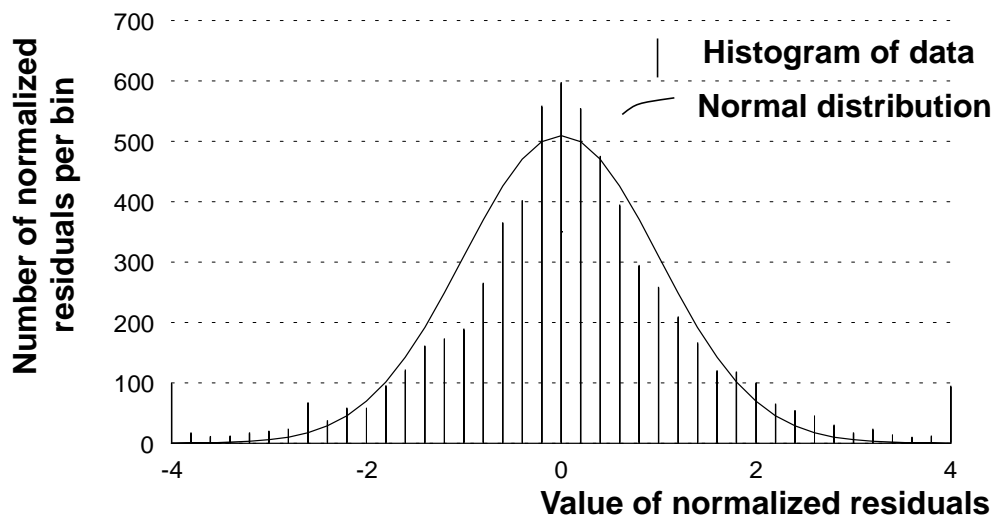
[3.3] “Techniques for evaluating discrepant data”, M.U. Rajput and T.D.MacMahon, Nucl. Inst. and Methods in Physics Research A312 (1992) p289-295.

removal of this measurement from the set will cause the largest reduction in χ^2 .

The normalized residual is normally distributed about zero and thus it is possible to define a maximum value beyond which it is unreasonable for a measurement consistent with the other data to exist. The most discrepant value can then have its uncertainty increased such that $|r_i|$ is equal to this maximum value. In this work 2.5 was chosen as the maximum value, a choice which appeared consistent with statistical tests of the total data set. In practice the data set, now including the revised uncertainty, is then reanalyzed and the procedure repeated if any further points are found now to have normalized residuals beyond the 2.5 limit.

In previous work towards UKFY2^[2.5] the distribution of normalized residuals were plotted for the UKFY2 database and shown to be distributed as predicted by theory with a small number of large discrepancies.

Figure 3.1: Normalized residuals for all fission yield data in UKFY2 compared to expected normal distribution.



The work of Rajput and MacMahon^[3.3] showed that the above procedure gave results similar to other methods when applied to analysis of half-life measurements. None of the techniques studied by Rajput and MacMahon gave significantly better or worse results than the normalized residual technique and thus it was decided to use this technique for the analysis of the UKFY3 database.

3.3 Procedure for the analysis of the UKFY3 experimental database

For the UKFY3 evaluation each product and yield type (chain, cumulative, fractional cumulative, fractional independent and independent yields) were analyzed for all measurements. The technique that has evolved for the analysis of UKFY3 can be traced back to the first UK evaluation where computers were used for analysis.

In 1973 Crouch^[3.4] described his technique of analysis as consisting of producing inverse variance weighted averages of repeated yield measurements; the uncertainty upon the resulting recommended yields being estimated by two methods. The first was through error propagation of the assessed measurement uncertainties in the averaging process, in other words the “internal” estimate of standard deviation of the weighted mean referred to above. The second technique is based upon the variation of the data from the simple mean, similar to the “external” standard deviation. The recommended uncertainty being the higher of the two estimates.

If the errors are normally distributed and the data are well represented by the sample available to be averaged then these two uncertainty estimates will be the same. If however, the errors are not normally distributed or the data is discrepant, the external value will differ. If a measured value is erroneous or its estimate of uncertainty is too small the external value will be larger. Alternatively, if the quoted uncertainties are too large or the data is highly correlated, for example a single measurement has been reported several times, the external value will be smaller. A χ^2 test was used to check the data for discrepancies.

Crouch converted relative and “ratio of ratio” data into absolute values on entry of the data to his database and updated this with new standard values on an “ad hoc” basis when significant changes were made to the standard yields used.

In the evaluations of Crouch, 1977^[3.5] and in James and Banai’s work, 1986 (UKFY1,

[3.4] “Fission product chain yields from experiments in reactors and accelerators producing fast neutrons with energies up to 14 MeV”, E.A.C. Crouch, AERE-R7394 (1973).

[3.5] “Fission product yields from neutron-induced fission”, E.A.C. Crouch, Atomic Data and Nuclear Data Tables, vol.19, no. 5 (1977).

which become part of JEF1) the same procedures were used.

However, with the UKFY2 evaluation of James, Mills and Weaver^[1.4] the database file was converted into a form where the 3 data types (absolute, relative and “ratio of ratio”) were placed in separate files. This allowed a recursive evaluation procedure to be used. Initially, estimates of the standards were produced using only the absolute data; these were then used to convert the relative and “ratio of ratio” measurements to absolute values which were only then merged with the absolute values and the set reanalyzed. This second set of data was then used to reconvert the relative and “ratio of ratio” measurements to absolute values before a final merging and analysis were performed.

The UKFY2 and UKFY3 analysis, unlike earlier UK evaluation, used the method described above of renormalizing the assessed uncertainties of individual measurements^[2.5] during the analysis procedure.

The effects of further iteration of the analysis were not studied for the UKFY2 analysis due to time constraints. However, for UKFY3 the effect of further steps of the recursive analysis of relative and “ratio of ratio” measurements were studied. The results of these studies are described below in section 3.3.2.

The basic analysis procedure, as justified above, has been described in James, Mills and Weaver^[1.4] and is as follows.

For a set of n measurements of value x_i and assessed standard deviation σ_i the mean \bar{x} is defined as:

$$\bar{x} = \sum_{i=1}^{i=n} \frac{w_i x_i}{W} \quad \text{Eqn (3.16)}$$

where W is the sum of the individual weights

$$W = \sum_{i=1}^{i=n} w_i \quad \text{Eqn (3.17)}$$

and the i^{th} weight is:

$$w_i = \frac{1}{\sigma_i^2} \quad \text{Eqn (3.18)}$$

The internal and external standard deviations are, respectively:

$$\sigma_{\text{int}} = \frac{1}{\sqrt{W}} \quad \text{Eqn (3.19)}$$

and

$$\sigma_{\text{ext}} = \sqrt{\frac{\sum_{i=1}^{i=n} w_i (x_i - \bar{x})^2}{W(n-1)}} \quad \text{Eqn (3.20)}$$

A useful test of the consistency of the data is the χ^2 test:

$$\chi^2 = \sum_{i=1}^{i=n} w_i (x_i - \bar{x})^2 \quad \text{Eqn (3.21)}$$

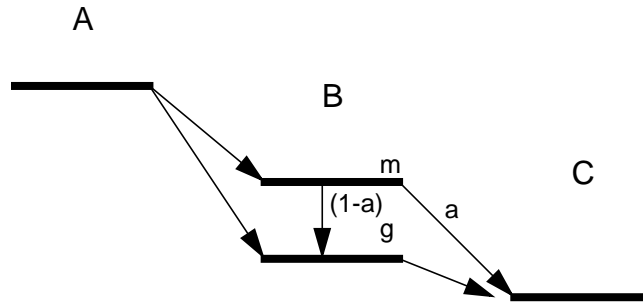
For cumulative, independent, fractional cumulative and fractional independent yields this procedure is applied simply for each data subset of the same incident neutron energy (or spontaneous fission), target actinide and product nuclide.

3.3.1 Procedure for chain yields

For chain yields it is necessary firstly to determine which cumulative yields at the end of the decay chain are equivalent to the chain yield to decide which measurements to include in the averaging process. This was carried out using the procedure described in section 2.5.

In addition, some chains have isomeric states in the nuclides near the end of the chain, as shown in the figure below. In UKFY2 and UKFY3, where the fractional independent values were small, the cumulative yields of the isomeric states could be used with the

decay data to supplement the data used to determine the chain yield^[1.4].



Typical Decay Scheme at the end of a decay chain

The figure shows a nuclide A which decays to both the ground and metastable states of nuclide B. These two states of nuclide B both decay to nuclide C.

Nuclide C is either stable, or its cumulative yield can be assumed to be equal to the chain yield Y. Nuclide B has two isomers: a ground state, g, with cumulative yield G and an metastable state, m, with cumulative yield M. A fraction a of the metastable state decays are by β^- emission to C, the remainder decaying by internal transition to the ground state. Measurements of M, G and Y were first analyzed separately to produce means and standard deviations as described above. The means were then adjusted by least-squares to fit the condition:

$$Y = G + aM \quad \text{Eqn (3.22)}$$

which holds if the independent yield of C is negligible.

If the unadjusted means and standard deviations are indicated by bars, then the adjusted chain yield, Y, is given by:

$$Y = \bar{Y} - (\bar{Y} - \bar{G} - a\bar{M})\bar{\sigma}_Y^2/D \quad \text{Eqn (3.23)}$$

with the adjusted standard deviation of Y, σ_Y , given by:

$$\sigma_Y^2 = \bar{\sigma}_Y^2(\bar{\sigma}_G^2 + a^2 \bar{\sigma}_M^2)/D \quad \text{Eqn (3.24)}$$

where

$$D = \bar{\sigma}_Y^2 + \bar{\sigma}_G^2 + a^2 \bar{\sigma}_M^2 \quad \text{Eqn (3.25)}$$

and, where $\bar{\sigma}_Y$, $\bar{\sigma}_G$ and $\bar{\sigma}_M$ are the unadjusted standard deviations of Y, G and M respectively. This analysis ignores any uncertainty in the branching fraction, a.

The value of χ^2 for the fit to Eqn (3.22) is:

$$\chi^2 = (\bar{Y} - \bar{G} - a\bar{M})^2/D \quad \text{Eqn (3.26)}$$

with 1 degree of freedom. If $\chi^2 > 1$, then σ_Y is multiplied by the Birge factor $R_B = \sqrt{\chi^2}$.

3.3.2 Recursive iteration of the data analysis

The procedure mentioned above can be considered as a operator A acting upon an experimental dataset of absolute measurements producing weighted means and estimates of the standard deviation of the means. Thus the first estimate of recommended yields and standard deviations, r_0 , can be calculated from the set of data containing the absolute measurements (I shall call this set a). This analysis can be represented by an operator, A.

Thus

$$r_0 = A[a] \quad \text{Eqn (3.27)}$$

The relative and ratio of ratio measurements set (defined as f) can then be converted to absolute values if the appropriate absolute measurements exist in the recommended yields. This conversion of set f to absolute yields can be considered to be an operator C to generate a corresponding set of absolute measurement values b i.e.

$$b = C(f, r_0) \quad \text{Eqn (3.28)}$$

Thus, combining a and b and then reanalyzing gives a revised set of recommended

yields r_1 i.e.

$$r_1 = A[a + C(f, r_0)] \quad \text{Eqn (3.29)}$$

This can then be easily iterated

$$r_n = A[a + C(f, r_{n-1})] \quad \text{Eqn (3.30)}$$

In the trivial case where a yield in r is not a function of any measurements in f , i.e. it is a standard or has only been measured absolutely, then

$$r_n(\text{standard}) = A[a] = r_0(\text{standard}) \quad \text{Eqn (3.31)}$$

as $A[A[a]]$ must equal $A[a]$.

If we consider a secondary standard which has been both measured absolutely and is related to a standard via f then

$$r_n \left(\begin{smallmatrix} \text{secondary} \\ \text{standard} \end{smallmatrix} \right) = A[a + C(f, A[a])] = r_1 \left(\begin{smallmatrix} \text{secondary} \\ \text{standard} \end{smallmatrix} \right) \quad \text{Eqn (3.32)}$$

Now if a third level standard is related to a second level standard it follows that

$$\begin{aligned} r_n \left(\begin{smallmatrix} \text{third-level} \\ \text{standard} \end{smallmatrix} \right) &= A[a + C(f, A[a + C(f, A[a])])] \\ &= r_2 \left(\begin{smallmatrix} \text{third-level} \\ \text{standard} \end{smallmatrix} \right) \end{aligned} \quad \text{Eqn (3.33)}$$

Thus it can be seen that, applying the analysis iteratively, the recommended yields will become constant depending upon the maximum number of levels from which a yield is related to an absolute measured “standard”. It should be noted that this analysis method only includes each measurement in sets a and f once at each step of the iteration and thus does not excessively weight the ratio data. Care was taken in UKFY3 to avoid ambiguous cases where “standards” of level n by one path are a function of standards of level $n+1$ or greater by another, which would add extra terms to the above equations and

would excessively weight the data in f. This was avoided by simply inverting the ratios of these cases. An example of this was an experiment in which yields were measured relative to barium-140 (a secondary standard) including a measurement of molybdenum-99 (which is normally a primary standard). In this case the measurement of the 99/140 ratio was converted to 140/99 in the database. In UKFY3 the analysis stabilized for all measured yields at $n=5$. Fractional independent yields stabilized at a level $n=4$.

There are 325 standards, of which 41 are used ten or more times (140 of them are used only for one relative measurement and 52 for only two). The top six are shown in Table 3.1.

Table 3.1: Commonly used standards in UKFY3 database

System	standard	yield type	number of measurements relative to standard	value of n at which standard stabilizes
U235T	Mo99	Cumulative	1119	0
U235T	Ba140	Cumulative	240	2
Pu239T	Mo99	Cumulative	143	3
U235T	He4	Cumulative	59	0
Cf252S	Ba140	Cumulative	37	3
U235T	H3	Cumulative	29	1
		Total this subset	1627	
		All standards	2906	

Now if we consider the chain yield data, which is the set with most ratio data, there are 537 yields which do change from their value at $n=0$ before converging (to 1 part in 10000) at $n=5$ out of a total of 2333 yields with measured data. Table 3.2 shows the change in the yields as a fraction of the initial ($n=0$) standard deviation. 83% of these yields change by less than one initial standard deviation and 95% change by less than two. Of these, 107 are based only on one measurement and thus directly dependent

upon the experimental estimate of the standard deviation without any independent (external) validation. If these are removed from the analysis then 85% are within one and 96% within two initial standard deviations.

Table 3.2: Changes between initial absolute yield and final converged value as a fraction of the initial standard deviation.

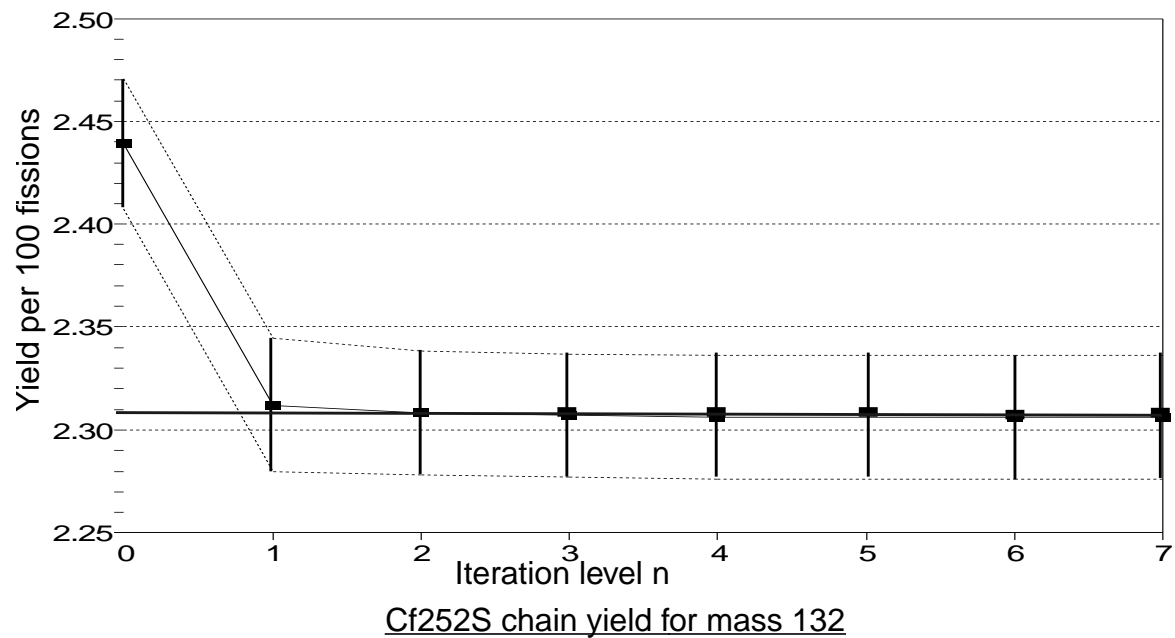
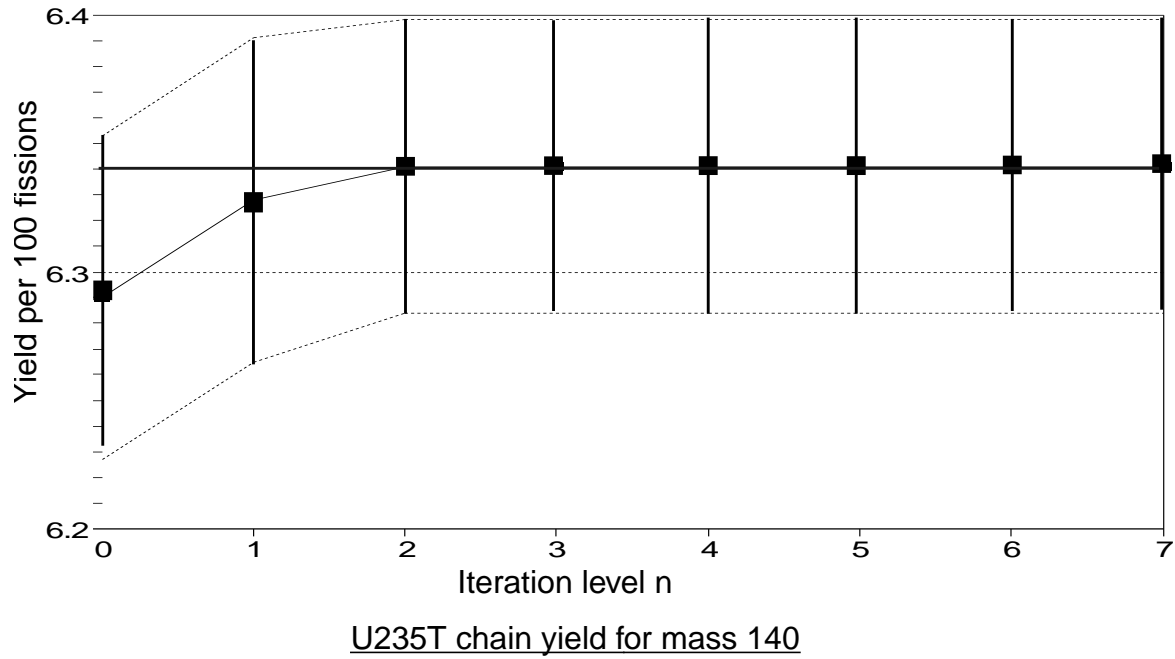
change/sd upper group boundary	For all yields			Ignoring yields with only one measurement		
	number above boundary	number in bin	fraction of total greater than boundary	number above boundary	number in bin	fraction of total above boundary
0.0	537	-	1.0000	430	-	1.0000
0.001	521	26	0.9702	416	14	0.9674
0.01	513	8	0.9553	410	6	0.9535
0.1	391	122	0.7281	306	104	0.7116
1.0	90	301	0.1676	62	244	0.1442
2.0	24	66	0.0447	15	47	0.0349
3.0	12	12	0.0223	8	7	0.0186
4.0	3	9	0.0056	2	6	0.0047
5.0	0	3	0.0000	0	2	0.0000

As an example of the recursion technique the commonly used third level standard of U235T* mass140 and a sixth level “standard” Cf252S mass 132 are shown in Figure 3.2.

It is interesting to note that the U235T mass 140 is based upon 27 absolute and 3 relative measurements, and the Cf252S mass 132 is based upon 8 absolute and 6 relative. In the Cf252S example the initial absolute estimate is extremely different from the final; over four initial standard deviations. However at n=1, where relative data has first been introduced the mean and standard deviation are very close to the final values.

* The nomenclature describing the fissioning system is the element, mass and neutron energy. Where the neutron energy is defined as: T=thermal, F=fast, H= high energy (14 MeV) and S specifies the results of spontaneous fission.

Figure 3.2: Changes for U235T mass 140 and Cf252S mass 132 with iteration level n



The points and bars represent the recommended yield and one standard deviation error at each iteration step.

The program that implemented the operators A and C is called ANALYSE, and this produced for each yield type: a set of recommended yields for use in subsequent programs; tables of the experimental data with recommended yields; and tables summarizing discrepancies as well as sparse data. The tables of chain and fractional independent yields for UKFY2 were published in two reports^{[1.5][1.6]}, and those for UKFY3 are found in appendices A1 to A5 of this thesis. Crouch for his 1977 evaluation produced similar tables^[1.3] based upon absolute data.

4 Chain Yields

4.1 Introduction

The techniques of analysis described in chapter 3 were applied to the UKFY3 measurement database to provide a “best estimate” set of the fission product yields and their uncertainties. This dataset covers a wide range of fissile nuclei from ^{227}Th to ^{257}Fm . However the completeness of the coverage varies considerably between different fissioning systems and yield types.

Because they relate to nuclides which are more easily identified and measured, the long-lived cumulative and chain yields measurements are more numerous and cover a wider range of fissioning systems and product masses than the other yield types. Also these nuclides are stable or have relatively long half-lives and the largest possible yields for their mass chain and this means that greater measurement precision can be achieved. Thus these yields give the most accurate insight into the production of fission products.

Even so, only for a limited set of fissioning systems are the chain yield distributions well defined. The thermal neutron fission of ^{235}U has a complete set of measurements of chain yields between masses 72 and 161. This represents all chain yields with a probability above 10^{-6} per fission. However, in other important systems gaps are common, especially in the valley region and at the wings of the distribution. In many of the remaining systems, especially the higher actinides, large regions exist where no measurements are available. At the extreme some fissioning systems have no measurements at all.

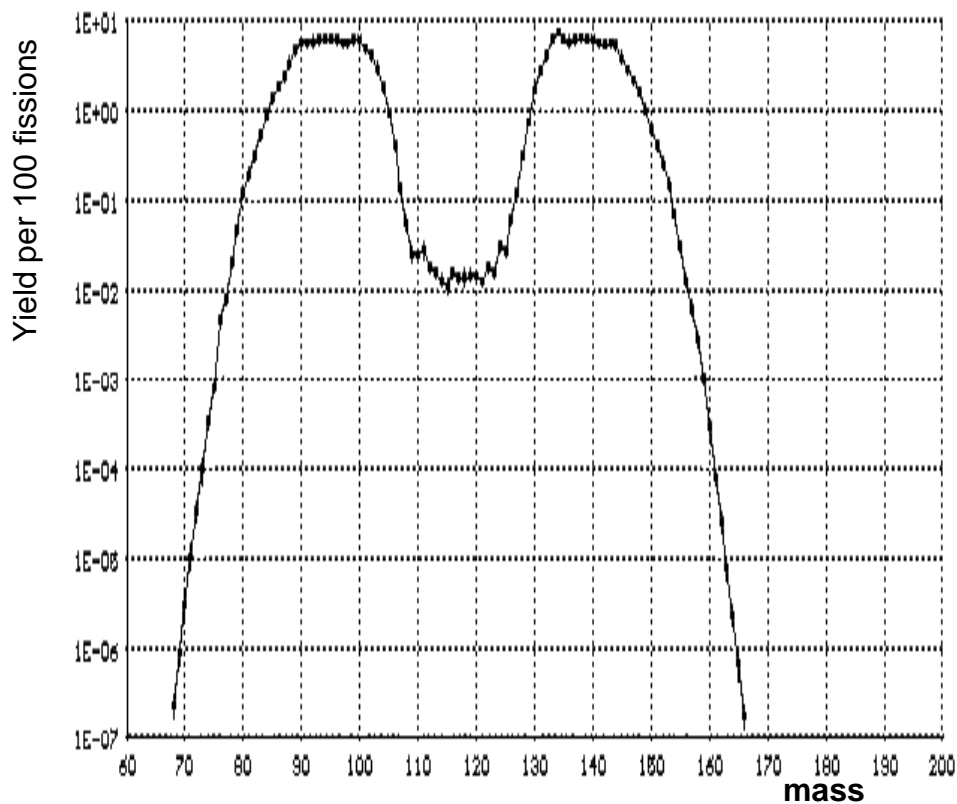
These long-lived cumulative yields are important for fuel handling and waste management applications. The nuclide inventory and its associated radiations before removal from the reactor are important for the studies of reactor operation, and accident scenarios where the fission products are released from the fuel matrix.

The need to produce complete chain yield distributions for practical applications has led to the development of empirical models and to attempts to understand the underlying principles of the processes giving rise to these distributions.

4.2 Modelling of chain yields

The observed chain yield distributions of most nuclides show a common set of features. The distribution consists of pair of peaks with a valley between them. The distribution is approximately symmetrical about the centre of the valley. This central mass is approximately the mean mass of the distribution. Figure 4.1 shows the mass yield curve for the thermal neutron fission of ^{235}U . This graph is taken from the JEF-PC program^[4.1] which is based upon the JEF2.2 evaluated file.

Figure 4.1: The mass distribution of fission products produced in the thermal neutron fission of ^{235}U .



The chain yield curves show trends with excitation energy and compound nucleus mass. It is observed that as the compound nucleus mass increases the light mass peak moves upwards but the heavy mass peak does not change position significantly. For some very massive compound nuclei the two peaks essentially merge into a single peak. An

[4.1]“JEF-PC: A program for displaying data from the Joint Evaluated File (JEF)”, OECD Nuclear Energy Agency, Le Seine St-Germain, 12 boulevard des Îles, 93130 Issy-les-Moulineaux, France. This program was jointly produced with the University of Birmingham, U.K. and CSNSM, Orsay, France.

example of this is the neutron fission of ^{257}Fm .

Colby et al^[4.2], employing alpha particle induced fission of ^{238}U with alpha particle energies of up to 40 MeV, showed that the peaks did not significantly alter position laterally with increased excitation energy.

On the other hand the yields in the valley region do increase with increasing excitation energy; however, despite the valley becoming less pronounced with increasing energy, Colby et al showed that a valley is still observed for 40 MeV helium-ion induced fission of ^{238}U .

It was realized^[4.3] that the chain yield distribution could be fitted empirically by the summation of a set of Gaussians if the small fluctuations on the distribution, believed to be shell effects, were ignored.

Attempts to model chain yields (and the closely related mass yields) from basic nuclear theory have been qualitatively successful. Turkevich and Niday^[4.4] considered the mass distribution of thorium as a result of multiple routes or “channels” from the excited nucleus to the point of scission i.e. breaking apart into fission fragments. However, quantitative attempts to explain the widths of the distributions by Whetstone^[4.5] and Karamyan et al^[4.6] could not explain the large widths observed experimentally without employing the concept of the neck between the two fragments rupturing at a random point along its length. Griffin and Kan^[4.7] proposed that this random neck rupture could arise from the hydrodynamic instability known as the Rayleigh instability where a small dent in a liquid drop or stream caused by fluctuations in the liquid surface could deepen and cause cleaving of the liquid. Brosa et al^[4.8] used these ideas to determine some of

[4.2] Phys. Rev. 121, 1415. L.J. Colby, M.L. Shoaf and J.W. Cobble (1961)

[4.3] Proc. Panel on Fission Product Nuclear Data, Bologna. Report IAEA-169, volume 2, p163-200. A.R. Musgrove, J.L. Cook and G.D. Trimble (1973)

[4.4] Phys. Rev. 84, 52. A. Turkevich and J.B. Niday (1951)

[4.5] Phys. Rev. 114, 581. S.L. Whetstone (1959)

[4.6] Sov. J. Nucl. Phys. 11, 546. S.A. Karamyan, Yu. Ts. Oganessian and B.I. Pustylnik (1970)

[4.7] Rev. Mod. Phys. 48, 467. J.J. Griffin and K.K. Kan (1976)

[4.8] Physics Reports (Review section of Physics Letters) 197, no. 4, 167. U. Brosa, S. Grossmann and A. Müller (1990)

the parameters of the mass distribution of fission fragments from several fissioning systems with quantitative success within the uncertainties of the basic nuclear parameters.

4.2.1 The Brosa model of multi-channel fission with random neck rupture

Brosa et al^[4.8] suggested a theory based upon the liquid drop model to explain the mass distribution from the fission of the excited compound nucleus resulting from low energy neutron absorption by a fissile nucleus. It should be noted that their work derived the fragment mass at scission of the two proto-fragments, i.e. before any prompt or delayed neutron emission. Thus $\bar{\nu}_p(A)$ and (to a smaller extent) delayed neutron emission must be considered in order to produce chain yield distributions from their work.

Their model considers the compound nucleus to be a liquid drop whose shape is described by five parameters. In a space defined by these shape parameters the potential energy surface can then be calculated using the approach of Strutinsky where the potential energy of the deformed nucleus E_{def} is composed of liquid drop and shell parts:

$$E_{\text{def}} = E_{\text{liquid drop}} + E_{\text{shell}} \quad \text{Eqn (4.1)}$$

The E_{def} can be calculated using models for the two components. Brosa et al used the Myers-Swiatecki model^[4.9] for the liquid drop component and their own treatment for the shell component. These results suggested that there exist “channels”, minima in the multi-dimensional potential energy surface, in which the nuclear shape would evolve before fission. As the results were 6 dimensional (5 shape parameters and the calculated E_{def}) a multi-dimensional channel searching technique was used. It was found that as the nuclear shape evolved there were points at which a channel divided into two. These were named ‘bifurcation points’. The different channels refer to different paths of evolution of the nucleus shape. This means that there are several possible nuclear shapes through which the nucleus could evolve as it approaches fission.

[4.9] Nucl. Phys. 81, 1. W.D. Myers and W.J. Swiatecki (1966)

Brosa et al found three channels were predicted from the calculations for most fissioning systems. However their investigation of the thermal neutron fission of ^{252}Cf predicted six channels.

When a channel reaches scission it is possible to derive the compound nucleus shape. This can then be used to determine the mass distribution by using the idea of random neck rupture.

Brosa et al describe ordinary fission as proceeding via a series of instabilities in the evolution of the shape of the nucleus. Firstly the fission barriers have to be passed; after this the nucleus develops an indentation in the middle, which with further stretching, becomes a neck between the two proto-fragments. Secondly the neck becomes flat and then thins in the middle. Finally, as the neck thins, random fluctuation in the nuclear material of the neck can produce a small indentation in the surface. This will rapidly deepen, due to Rayleigh instability, until the nucleus is pushed apart by Coulomb repulsion. It should be noted that once past the fission barrier the process, although governed by a potential which consists of liquid drop and shell components, is based upon fluid dynamics.

Each of the channels was shown to give rise to a mass distribution which can be well fitted as the sum of two Gaussian distributions. It should be noted that in this model the Gaussian distribution is used as it gives a good fit to the results of the numerical calculations.

The total mass yield, $Y(A)$, is the sum of the product of the individual channel mass distributions with the probability of the fission proceeding via that particular channel. This can be described by:

$$Y(A) = \sum_c P_c Y_c(A)$$

$$Y_c(A) = \frac{1}{\sqrt{2\pi\sigma_{A,c}^2}} \left[e^{-\left(\frac{(A - \bar{A}_c)^2}{2\sigma_{A,c}^2}\right)} + e^{-\left(\frac{(A - A_{cn} + \bar{A}_c)^2}{2\sigma_{A,c}^2}\right)} \right] \quad \text{Eqn (4.2)}$$

where P_c and $Y_c(A)$ are the probability and yield distribution of channel c . $\sigma_{A,c}$ is the width of the mass distribution of channel c . \bar{A}_c is the average mass of the channel c and A_{cn} is the compound nucleus' mass.

This is directly comparable to the multiple Gaussian model described under section 4.2.2 if for one channel \bar{A}_c equals $\bar{A}_c - A_{cn}$ i.e. \bar{A}_c is half of A_{cn} . The mass distribution of this channel then simplifies into a single Gaussian distribution.

Brosa et al quote an uncertainty on the shape parameters of 0.5 fm, due mostly to the determination of the E_{shell} . This gives rise to an uncertainty of 3 mass units on the average channel mass \bar{A}_c and 25% on the channel width $\sigma_{A,c}$. An important point to note is that the probability of each channel, P_c , is not calculated directly but is obtained by fitting to experimental data.

Thus Brosa et al have shown that it is possible to predict the **shape** of the mass distribution, but in order to determine the distribution completely experimental measurements are required.

It was noted above that, for all but ^{252}Cf , Brosa et al showed that three channels were sufficient to describe the mass distribution; in the special case of ^{252}Cf three of the channels represented 98.2% of the total chain yield distribution. When the uncertainties of the model and fitting are considered the existence of the other three extra channels cannot be definitely proven.

It should be remembered that Brosa et al have developed their theory to describe the mass distribution prior to neutron emission and decay. They then used the mass distribution to determine the neutron emission and kinetic energy of the fragments. The uncertainties on the nuclear shape just before scission give rise to uncertainties of $\pm 5\text{MeV}$ on the total kinetic energy of the fragments and ± 1 neutron on $\bar{\nu}_p$ respectively.

4.2.1.1 Energy dependence of Brosa's multi-channel model

It is interesting to note that Brosa et al^[4.8] considered the effect of small increases in the incident neutron energy on the results of their work. They noted work by Hambsch et al^[4.10] which showed that a small increase in neutron energy (from thermal to 8.77 eV) could radically change the fission fragment properties; this work studied the neutron fission of ²³⁵U. The total kinetic energy of the fragments around mass 118 was found to alter by 0.5 ± 0.2 MeV when the neutron energy was altered from thermal to 8.77 eV. Brosa et al point out that the extra fractional excitation of the nucleus is too insignificant to account for this effect when using their model. The only parameters which can change sufficiently are the probabilities of following different routes at the bifurcation points. These parameters are not calculated from the model but fitted to experimental data. The differences could therefore only be explained, in their model, by variation of these probabilities with neutron energy.

Hambsch et al also noted changes in the mass yield curve in the resolved energy region. Previous experimental yield studies (see section 4.4.2) have also reported significant changes of the yield distribution in the valley region with variation of neutron energies from thermal to 85 eV for neutron induced fission of ²³⁵U. In the Brosa model these changes could also be explained by variation of the P_c parameters.

4.2.2 Empirical Multiple Gaussian representation

The literature shows several mathematical functions which have been used to predict chain yield distributions. All of these are variations on the common theme of the distribution being expressed empirically by the summation of several Gaussian functions.

Musgrove et al^[4.3] used the sum of five Gaussian distributions (4 asymmetric and 1 central) to approximate the chain yield distribution for several fissioning systems. The model assumes that the distribution is symmetrical about an average mass (\bar{A}).

The average number of neutrons emitted by each fragment is observed to vary with

[4.10] Nucl. Phys. A491, 56. F.J. Hambsch, H.H. Knitter, C. Budtz-Jørgensen and J.P. Theobald (1989)

fragment mass and is not symmetrical about \bar{A} . This is described in more detail within chapter 6. Thus the yield distribution will be a slightly shifted away from symmetry after prompt and (to a lesser extent) delayed neutron emission. However this effect is minor compared to the fine structure observed on the distribution.

Also the sum of the magnitudes (N) of all the Gaussians is assumed to equal two. This is a direct result of the fissioning nucleus splitting into two fragments.

Each off-centre Gaussian distribution is reflected about the average mass (\bar{A}) of the whole distribution. Thus each pair of off-centre Gaussians has 3 parameters: magnitude (N), width (σ) and position from centre (D). The central Gaussian has only 2 parameters, a width and a magnitude, however the magnitude can be calculated from the total summation of the whole distribution (2.0) minus the asymmetrical Gaussian magnitudes.

Thus there are 7 free parameters used in this model as shown in the equation:

$$\begin{aligned}
 Y(A) = & \frac{N_1}{\sigma_1 \sqrt{2\pi}} \left[e^{-\left(\frac{(A - \bar{A} - D_1)^2}{2\sigma_1^2}\right)} + e^{-\left(\frac{(A - \bar{A} + D_1)^2}{2\sigma_1^2}\right)} \right] \\
 & + \frac{N_2}{\sigma_2 \sqrt{2\pi}} \left[e^{-\left(\frac{(A - \bar{A} - D_2)^2}{2\sigma_2^2}\right)} + e^{-\left(\frac{(A - \bar{A} + D_2)^2}{2\sigma_2^2}\right)} \right] \\
 & + \frac{N_3}{\sigma_3 \sqrt{2\pi}} e^{-\left(\frac{(A - \bar{A})^2}{2\sigma_3^2}\right)}
 \end{aligned} \tag{Eqn (4.3)}$$

with $N_3 = 2(1 - N_1 - N_2)$.

They showed that the parametrization could be used to fit smoothed experimental neutron induced chain yield distributions for six nuclides (^{232}Th , $^{233}, ^{235}, ^{238}\text{U}$ and $^{239}, ^{241}\text{Pu}$). The model fitted the shape of the curves over several orders of magnitude. They, therefore,

considered it to be impractical to quote an average difference between the fit and the experimental data. Instead they employed a fractional difference; the fractional difference for a given mass is defined here as the magnitude of the difference between the yield calculated from the fit and the experimental yield, divided by the experimental yield. They reported the variation in the fractional differences appeared randomly distributed about the experimental data. Thus they quoted the root mean square of the fractional deviation. The fits all had similar r.m.s. fractional deviations of around 0.1. However their investigation of the parameters did not show trends which could be used for accurate interpolation and extrapolation to other fissioning systems.

Later Cook and Rose^[4.11] continued Musgrove's work by fitting a simpler three Gaussian model to 42 fissioning systems without smoothing the data. The data were taken mainly from the then current evaluations of Crouch^[4.12] and Meek and Rider^[4.13]. However, comparison between the experimental points and predictions from the model showed a r.m.s. fractional deviation of around 0.25 for most fissioning systems. The parameters of these fits could be interpolated to different fissioning systems and different incident neutron energies (thermal, fast and 14 MeV), but the large uncertainties in the interpolated parameters produced uncertainties on the calculated chain yields which were much greater than the differences in the chain yield distributions between the fissioning systems.

Dickens^[4.14] reported a study using the five Gaussian model. He studied the fast neutron fission of ²⁴³, ²⁴⁴, ²⁴⁶, ²⁴⁸Cm for which data had recently been published. This data set was too sparse to directly fit the model. However by interpolation of some model parameters and fitting the remainder using the sparse experimental data he was able to produce complete yield sets for these fissioning systems.

4.2.2.1 Test of the multiple Gaussian approach.

[4.11] Lab report AAEC/E386 from the Australian Atomic Energy Commission Research Establishment Lucas Heights. "Test of the Three-Gaussian Assumption for Fission Product Mass Yield Curves". J.L. Cook and E.K. Rose (1976)

[4.12] Lab report AERE-R7209 from the UK Atomic Energy Authority Harwell. E.A.C. Crouch (1973).

[4.13] Lab report NEDO-12154-1 from General Electric Co., Valletos At. Labs U.S.A. M.E.Meek and B.F.Rider (1974).

[4.14] Nucl. Sci. and Eng. 96, 8. J.K. Dickens (1987).

To test the multiple Gaussian summation approach the chain yield distribution from the thermal neutron induced fission of ^{235}U was fitted to Eqn (4.2) with two to ten channels. In each fit one channel was set to be at the centre of the distribution. The experimental data set used was from the analysis of UKFY3 and contained 88 chain yields.

The results of this study is shown in Table 4.1. This shows that no improvement was obtained by using more than three channels. The large χ^2 per degree of freedom presumably derives from the fact that the model is a smooth curve approximation to the yield curve and does not attempt to follow the fine structure on the experimental results.

The accuracy of the fits was examined by studying the fractional differences of the model from the measured data. The r.m.s. of the fractional differences for three or more channels is 0.019. If the fractional differences are normally distributed then 66% of the differences should lie with ± 0.019 . Whereas in fact 66% of the differences only fall within ± 0.075 ; this shows that the fractional differences are not normally distributed. A third test is to examine the maximum deviation from the model. These results show the distribution is more centrally peaked than would be expected from a normal distribution but with a larger than expected number of extreme differences.

Table 4.1: Fitting of the chain yield distribution from the thermal neutron fission of ^{235}U with UKFY3 data using different numbers of channels.

Number of channels	χ^2	χ^2 per degree of freedom	r.m.s. fractional deviation	66% limit	Maximum deviation
2	101332	1220.9	0.050	0.250	0.939
3	3197.9	40.0	0.019	0.075	0.498
4	3183.3	41.3	0.019	0.075	0.507
5	3178.4	43.0	0.019	0.075	0.501
6	3198.9	45.1	0.019	0.075	0.501
7	3172.8	46.7	0.019	0.075	0.495
8	3165.8	48.7	0.019	0.075	0.498
9	3189.0	51.4	0.019	0.075	0.495
10	3175.7	51.4	0.019	0.075	0.495

From the overall distribution of results from the fitting with differing numbers of channels

it can be concluded that for the thermal neutron fission of ^{235}U no improvement is obtained by using more than three channels (which is directly equivalent to the sum of five Gaussian distributions).

4.2.3 Interpolation of chain yields

In addition to fitting the chain yield distributions to mathematical functions, it is possible to fill gaps in the experimental data by interpolation. Two interpolation techniques are possible. The first is direct interpolation of the chain yield distribution with mass. The second is interpolation of the chain yield for an individual mass across different fissioning systems. Both of these techniques were employed in the UKFY2 evaluation. These are discussed below using the UKFY3 data.

4.2.3.1 Interpolation of chain yields with chain mass

This form of interpolation is the simplest method of chain yield estimation. The interpolation can be either linear interpolation of chain yield with mass or of the logarithm of the chain yield with mass.

These methods have two problems. Firstly the curve has fine structure which the interpolation cannot follow. But, secondly, the curvature of the distribution on the wings and peaks is negative. Thus any straight line interpolation in these regions will always under-predict the missing yields. Conversely in the valley the curvature is positive and thus the yields would be over-predicted.

For the UKFY2 evaluation gaps of up to two masses had been estimated by linear interpolation of the logarithm of the chain yield with mass. Larger gaps were filled by the five Gaussian model. However, this does not necessarily produce a predicted value which match the experimental values at either end of a gap. Therefore, the predicted five Gaussian yields at each end of the gap were adjusted to the measured values by defining a normalisation factor, which is equal to the measured yield divided by the five Gaussian prediction. The logarithm of the normalisation factor was then assumed to vary linearly with mass across the gap. Thus by normalising the model prediction with the normalisation factor, a smooth curve could be generated. As this renormalisation technique produces a curve with an approximation to the curvature of the chain yield distribution it was adopted to fill **all** gaps in the UKFY3 evaluation.

4.2.3.2 Interpolation of chain yields with compound nucleus mass

This technique is based upon the observation by James^[4.15] that the chain yields of mass 85 for many different fissioning systems lie upon a smooth curve when plotted against the mass of the fissioning nuclide. When the plot was made against the compound nucleus mass minus $\bar{\nu}_p$ the agreement was found to be even better.

Figures 4.2 to 4.9 show the results of plotting the data in the UKFY3 database for eight masses. These masses were chosen to be representative of yields in the wings, peaks and valley of the distributions. The masses shown are 85, 99, 106, 112, 115, 125, 140 and 154. For many of the other masses the results were inconclusive; either the uncertainties were too large or there were too few experimental measurements.

It is interesting to note that yields on the wings and peaks show no energy dependence. However in the valley region there is a marked energy dependence. The figures also show the movement of the low mass peak towards higher mass with increasing compound nucleus mass. But that the higher mass peak remains stationary. It is interesting that where the low mass peak moves sufficiently upwards that a yield moves from the valley to the peak then the energy dependence disappears.

During the UKFY2 evaluation a set of functions were generated that approximated the variation of the parameters of the five Gaussian model for thermal and fast neutron induced fission. These parameters were found to be dependent upon the compound nucleus mass. As a comparison the results of these five Gaussian predictions are shown on the figures.

The figures show that interpolation of measured yields is possible, but that the uncertainties of such a prediction are about the same as that produced by the UKFY2 five Gaussian predictions. However, a definite trend away from the UKFY2 predictions occurs in the region of masses 89-100 for $(A_f - \bar{\nu}_p) < 232$. For UKFY2 these regions were fitted to straight lines on $\log Y$ against $(A_f - \bar{\nu}_p)$ graphs. However, improvements in the UKFY3 database allowed all the required fissioning systems in this region to be fitted to the five Gaussian model and thus these straight line approximations were not needed for this later evaluation.

[4.15] Private communication. M.F.James, UK Atomic Energy Establishment WInfrith (1988).

Figure 4.2: Experimental chain yields for mass 85 plotted against compound nucleus mass A_f minus $\bar{\nu}_p$.

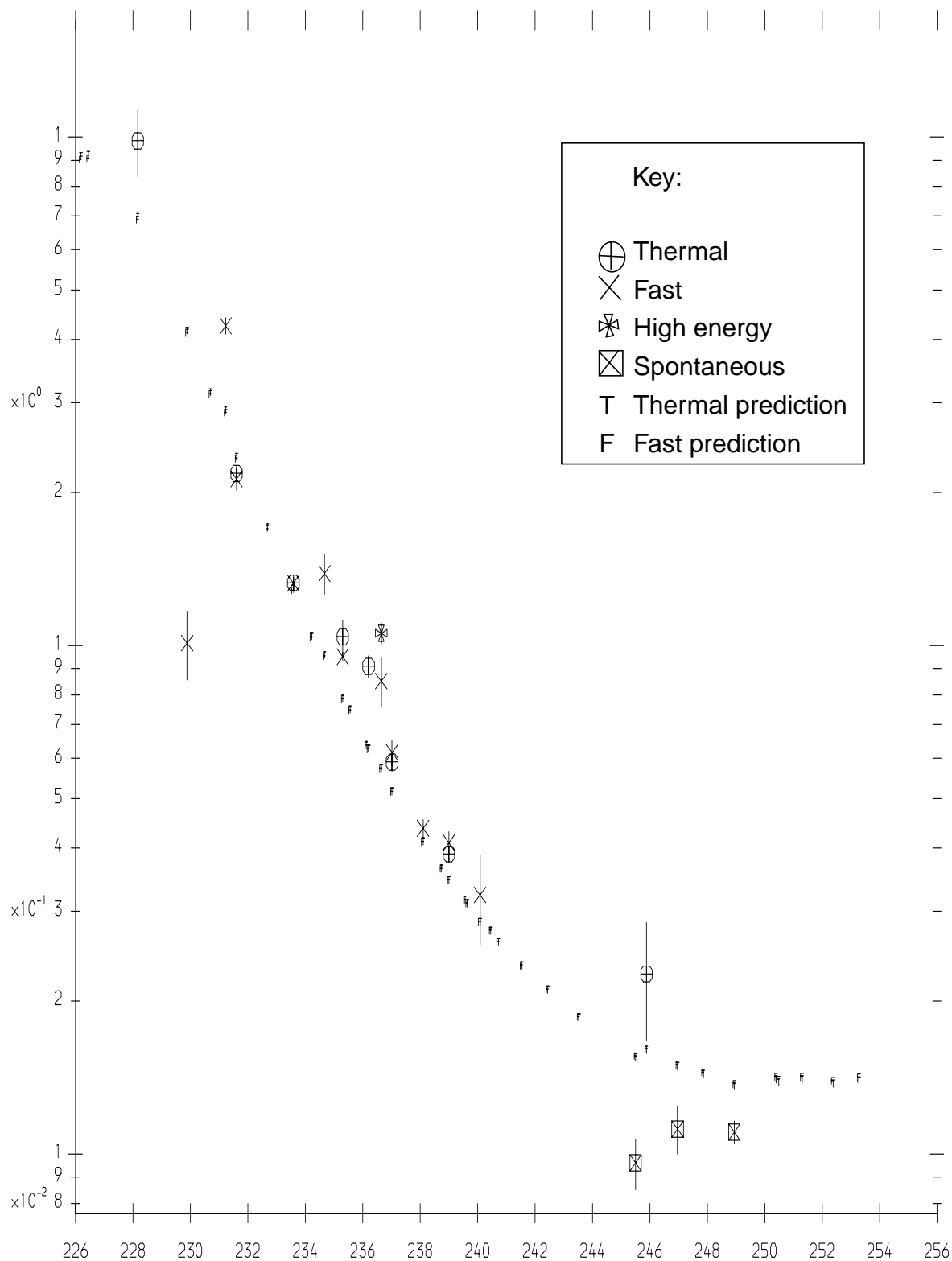


Figure 4.3: Experimental chain yields for mass 99 plotted against compound nucleus mass A_f minus $\bar{\nu}_p$.

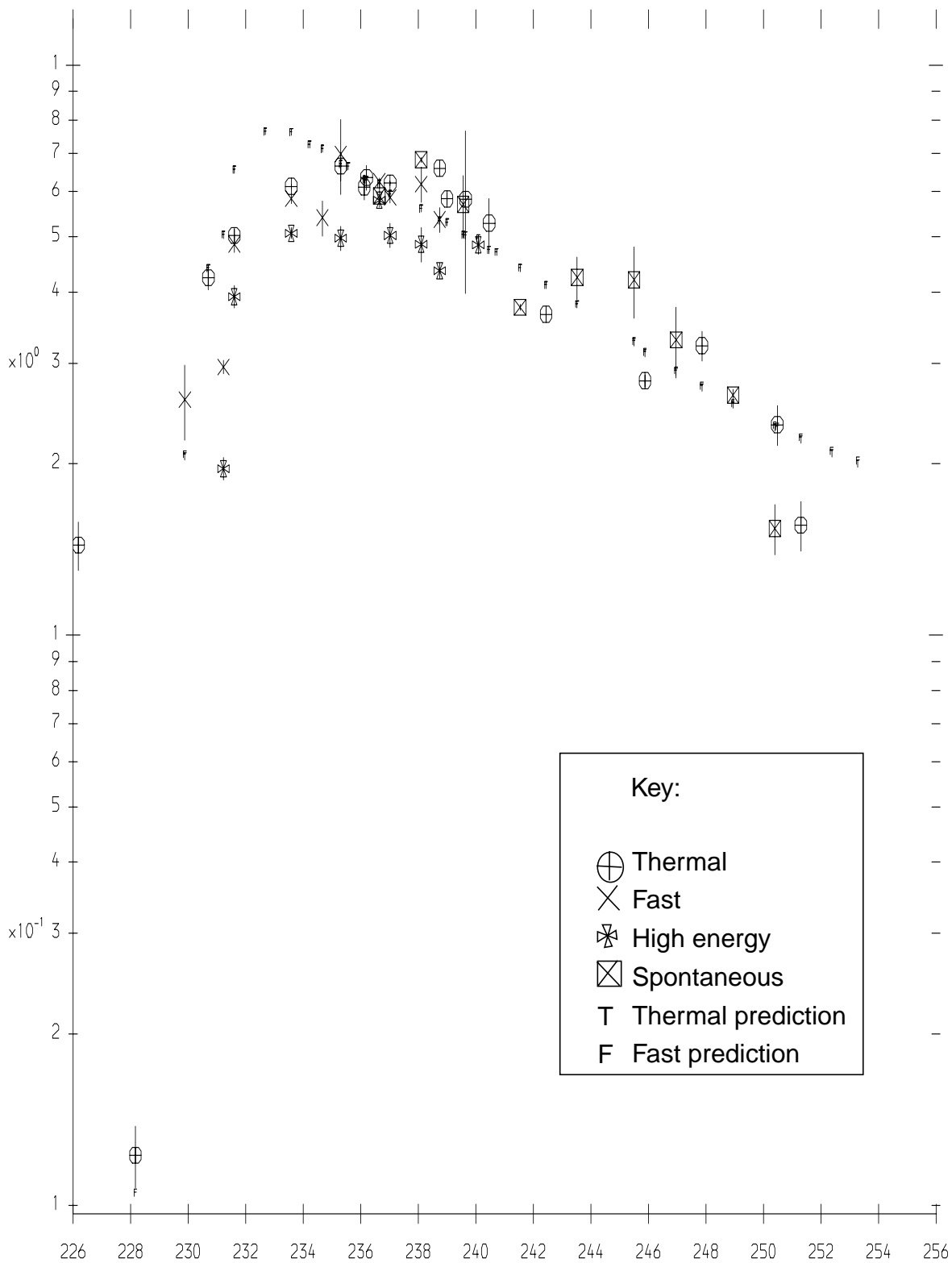


Figure 4.4: Experimental chain yields for mass 106 plotted against compound nucleus mass A_f minus $\bar{\nu}_p$.

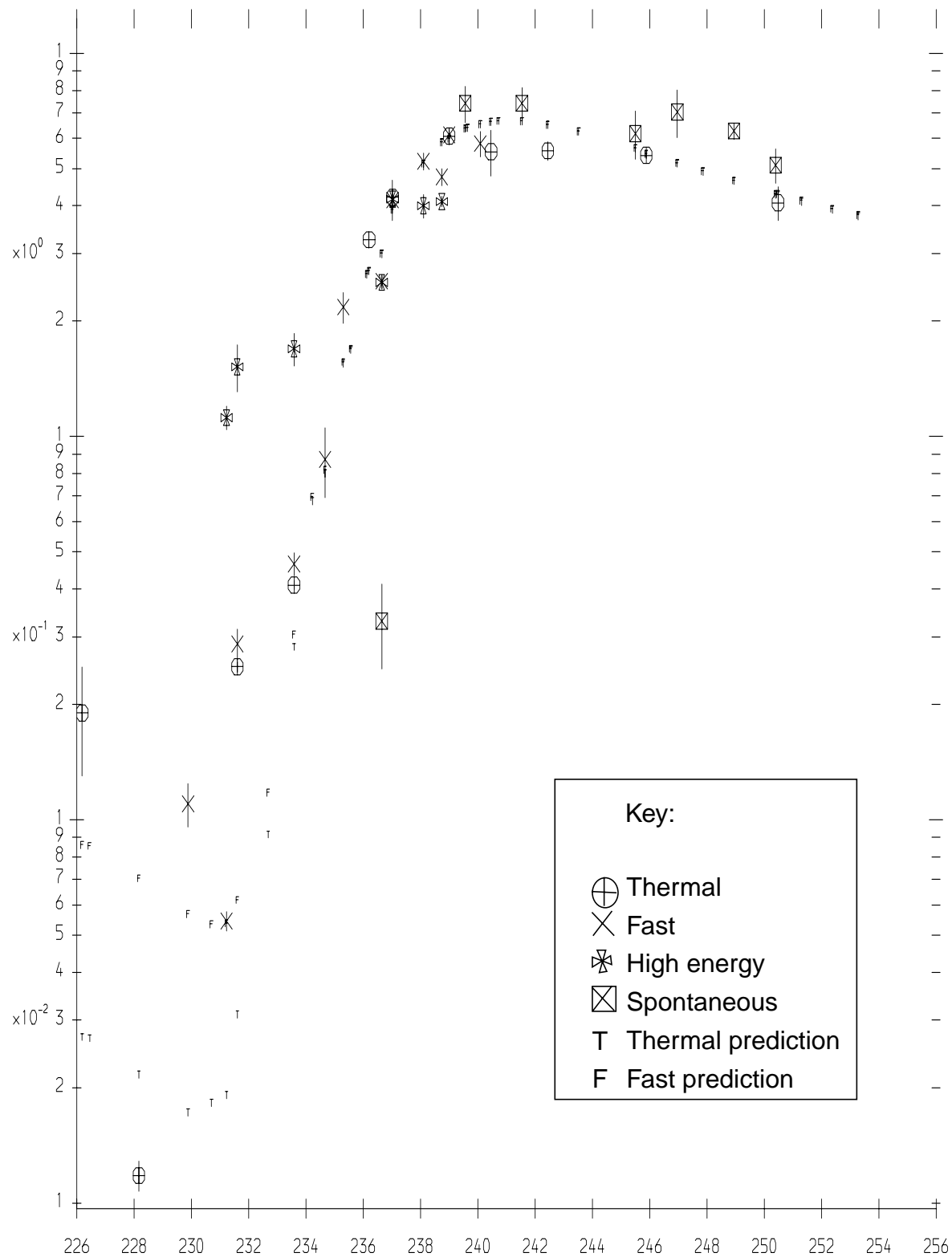


Figure 4.5: Experimental chain yields for mass 112 plotted against compound nucleus mass A_f minus $\bar{\nu}_p$

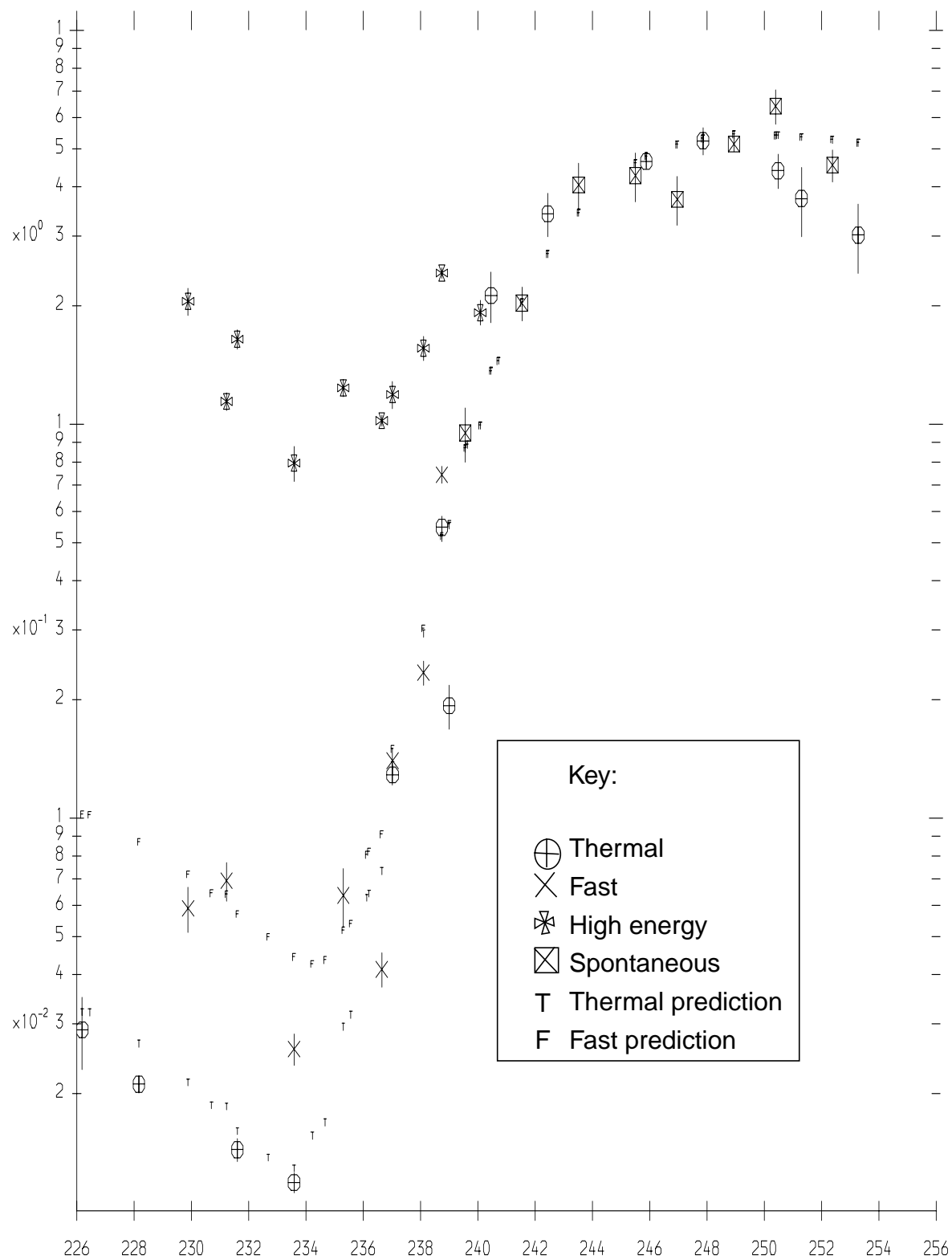


Figure 4.6: Experimental chain yields for mass 115 plotted against compound nucleus mass A_f minus $\bar{\nu}_p$

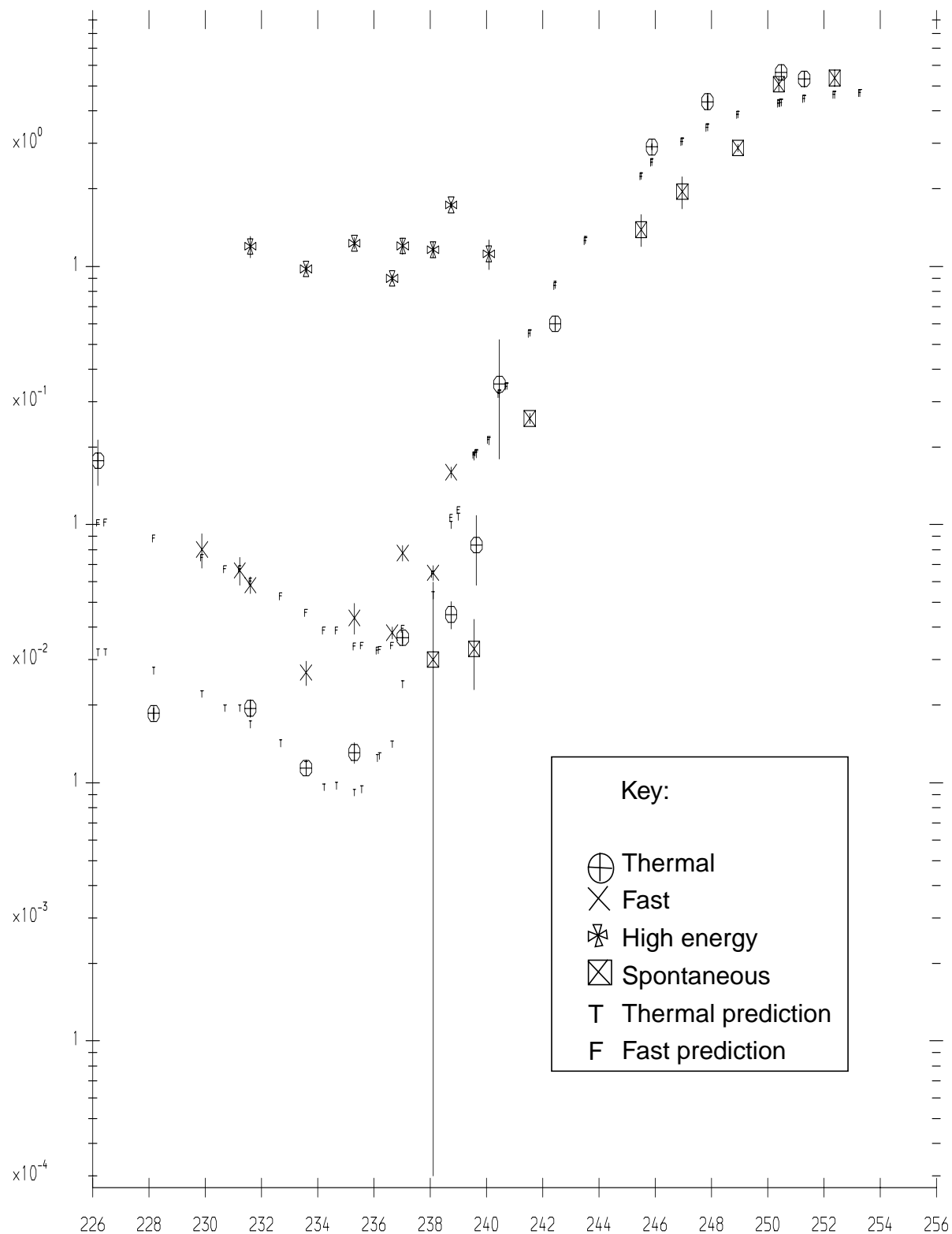


Figure 4.7: Experimental chain yields for mass 125 plotted against compound nucleus mass A_f minus $\bar{\nu}_p$

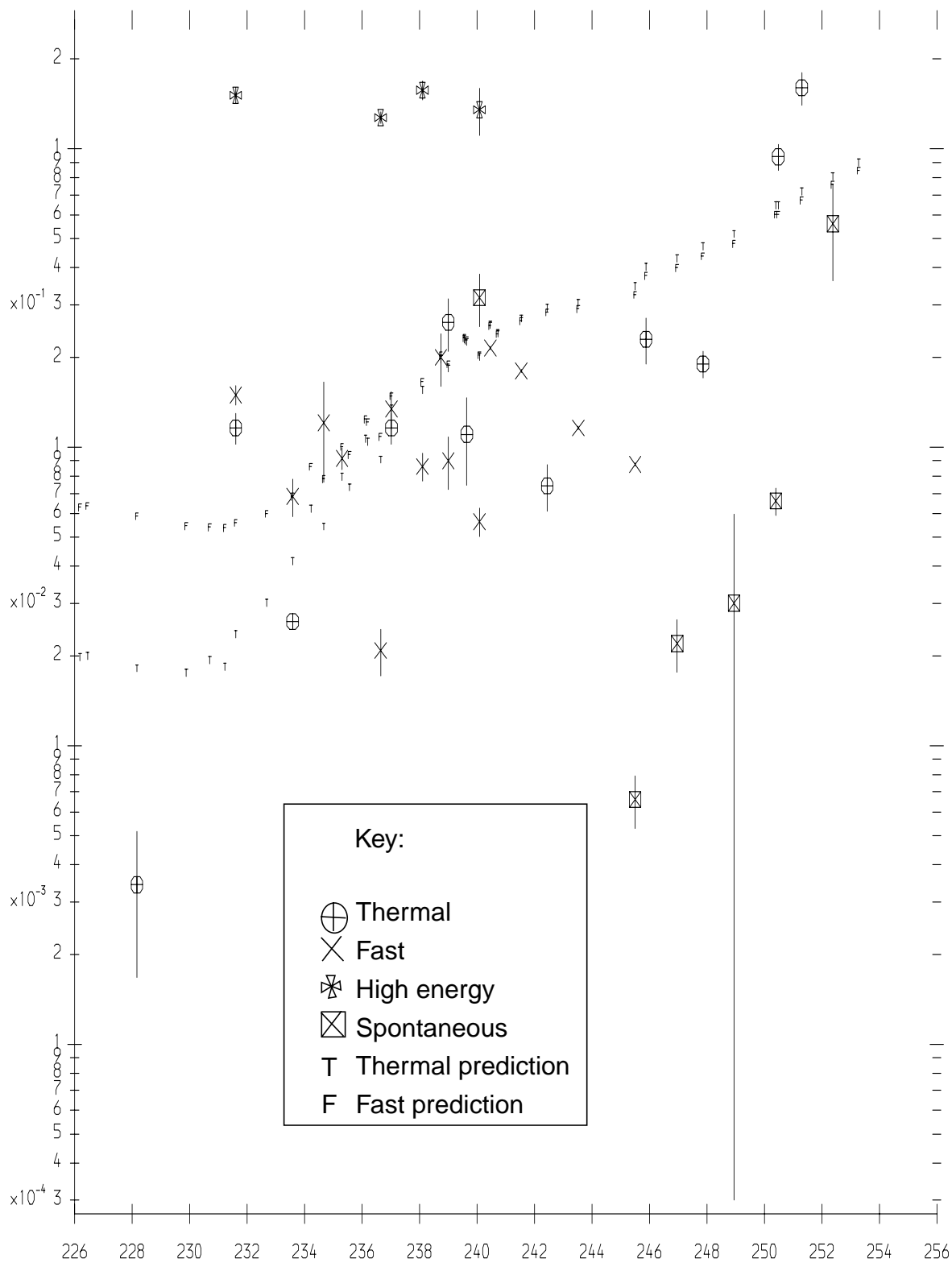


Figure 4.8: Experimental chain yields for mass 140 plotted against compound nucleus mass A_f minus $\bar{\nu}_p$

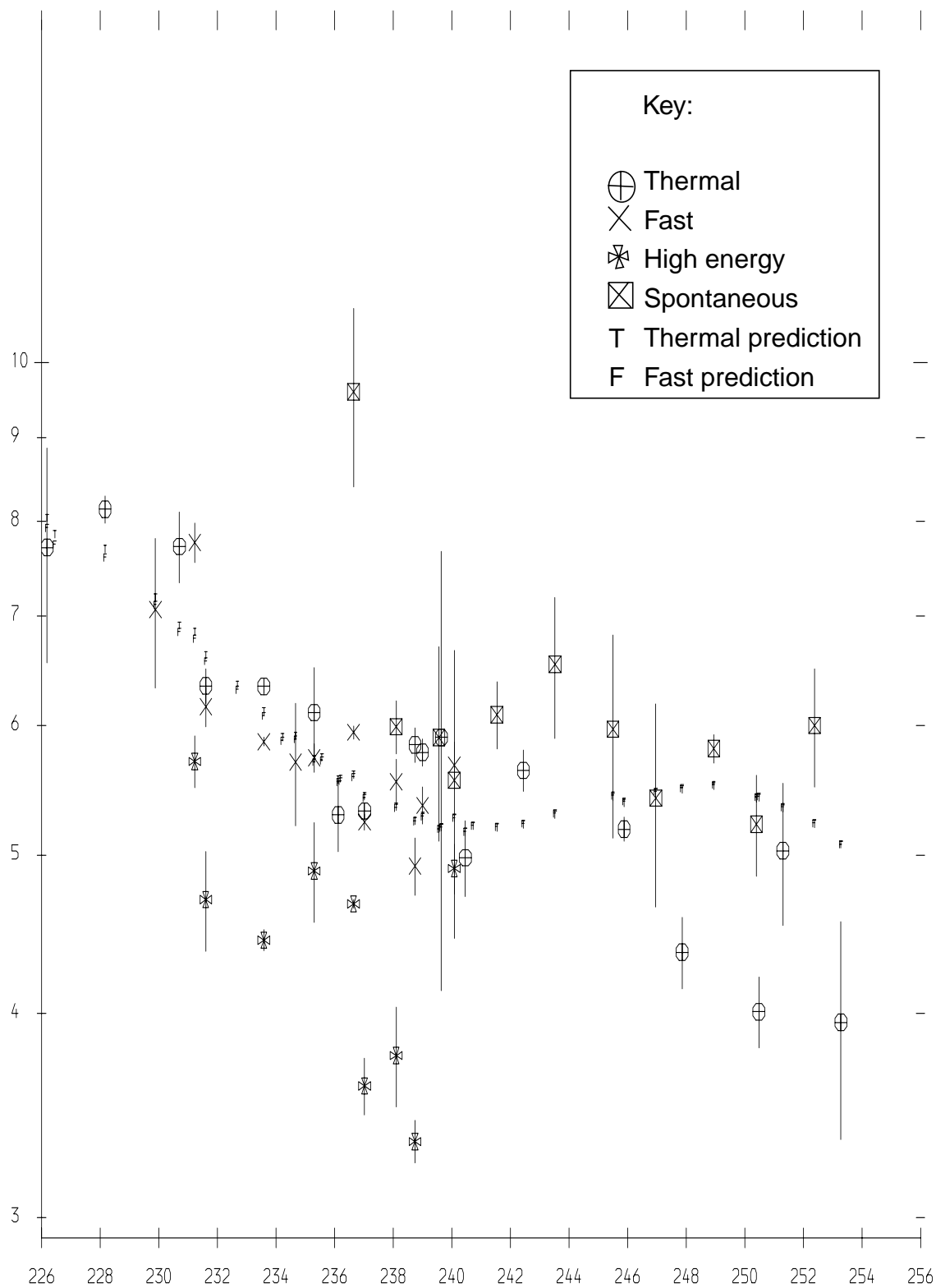
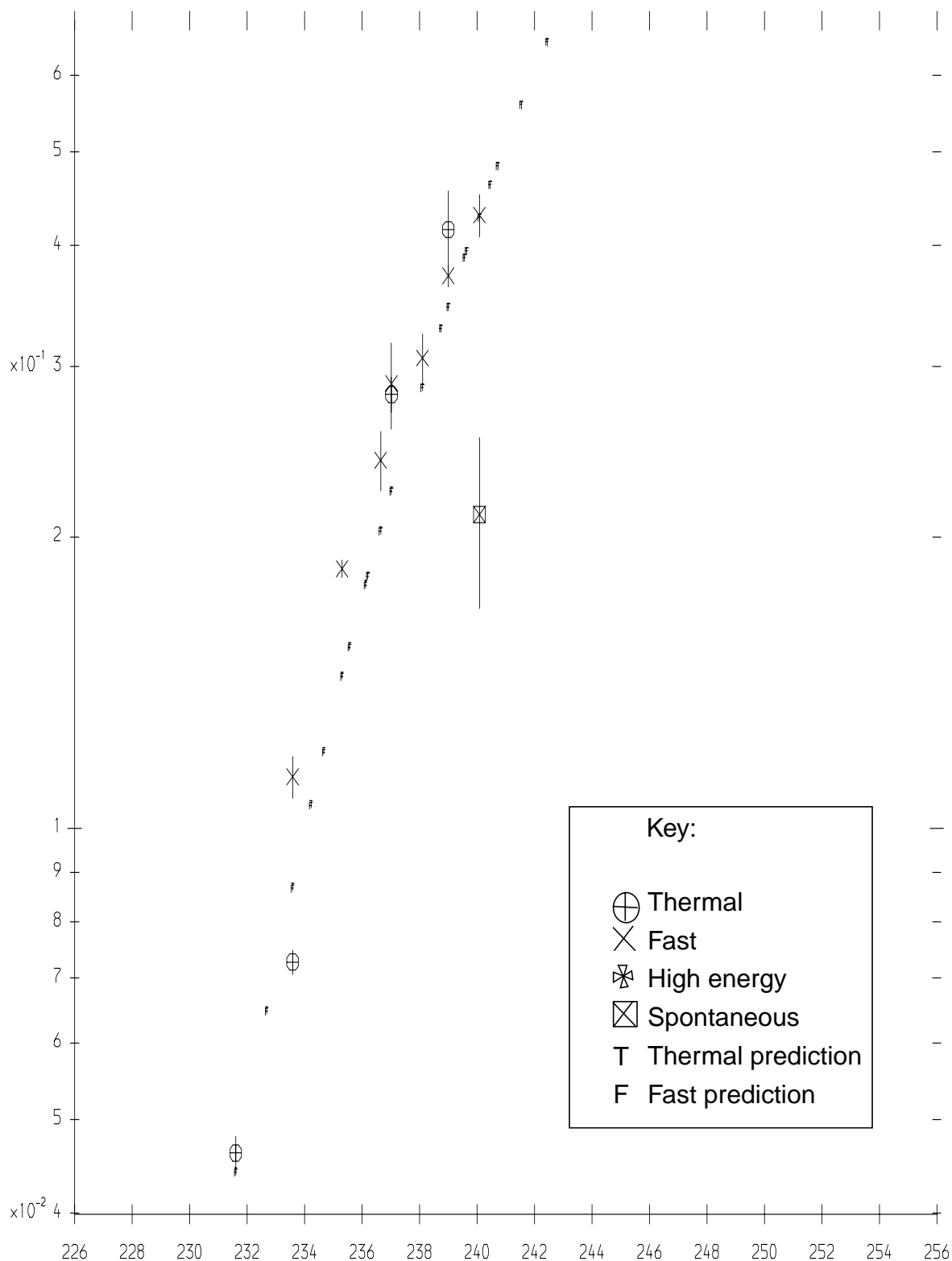


Figure 4.9: Experimental chain yields for mass 154 plotted against compound nucleus mass A_f minus $\bar{\nu}_p$



4.3 Fitting of experimental data to five Gaussian model

The five Gaussian model parameters described by Eqn (4.3) cannot be fitted to experimental data by linear least-squares techniques. Therefore a non-linear least-squares technique is required. In this thesis these model parameters were fitted using a FORTRAN subroutine published by Press et al^[4.16]. The subroutine is based upon the method described by Levenberg and Marquardt.

4.3.1 Fitting of the UKFY2 data

In previous work^[1.4] the UKFY2 recommended chain yields were fitted to the five Gaussian model. The fissioning systems for which results could be obtained are shown in Table 4.2.

Table 4.2: Parameters of the five Gaussian model fitted for the UKFY2 chain yields.

System	\bar{A}	N_1	σ_1	D_1	N_2	σ_2	D_2	σ_3
U233T	115.86	0.7116	4.230	24.63	0.2855	3.048	17.11	13.79
U235T	116.90	0.7158	4.298	24.02	0.2823	2.423	16.63	9.250
Pu239T	118.50	0.7100	5.587	21.34	0.2887	2.630	15.27	2.237
Th229T	114.03	0.7146	3.081	27.80	0.2832	2.335	21.73	11.22
Th232F	115.49	0.7079	3.522	26.45	0.2823	2.472	19.10	11.80
U235F	116.79	0.7081	4.516	23.76	0.2868	2.503	16.42	13.09
U238F	118.02	0.7102	5.031	22.85	0.2852	2.131	15.85	9.525
Th232H	114.65	0.6989	4.451	24.88	0.1164	4.264	18.78	11.17
U233H	115.12	0.5586	5.959	23.12	0.2190	5.243	19.27	11.78
U235H	116.01	0.6241	5.535	23.26	0.1824	3.208	16.00	11.99
U238H	117.42	0.6605	5.962	22.32	0.1921	2.938	15.81	11.80

These eleven systems cover the most important fissioning systems for applications (the neutron fission of ^{235}U , ^{238}U and ^{239}Pu). However the work described in section 8.3 shows that many more systems are required where high accuracy is required, especially for high burnup uranium oxide and mixed oxide fuels.

[4.16] "Numerical Recipes: The art of scientific computing", W.H. Press, B.P. Flannery, S.A. Teuolsky and W.T. Vetterling. Cambridge University Press (1986)

To extend the five Gaussian representation to systems with sparse data, the parameters in Table 4.2 were plotted against fissioning mass and charge, and fitted by linear or quadratic functions of A_f . No systematic trend with Z_f could be detected. The \bar{A} parameter showed a good agreement when approximated as half of the compound nucleus mass A_f . This agreement improved when the average number of prompt neutrons were subtracted from A_f . However the other parameters showed considerable scatter. A different technique was therefore required. For each parameter in turn, with the current best estimate of the functions of A_f defining the other parameters new five Gaussian model fits were made. The fitted parameter was then fitted to a linear or quadratic function of A_f . The process was then repeated for each parameter in turn. After all parameters had been fitted in this manner, the whole process was repeated. After two iterations the refitting procedure failed to produce any improvement in χ^2 . The predictions were then tested against measured data and, given that the data was not normally distributed, a guide to the uncertainty was estimated by examining the bounds that enclosed 66% of the distribution of the data about the prediction. This gave an estimate of the uncertainty as $\pm 30\%$ of the prediction.

The parameters developed by this procedure are given by the following functions:

$$\begin{aligned}\bar{A} &= \frac{A_f - \bar{\nu}_p}{2} \\ \sigma_1 &= 0.2017A_f - 42.906 \\ \sigma_2 &= 0.1125A_f - 24.375 \\ \sigma_3 &= 12.0 \\ N_1 &= 0.0003846A_f + 0.6215 \quad [\text{fast}] \\ N_1 &= 0.0010563A_f + 0.4579 \quad [\text{thermal}] \\ N_2 &= 0.286 \\ D_1 &= 27.1 - 0.67832(A_f - 230) + 0.013664(A_f - 230)^2 \\ D_2 &= 19.9 - 0.59500(A_f - 230) + 0.001250(A_f - 230)^2\end{aligned}$$

Figures 4.2 to 4.9 show experimental data and calculations for thermal and fast neutron fission using these functions. These predictions give good approximations of trends in the chain yield distributions for fast and thermal neutron induced fission. However they differ significantly from many measurements. This is a result of fitting the distributions to

smooth functions which cannot follow the fine structure; this fine structure does not follow an easily modelled pattern. Thus the smooth curves cannot be corrected to give a better estimate of the data.

4.3.2 Fitting of the UKFY3 data

Following the UKFY3 analysis the new chain yield data were fitted to the multiple Gaussian model. In section 4.2.2.1 above, a study was made of the approximation of $(1+2n)$ Gaussian distributions to model the UKFY3 chain yield distribution of the thermal neutron induced fission of ^{235}U . In the following this was repeated for all fissioning systems with more than twenty chain yield measurements. To fit the model successfully it is necessary to have data defining the valley region and at least one peak. Of the systems that could be successfully fitted, it was found that using more than five Gaussians did not improve the fits.

The effects of prompt and delayed neutrons on the distributions were also studied for the thermal fission of ^{235}U . The delayed neutron effect was examined by converting the chain yields to mass yields using the technique described by Eqn (8.7), in section 8.5. The prompt neutron effect was examined by shifting each chain yield in the distribution upward by the average number of neutrons, $\bar{\nu}_p(A)$, emitted by a fragment of mass A . The $\bar{\nu}_p(A)$ function used is described in section 6.2. The results of these calculations are shown in Table 4.1.

Table 4.3: Fitting of the chain yield distribution from the thermal neutron fission of ^{235}U with UKFY3 data correcting for prompt and delayed neutron emission.

Correction	χ^2	χ^2 per degree of freedom	r.m.s. fractional deviation	66% limit	Maximum deviation
no correction	3197.9	40.0	0.019	0.075	0.348
delayed neutron correction	3543.5	44.4	0.019	0.25	0.534
$\bar{\nu}_p(A)$ correction	51517.2	644.0	0.057	0.25	2.589
both	52801.6	660.0	0.060	0.25	2.211

These results show that the model best fits the chain yield distribution without correction. It is interesting that these “corrections” make the fits significantly worse. The prompt and

delayed neutron emission will smooth the yield distribution, thus reducing the fine structure on the distribution which the model cannot follow. Therefore correcting for these effects will make the fits worse. The simple fitting of the chain yield distribution to the model was thus used for predicting missing yields.

A further attempt to improve the model was made by not allowing the input standard deviations to fall below a minimum uncertainty. The use of the minimum uncertainty instead of the smaller, measured uncertainty reduces the weight given to these individual results. The table below shows the results of using three different cut-offs. The χ^2 values, which are dependent upon the uncertainties, are thus not a useful guide of the accuracy of the calculations. The goodness of fit parameters described above have therefore been used as a means of assessment.

Table 4.4: Fitting of the chain yield distribution from the thermal neutron fission of ^{235}U with UKFY3 data correcting for prompt and delayed neutron emission.

Minimum standard deviation as % of data value	χ^2	χ^2 per degree of freedom	r.m.s. fractional deviation	66% limit	Maximum deviation
0.0	3197.9	40.0	0.019	0.075	0.498
5.0	1149.2	14.4	0.019	0.075	0.498
10.0	287.5	3.6	0.019	0.075	0.498

The results show that the agreement between the fit and the experimental data is not altered by the application of a cut-off between zero and ten percent and thus there appears to be no incentive in using a cut-off during fitting.

The five Gaussian model was thus fitted to the UKFY3 experimental chain yield data with no correction or cut-off. The model was fitted to all fissioning systems with more than twenty data points; forty-seven such systems existed. However many had too few data to define all the parameters of the model. If, for a particular system, no data points existed in either the valley, peaks or wings then some of the parameters were unconstrained and the model could not be successfully fitted. Hence, only twenty-seven systems could be fitted to the model. The fitted parameters of these are shown in Table 4.5. The goodness of fit between the model and the data are shown in Table 4.6. The fit to the thermal neutron induced chain yield distribution for ^{235}U is shown in Figure 4.10.

Figure 4.10: Fit of chain yield distribution for the thermal neutron fission of ^{235}U

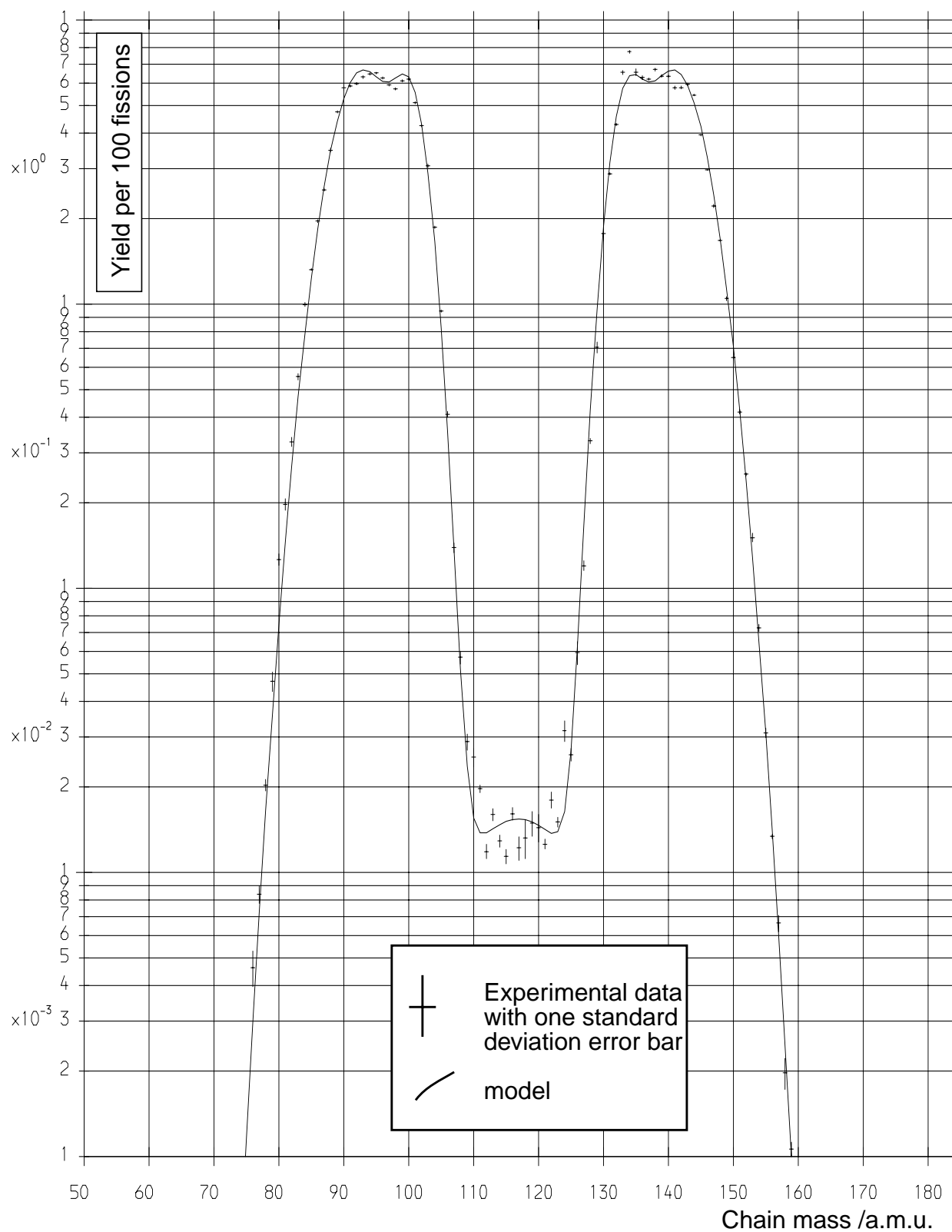


Table 4.5: Parameters of five Gaussian model fitted for UKFY3 data.

System	\bar{A}	σ_3	N_3	D_1	σ_1	N_1	D_2	σ_2
U232T	114.95	7.793	0.12348	25.622	3.3131	0.58928	18.165	2.5814
U233T	115.77	12.403	3.5518E-3	25.173	4.0843	0.63013	18.106	2.8934
U235T	116.90	9.2523	1.7926E-3	24.020	4.2980	0.71541	16.63	2.4233
Np237T	117.65	11.999	1.9580E-3	23.021	4.8979	0.71223	16.347	2.2646
Pu238T	118.07	14.013	5.7234E-2	22.344	4.3587	0.52996	15.465	2.5792
Pu239T	118.56	5.0556	2.6530E-3	22.019	5.4481	0.62909	15.529	2.8419
Th232F	115.55	12.583	1.1459E-2	25.777	3.7309	0.76299	18.748	2.3108
U233F	115.73	12.597	1.0323E-2	25.149	4.117	0.60318	18.054	3.2895
U235F	116.90	9.2473	4.8303E-3	24.02	4.2996	0.71242	16.629	2.4223
U236F	117.26	12.357	9.3219E-3	23.506	4.6746	0.69363	16.698	2.6646
U238F	118.25	11.091	2.0110E-3	22.573	5.0631	0.70937	15.923	2.3411
Np237F	117.62	5.0262	3.1789E-3	22.984	5.1300	0.68104	16.316	2.822
Pu239F	118.53	13.11	8.4215E-3	22.054	5.5834	0.59505	15.557	3.0172
Pu240F	118.98	11.908	5.4060E-3	21.687	5.5375	0.64734	15.205	2.7563
Am241F	119.41	18.042	1.0871E-2	21.271	6.1518	0.68763	14.821	3.0097
Th232H	114.63	17.959	0.26599	25.116	4.9097	0.64460	19.822	2.1401
U233H	115.06	8.7537	0.15569	24.879	6.0685	0.23376	20.061	5.7029
U235H	115.78	10.625	0.14799	23.901	5.722	0.43167	18.751	5.3988
U238H	117.29	11.605	0.14141	22.626	5.9625	0.63919	15.935	3.0685
Np237H	117.00	14.988	0.22453	22.93	5.8876	0.53814	16.800	5.0347
Pu239H	117.67	19.364	0.28772	22.256	6.5284	0.47125	14.868	3.7989
Pu240H	117.88	13.295	0.10671	21.765	6.6275	0.54892	14.996	4.4052
Pu242H	118.78	13.091	0.16488	20.819	6.3737	0.67228	14.811	2.3789
Am241H	118.32	12.168	0.26029	21.034	7.6984	0.52527	14.551	4.043

Table 4.6: Goodness of fits of UKFY3 data fitted to five Gaussian model.

System	Number of points	χ^2	χ^2 per degree of freedom	r.m.s. % deviation	third of maximum % deviation	66% limit
U232T	26	250.4	13.9	3.8	17.9	10.

Table 4.6: Goodness of fits of UKFY3 data fitted to five Gaussian model.

System	Number of points	χ^2	χ^2 per degree of freedom	r.m.s. % deviation	third of maximum % deviation	66% limit
U233T	74	6041.4	91.5	3.3	23.4	12.5
U235T	88	3197.9	40.0	1.9	16.6	7.5
Np237T	32	65.9	2.7	3.	21.3	7.5
Pu238T	32	142.3	5.9	3.1	19.9	7.5
Pu239T	78	1623.	23.2	2.1	19.4	7.5
Th232F	50	505.9	12.	3.6	37.8	10.
U233F	60	289.8	5.6	3.	30.8	7.5
U235F	62	2152.4	39.9	2.6	23.3	7.5
U236F	42	152.3	4.5	2.9	17.4	10.
U238F	67	1300.7	22.	5.	57.3	10.
Np237F	60	491.1	9.4	1.6	11.6	5.
Pu239F	65	766.8	13.5	2.3	21.4	7.5
Pu240F	66	672.3	11.6	2.6	30.4	5.
Am241F	45	369.6	10.	7.3	99.6	10.
Th232H	48	412.4	10.3	4.8	45.4	10.
U233H	44	360.	10.	4.2	31.8	10.
U235H	47	1333.	34.2	5.2	34.1	7.5
U238H	68	618.8	10.3	3.1	36.3	5.
Np237H	28	184.5	9.2	8.5	64.6	10.
Pu239H	26	70.2	3.9	3.3	15.6	7.5
Pu240H	47	364.5	9.3	3.8	28.1	10.
Pu242H	37	194.4	6.7	3.9	27.2	10.
Am241H	38	276.6	9.2	1.5	8.7	5.

Figure 4.10 shows that considerable structure exists in the valley and on the peaks of the

distribution. Interestingly, no structure can be seen in regions where the yield is rapidly rising or falling and the model fits the experimental data well in these regions.

A much larger number of fissioning systems have been fitted to the five Gaussian model with the UKFY3 data than was possible with the UKFY2 data. It is thus possible to predict the yield curves of many more systems with greater accuracy than is possible using the generalised five Gaussian parameters developed for UKFY2.

4.3.3 Generation of complete chain yield datasets

It is thus possible using the UKFY3 five Gaussian fits and the five Gaussian parameter functions developed for UKFY2 to produce complete sets of chain yields. However the fine structure in some regions produce considerable variation between the fit and the experimental data. To improve the fit, where experimental data is available, the data is used to normalise the edges of any gap and the log of the normalisation factor is linearly interpolated across the gap. Similarly, for the wings the highest and lowest mass chain yield measurement are used to normalise the yields above and below these yields.

The uncertainties of values based upon these predictions are, however, a problem as the differences between the model and the data are not normally distributed. Thus the r.m.s. percentage difference cannot be quoted as an overall one standard deviation uncertainty. The percentage uncertainty whose \pm envelope includes 66% of the experimental data was thus used as some form of estimate of the fractional variation of the fit from the data. These values varied from 5 to 12.5%. It was thus decided to use a value of 15% as an appropriate uncertainty for all the fitted systems. Similar comparisons of the UKFY2 predicted parameter calculations and experimental data showed the 66% envelope to be just less than $\pm 30\%$ and in that case the predictions were assigned an uncertainty of 30%.

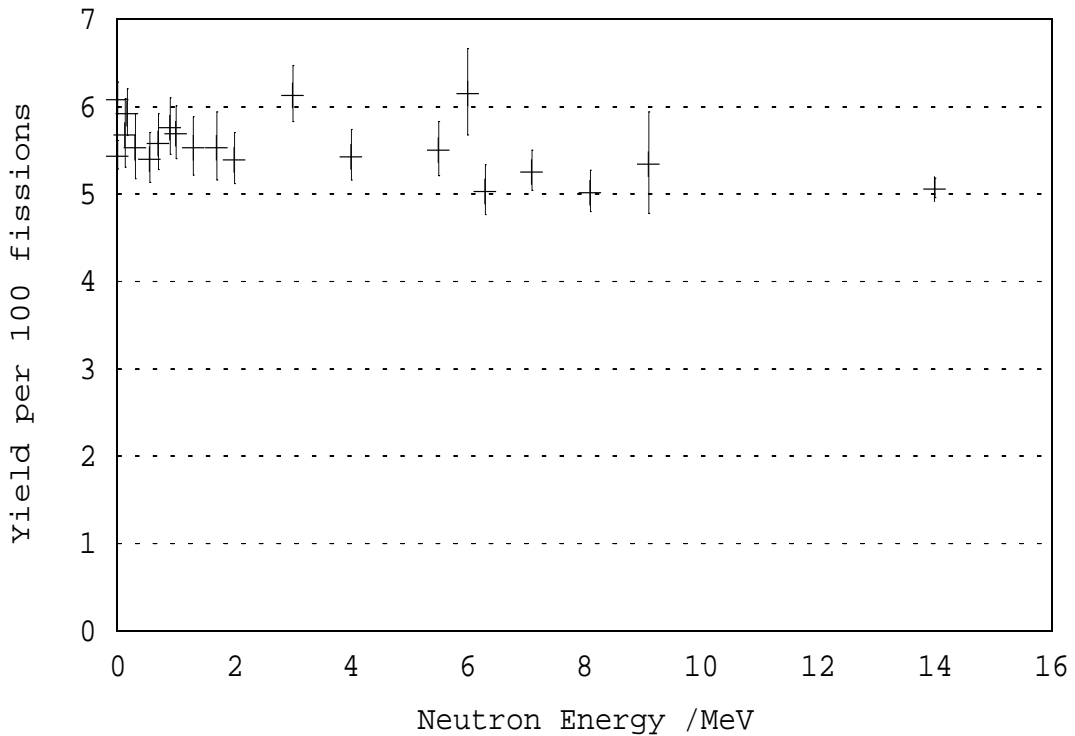
The main fissioning systems could be fitted with the UKFY3 data. Also it was felt unlikely that repeating with the UKFY3 data the fitting of five Gaussian parameters to functions of A_f , as in section 4.3.1, would significantly improve the results. Thus this form of analysis was not repeated and it was decided to use the UKFY2 predicted parameter calculations to fill gaps in fissioning systems that could not be fitted in the UKFY3 analysis.

4.4 Energy dependence of chain yield distributions

4.4.1 General observations

The only mass region where significant dependence of the chain yield on the energy of the incident neutron is in the valley between the high and low mass peaks. The valley yields increase with increasing excitation energy. The sum of all yields being equal to two thus requires the height of peaks to reduce in order to compensate for the increase in the valley region by falling slightly. However due to the large difference in the peak and valley yields even at large excitation energy the peaks are only slightly affected. This slight fall in peak height is just visible in Figure 4.11.

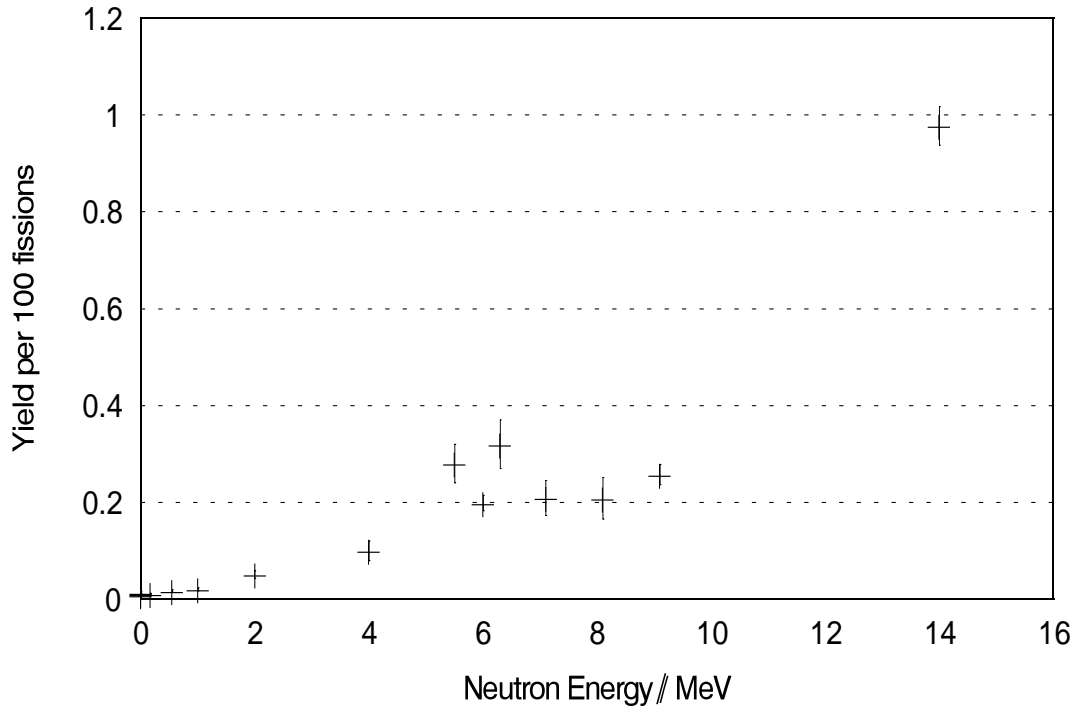
Figure 4.11: Variation of the mass 99 chain yield from ^{235}U with neutron energy



The rise of yields in the valley region is shown in Figure 4.12 where the ^{115}Cd yield is

seen to rise significantly with neutron energy.

Figure 4.12: Variation of the mass 115 chain yield from ^{235}U with neutron energy



This filling of the valley with increasing energy is a well known effect. The valley yields change slowly with changes of neutron energy over MeV. However there has been some experimental work which has suggested that in the resolved resonance region the yield distribution can vary considerably over changes of neutron energy of the order of eV.

4.4.2 Investigation of possible energy dependence of fission product yields in the resolved resonance region

4.4.2.1 Experimental data

There have been several experimental studies that suggest the chain yield distribution varies significantly for small changes in neutron energy. The first published work in this area was by the Los Alamos Radiochemistry Group^[4.17]. Here two ^{235}U samples were wrapped in different thicknesses of cadmium and, after irradiation, the ratio of activity of various nuclides relative to ^{99}Mo were measured. The different thicknesses of cadmium did not significantly change the measured ratios. These ratios were then divided by the

[4.17] Phys. Rev. 107, 325. Los Alamos Radiochemistry Group (1957)

ratios measured for thermal neutron induced fission. These ratio of ratio results are shown in Table 4.7. Of the nuclides measured only ^{115}Cd and ^{112}Pd , yields in the valley, showed significant changes from the thermal neutron case. However, all nuclides in the valley region have lower yields than from thermal fission. It should be noted that Figure 4.12 above shows an increase in yield with increasing energy.

Table 4.7: Ratio of epi-thermal to thermal results for activities of fission products measured relative to ^{99}Mo

Fission product	Ratio of ratio results	
	set 1	set 2
^{97}Zr	1.00 ± 0.10	0.98 ± 0.10
^{109}Pd	0.98 ± 0.10	1.00 ± 0.10
^{111}Ag	0.89 ± 0.10	0.92 ± 0.10
^{112}Pd	0.85 ± 0.10	0.86 ± 0.10
^{115}Cd	0.84 ± 0.10	0.83 ± 0.10
^{136}Cs	0.98 ± 0.10	0.96 ± 0.10

Measurements carried out by Nasuhoglu et al [4.18] used a crystal spectrometer to produce monoenergetic neutron beams between 1 and 10 eV. The neutron spectra had an energy spread (full-width at half-maximum) of 0.053eV at 1 eV and 0.15eV at 9eV. The beams were used to irradiate a ^{235}U sample. The activity ratios of ^{111}Ag , ^{115}Cd and ^{127}Sb were measured relative to ^{89}Sr . These ratios were then divided by the activity ratio for thermal neutron induced fission. However these differences were not significant when their experimental uncertainty is considered. These results are shown in Table 4.8.

[4.18]Phys. Rev. 108, 1522. R.Nasuhoglu, G.R.Ringo, L.E.Glendenin and E.P.Steinberg (1957).

Table 4.8: Ratio of monoenergetic to thermal neutron induced fission yields measured relative to ^{89}Sr

Fission Product	Neutron Energy /eV		
	1.1	3.1	9.5
^{111}Ag	1.11 ± 0.20	1.06 ± 0.20	1.00 ± 0.20
^{115}Cd	1.18 ± 0.20	0.73 ± 0.20	0.91 ± 0.20
^{127}Sb	1.10 ± 0.20	no data	no data

There appears to be a slight drop of the $^{115}\text{Cd}/^{89}\text{Sr}$ yield ratio at 3.1 eV however these results were inconclusive due to the large counting uncertainties. This was a result of the low neutron fluxes and thus low fission rates generated in the experiments.

In the early 1960s an alternative high flux source was used to study these resonance effects. The technique involved using a thin annulus of fissile material attached to a backing disc rotating at high speed. An atomic bomb was detonated around 200 metres from the disc. The neutrons travelled through a tunnel in the rock from the explosion to the rotating disc. The beam being collimated by a slit at the disc.

The neutron time of flight from the explosion to the disc is determined by the neutron velocity and thus the energy of the neutrons. Thus, as the disc rotated, the energy of neutrons reaching the disc was reduced. The gamma pulse from the explosion, travelling at the speed of light, produced a burst of photo-fission on the disc which was used as a time marker. Thus given the distance of the explosion from the disc, the speed of light, the angular rotation of the disc from the gamma fission mark and the rotational speed it was possible to determine the neutron energy that irradiated a position on the annulus.

The beam was cut-off by a shutter after approximately one half revolution of the disc after the explosion so that lower energy neutrons from the explosion did not re-expose parts of the disc during the second and subsequent revolutions.

After the irradiation the annulus was cut into thin radial slices. From the distance around the rim it was possible to determine the neutron energy at the start and end of the slice.

The ^{115}Cd and ^{99}Mo activities were then measured for each slice. Thus a mean activity ratio was obtained for a series of energy regions.

Several experiments of this type were performed during the 1960s. Samples of both ^{235}U and ^{239}Pu were used. The measurements were reported by Cowan et al for ^{235}U [4.19][4.20][4.21] and ^{239}Pu [4.22]. These experiments covered in total a range of neutron energy from 19.33 to 86.3eV for ^{235}U and 15.8 to 204 eV for ^{239}Pu . The result of these measurements are shown in Figure 4.13 and Figure 4.14. The error bars shown are the measurers' estimate of one standard deviation error. The width of the error bars give the neutron energy range which irradiated the measured sample slice.

These results show significant variation from the thermal values. However study of these results by Cowan et al could not determine if properties of the resonances could explain these differences. They tried to associate the ratio to the resonance spin assignments. The ^{239}Pu data showed a correlation with the resonance spin assignments but this was at the level of the uncertainty on the fit. It was not possible to produce a similar correlation for ^{235}U . They suggested that the inability to correlate the ^{235}U data with spin assignment may be due to multiple channels for each spin, each channel having a characteristic yield distribution.

[4.19] Phys. Rev. 122, 1286. G.A.Cowan, A.Turkevich, C.I.Browne and the Los Alamos Radiochemistry Group (1960)

[4.20] Phys. Rev. 130, 2380. G.A.Cowan, B.P.Bayhurst and R.J. Prestwood (1963)

[4.21] Phys. Rev. C 2, 615. G.A.Cowan, B.P.Bayhurst, R.J. Prestwood, J.S. Gilmore and G.W. Knobeloch (1970)

[4.22] Phys. Rev. 144, 979. G.A.Cowan, B.P.Bayhurst, R.J. Prestwood, J.S. Gilmore and G.W. Knobeloch (1965)

Figure 4.13: Ratio of ^{115}Cd to ^{99}Mo activity ratio for ^{235}U relative to the thermal neutron induced value.

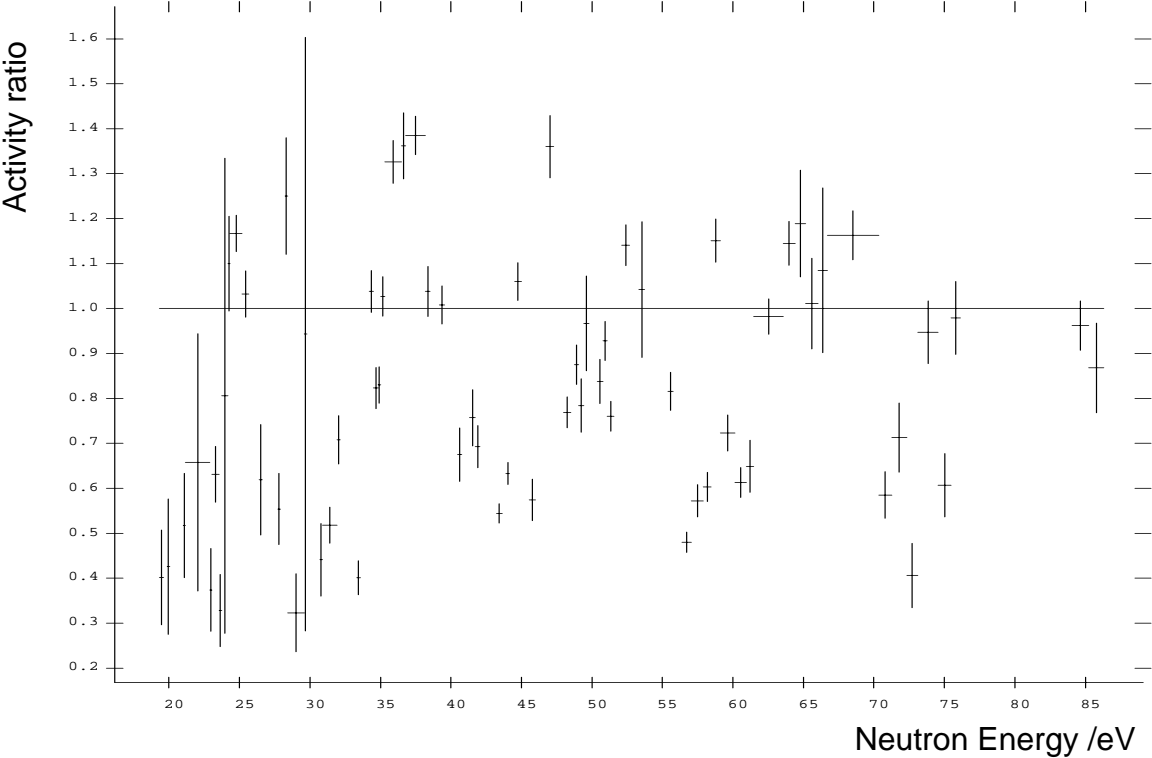
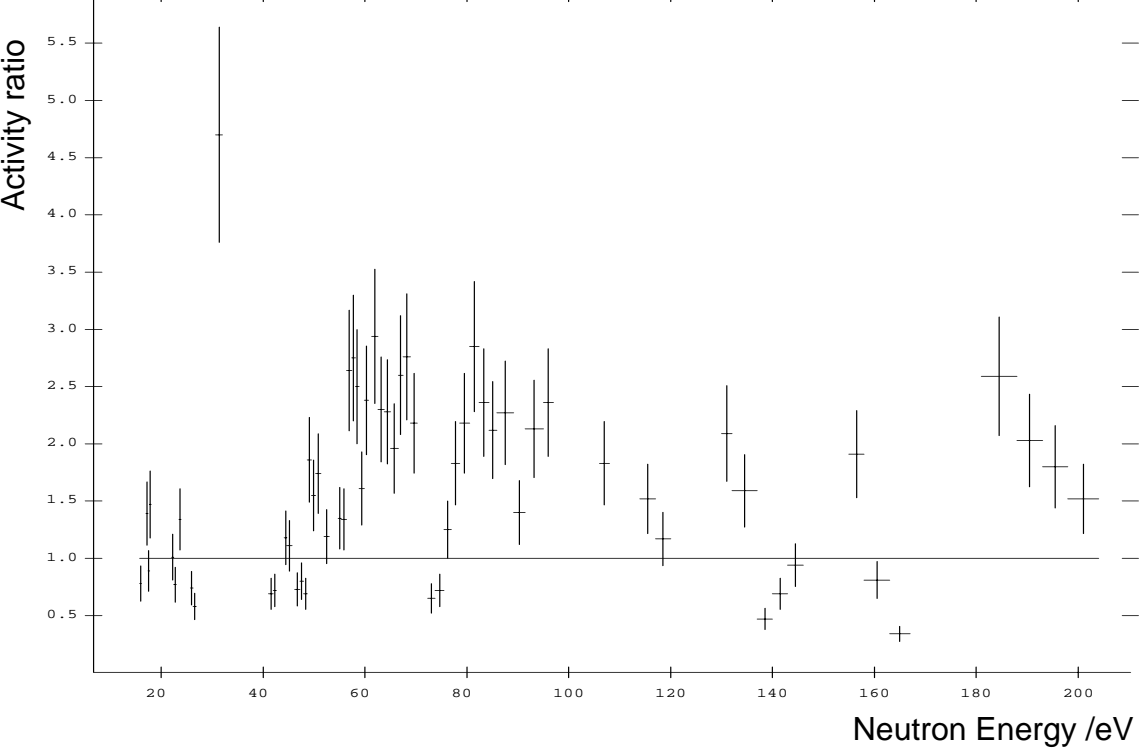


Figure 4.14: Ratio of ^{115}Cd to ^{99}Mo activity ratio for ^{239}Pu relative to the thermal neutron induced value.



4.4.2.2 The Reich-Moore formalism to describe resonance fission

The Reich-Moore formalism^[4.23] is used to describe the shape of neutron cross-section resonances in the energy region where resonance shape can be determined. This formalism describes each resonance by the resonance neutron energy, the total angular momentum of the resonance, the neutron width, the capture width and two fission widths. This model considers there to be two possible results of neutron capture: either gamma de-excitation of the nucleus or fission. The work of Farrell^[4.24] showed that after a neutron enters the nucleus to form a compound nucleus there are many possible final states resulting in neutron capture but only two resulting in fission. Thus it is possible to model the capture statistically but the fission states must be modelled separately. These fission states are channels through which fission must proceed.

For ^{235}U the neutron absorption can leave a compound nucleus with a spin of 3 or 4. The probability of fission is split into two channels, usually defined as A and B, for each of the two spins. Similarly, for ^{239}Pu , compound nuclei with spins of 0 and 1 can be formed, but the spin 1 state has only one fission channel.

The use of these different routes to fission is similar to that suggested by Cowan, and thus it was decided to test whether the Cowan data was consistent with each of the spins and Reich-Moore channel combinations having different yield distributions. Using the NJOY code version 89^[4.25] the resonance parameters files for ^{235}U and ^{239}Pu from both JEF2.2 and ENDF/B-VI were processed to produce a series of partial cross-sections for each spin state and channel. It was necessary to modify the code to write out each of the partial cross-sections before they were combined into a single fission cross-section. These were then condensed to the energy groups defined by the Cowan et al experiments. To condense the cross-sections a constant flux was assumed in each energy region. This is based upon experimental measurements made by Cowan et al which showed the neutron flux was constant in the range of energies where their

[4.23] Phys. Rev. 111, 929. C.W.Reich and M.S. Moore (1968)

[4.24] Phys. Rev. 165, 1371. J.A. Farrell (1968)

[4.25] Laboratory report from Los Alamos, U.S. Report number LA-UR 89-2057, "Introducing NJOY89" by R.E.MacFarlane (1989)

measurements were made. This resulted in a set of four grouped partial fission cross-sections for ^{235}U (3A, 3B, 4A and 4B) and similarly three partial cross-sections for ^{239}Pu (0A, 0B, 1A).

If each of these routes give rise to a different fission yield distribution then the combined distribution is the weighted mean of each distribution. The distributions being weighted by the partial cross-sections. The mean ^{115}Cd to ^{99}Mo activity ratio, \bar{R} , in any energy region would thus be given by:

$$\bar{R} = \frac{\sum_i \sigma_i R_i}{\sum_i \sigma_i} \quad \text{Eqn (4.4)}$$

where σ_i is the partial cross-section for each of the i routes in the energy region.

4.4.2.3 Fitting of the Reich-Moore channels to the resonance yield data

The experimental values of \bar{R} were fitted to Eqn (4.4) using the σ_i values produced by the NJOY code to produce values of R_i .

The results of this fitting for the two ^{235}U evaluated files are shown in Table 4.9. These results show that the R_i values are not significantly different for the different partial cross-sections. Also the different evaluated files do not produce significantly different results. However, this is a result of the same resonance parameter analysis being used by both files. That analysis was based upon the work by Derrien et al [4.26], with minor changes introduced to the JEF2.2 file in order to be consistent with some more recent measurements.

[4.26] International conference Nuclear Data for Science and Technology, May 30-June 3, 1988, Mito, Japan. H.Derrien, G. de Saussure, N.M.Larson, L.C. Leal and R.B.Perez "R-Matrix Analyses of the ^{235}U and ^{239}Pu neutron Cross Sections", p 83-86. (1988)

Table 4.9: Fitted activity ratios for each of the partial cross-section for ^{235}U

U235	χ^2 per degrees of freedom	^{115}Cd to ^{99}Mo activity ratio, R_i for each route			
		3A	4A	3B	4B
JEF2.2	26.42	0.87 ± 0.10	0.86 ± 0.15	0.84 ± 0.14	0.51 ± 0.24
ENDF/B-VI	26.18	0.86 ± 0.10	0.92 ± 0.15	0.84 ± 0.14	0.48 ± 0.26

The large χ^2 per degrees of freedom shows that a poor fit is obtained. Attempts to use different initial estimates of the R_i values did not alter the results. A plot of measured against calculated results of this fit, shown in Figure 4.15, shows a poor fit.

Using similar techniques, the ^{239}Pu results are shown in Table 4.10. These results do show a significant change in R_i for the channel A of the low spin state. However, the large χ^2 per degrees of freedom and the scatter plot shown in Figure 4.16 show overall a relatively poor fit to the data. As with ^{235}U the JEF2.2 resonance parameters are taken from ENDF/B-VI with modifications to allow for new experiments.

Table 4.10: Fitted activity ratios for each of the partial cross-section for ^{239}Pu

PU239	χ^2 per degrees of freedom	^{115}Cd to ^{99}Mo activity ratio, R_i for each route		
		0A	1A	0B
JEF2.2	5.93	1.42 ± 0.12	0.74 ± 0.12	0.64 ± 0.36
ENDF/B-VI	5.92	1.43 ± 0.12	0.874 ± 0.12	0.65 ± 0.36

The scatter plots appear to have some structure which suggests that a real effects may be being masked by discrepant data. The A and B channel widths are determined by the SAMMY code. This code fits all available experimental cross-section data to produce a best estimate of the cross-sections, not the resonance parameters. The resonance parameter widths used to produce the cross-section may not be accurately determined for each resonance. Thus some of the partial cross-sections used in the fitting may not have any physical justification. This may introduce unnecessary discrepancies into the

fitting. However due to the nature of the determination of the resonance parameters and the group partial cross-sections it is not possible to fit a selected set of the experimental data for which the channel widths are most accurately determined.

More recently, work by Hambsch^[4.10] has shown similar effects to that produced by Cowan et al. The Hambsch work used a high flux reactor and a fission product mass separator to study these effects. Although this new work cannot be directly compared with the Cowan work the measurement of changes in fragment yields and their kinetic energy suggests that a real physical phenomena is being observed.

The uncertainties and inconsistencies in the fission yields in the resolved resonance region demonstrates that is an area where both experimental and theoretical work is still required before any clear picture can be obtained of the systematics.

Figure 4.15: Scatter plot of experimental and fitted activity ratios for ^{235}U .

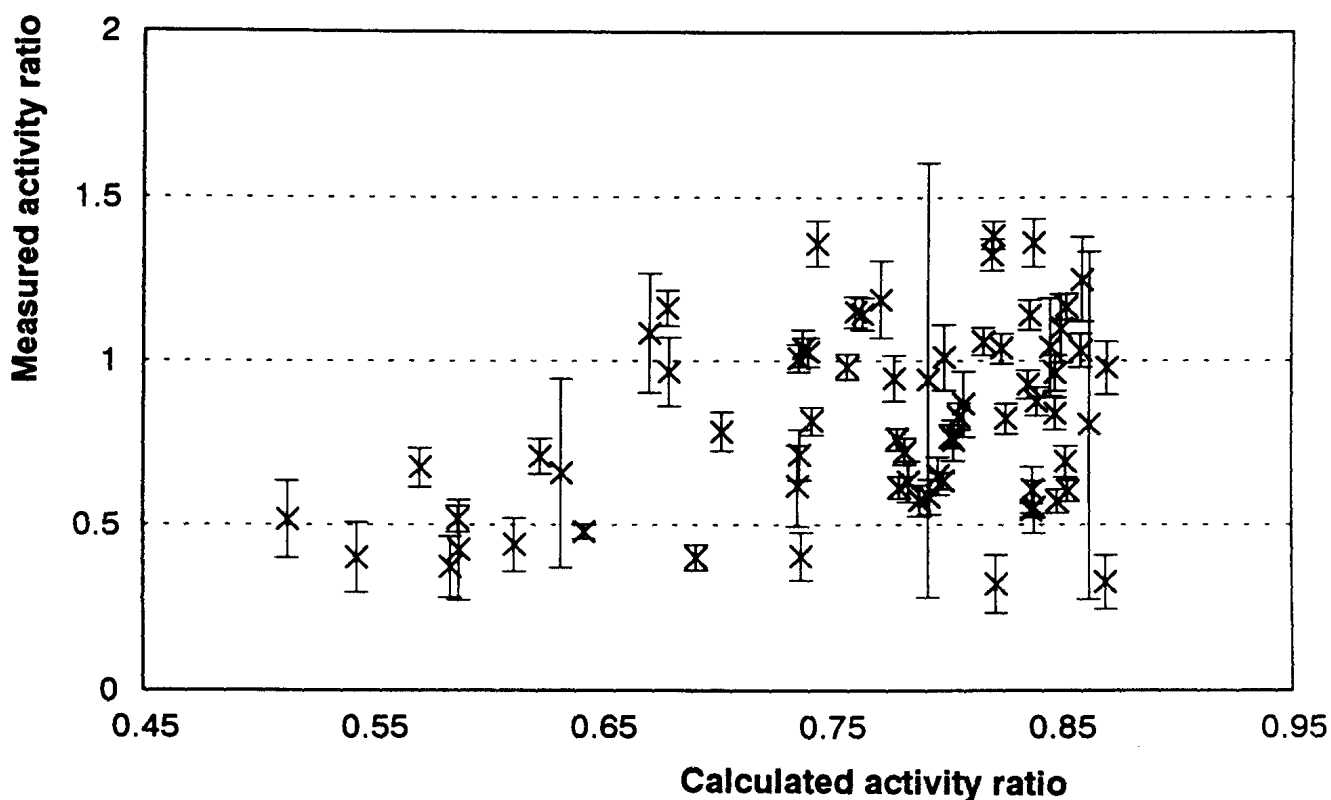
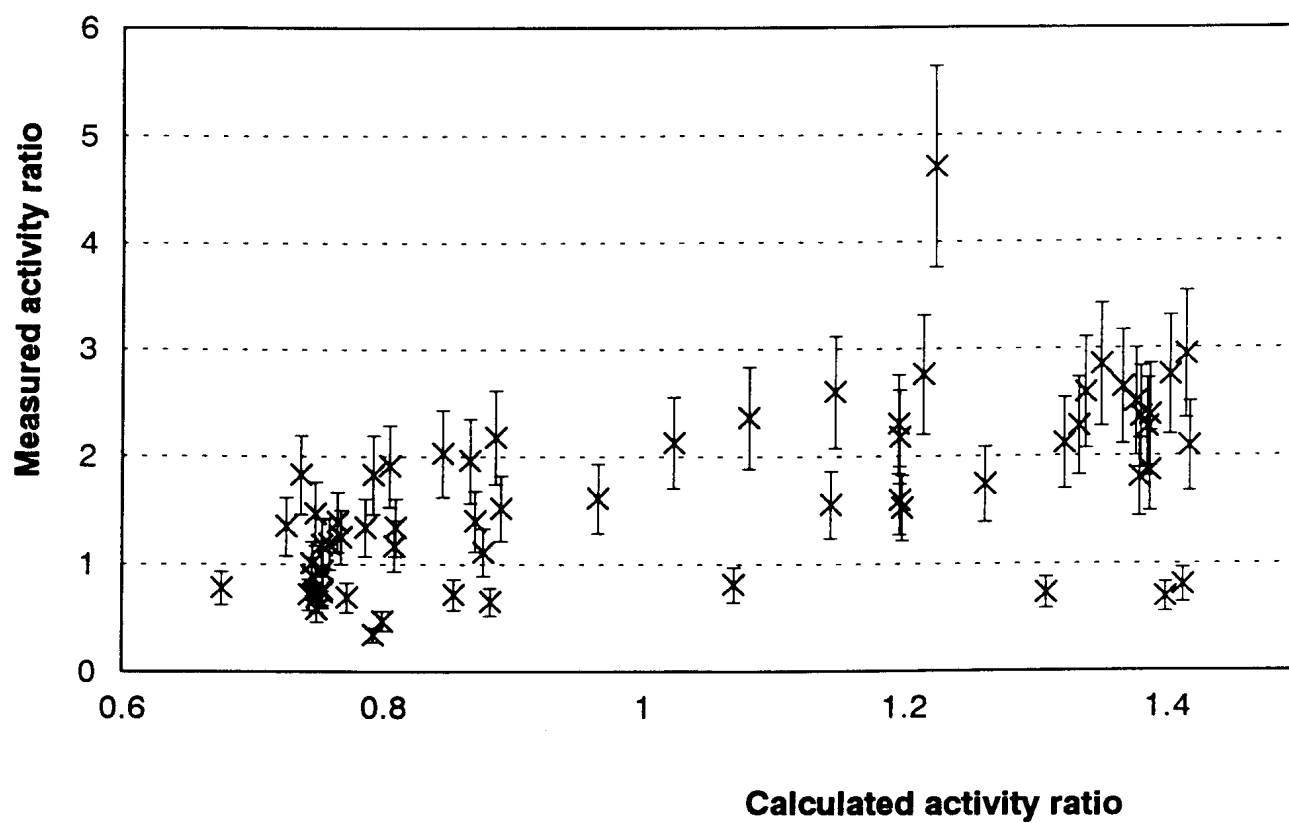


Figure 4.16: Scatter plot of experimental and fitted activity ratios for ^{239}Pu .



5. Light Charged Particle Fission Product Yields

5.1 Introduction

During fission there is a probability of producing a light charged particle, for example an alpha particle or a triton, as well as the two main fragments and neutrons. This emission occurs in less than one in a hundred fissions. The process is sometimes called ternary fission as a third fragment is produced.

Since the discovery, in 1946, of the emission of light charged particles during fission this process has been extensively studied and reviewed^{[5.1] [5.2]}. From measurements of the angular distribution of the particles to the light fragment direction by several groups including Guet et al^[5.3] it was observed that the alpha particles were peaked at $81.3^\circ \pm 0.5^\circ$ with a full width half maximum of $18.5^\circ \pm 0.8^\circ$. Guet et al noted that their measurements agreed well with other measurements for ^{235}U and measurements of the spontaneous fission of ^{252}Cf , which is a surprising result given the different fission mode and very different nucleus. The experimental evidence suggests that the particles are formed between the two main fragments very close in time to the scission of the compound nucleus and before the fragments have separated significantly by Coulombic repulsion. Thus the alpha particles are repelled by the fragments away from the axis upon which the fission products are being accelerated.

Most experimental studies of ternary fission are concerned with determining properties of the compound nucleus at scission by studying the light charged particle. These measurements, however, cannot usually be used to determine yields. On the other hand the yields of these ternary particles are important in reactors, giving rise mainly to hydrogen and helium isotopes. The tritium, ^3H , produced from fission is a β emitter with a half-life of 12.33 ± 0.06 years^[1.8] which, if it comes into contact, can be easily absorbed

[5.1] "Nuclear Fission" by R.Vandenbosch and J.R. Huizenga, Academic Press, ISBN 0-12-710850-5 (1973)

[5.2] "The Nuclear Fission Process" by C.Wagemans, CRC Press (1992)

[5.3] Nuclear Physics A314 1-26 "A detailed investigation of the thermal neutron fission of ^{235}U " by C.Guet, C.Signarbieux, P.Perrin, H.Nifenecker, M.Asghar, F.Caïtucolli and B.Leroux (1979)

by living tissue. The tritium fission yield is thus important for calculations concerned with handling and reprocessing of irradiated fuels, and for modelling of accident scenarios. These requirements have led to many measurements of such yields, primarily of ^4He and ^3H . The ^4He is not of itself significant but is used as a standard yield for tritium measurements.

The measurements can be of two types: radiochemical measurements of a sample after irradiation or measurements of the number and parameters (energy, nuclear charge or mass) of the long ranged emitted particles. It should be noted that the second type of measurement can be achieved by several techniques. One of these is to measure the particle kinetic energy as the coulombic repulsion is different for hydrogen (1 proton) and helium (2 protons) as the acceleration depends on the charge to mass ratio. The energy distributions of the different particles considerably overlap. Thus the considerably larger alpha peak has to be modelled and then subtracted to estimate the other particles. However work by D'Hondt et al [5.4] and Caïtucoli et al [5.5] showed that the low energy tail of the alpha particle spectrum deviated significantly from a previously assumed Gaussian distribution. This means that measurements made of low probability yields where the alpha spectrum tail has been assumed to be Gaussian, and has been subtracted are invalid; this covers for example, many measurements involving tritium.

An improved technique uses two detectors, one being very thin and absorbing only part of the particle's energy and the other absorbing the remaining energy. From the energy loss in the thin detector and the total energy the charge of the particle can be determined. This technique usually plots the energy loss against total energy; areas can then be defined where the particles charge and mass are uniquely defined. Thus the yield for a given mass and charge can be determined. This technique can measure yields of tritium and other nuclides relative to the alpha yield.

[5.4] "Study of alpha particles produced in thermal neutron induced reactions on ^{235}U "
P.D'Hondt, A. De Clerq, A. Deruytter, C. Wagemans, M. Asghar and A. Emsallem, Nucl.
Phys. A303 (1978)

[5.5] "Investigation of the low energy part of the alpha spectrum", F. Caïtucoli, B. Leroux,
G. Barreau, N. Cârjan, T. Benfoughal, T. Doan, F. El Hage, A. Sicre, M. Asghar, P. Perrin
and G. Siegert, Z. Phys. A298, (1980).

Several models have been used to explain some of the properties of the ternary particles. Halpern^[5.6] suggested that the particle is produced by a sudden snap back of the stubs of the scissioned neck directly following scission. Cârjan^[5.7] considered the alphas to be produced from the alpha decay of the compound nucleus as it approached scission. Other authors, including Rubchenya and Yavshits^[5.8] have extended the work of Brosa and Grossman described in chapter 4 to consider the ternary emission as a simultaneous splitting of the neck at two points giving rise to the ternary particles. Although these models can estimate the energies and angular distribution of the ternary particles they cannot determine the probability of emission required for applications.

The evaluation of ternary yields thus relies upon the analysis of measurements from which empirical models can be used to extend the measurements to other fissioning systems.

Evaluations of ternary yields have been produced in the recent UK evaluations^{[1.4], [1.5]} and the work of Madland and Stewart^[5.9]. The results for alpha yields are shown in Table 5.1 for the four main thermal neutron reactor fissile fuel nuclides. The alpha yields are typically measured by identification of particles directly resulting from fission due to the difficulties of measuring helium because many other routes of production exist and the nuclide does not undergo radioactive decay.

[5.6]Proc. IAEA Symp. Phys. Chem. Fission, Salzburg, p369 (1965)

[5.7] "Sur l'origine des alphas de scission", N.Cârjan. J. Phys. (Paris) 37, 1279 (1976).

[5.8] "Dynamic treatment of ternary fission" V.Rubchenya and S.Yavshits Z.Phys. A329, 217 (1988).

[5.9] "Light ternary fission products: probabilities and charge distributions", D.G.Madland and L.Stewart, Report LA-6783-MS (also ENDF-247) (1977)

Table 5.1: The thermal neutron fission yields of Helium-4 from recent evaluations^a

Nuclide	UKFY3 (1993)	UKFY2 (1990)	UKFY1 (1986)	ENDF-247 (1977)
U233	0.2065 (4.1%) [9]	0.2397 (1.4%) [7]	0.2072	0.2268 (3.9%)
U235	0.1699 (3.6%) [12]	0.1882 (1.6%) [13]	0.1680	0.1950 (9.2%)
Pu239	0.2080 (3.3%) [8]	0.2232 (1.1%) [8]	0.2148	0.2326 ^b (4.6%)
Pu241	0.2015 (10.0%) [2]	0.1938 (11.0%) [2]	0.1860	2.273 ^c (6.4%)

a. Estimate of standard deviation given in () and number of analyzed experimental measurements in [].

b. Estimate of total light charged particle emission, not only alpha particle yield.

c. Estimate of total light charged particle emission, not only alpha particle yield.

The tritium fission yields corresponding with the set given in Table 5.1 are shown in Table 5.2. It should be noted that tritium yields can be measured radiochemically by the tritium gas produced in an irradiated sample or by the identification of particles resulting from directly from fission.

Table 5.2: The thermal neutron fission yields of Tritium from recent evaluations^a

Nuclide	UKFY3 (1993)	UKFY2 (1990)	UKFY1 (1986)	ENDF-247 (1977)
U233	0.009691 (24.3%) [4]	0.01006 (6.9%) [3]	0.01030	0.01043 (20%)
U235	0.009314 (3.8%) [15]	0.01004 (2.0%) [14]	0.01084	0.01219 (25%)
Pu239	0.01442 (5.3%) [5]	0.01471 (2.2%) [5]	0.01479	no value reported
Pu241	0.01410 (10.0%) [1]	0.01410 (4.3%) [1]	0.01410	no value reported

a. One standard deviation given in () and number of experimental measurements in [].

To fill the gaps in the measured yields it is necessary to understand how the ternary yields vary for different fissioning systems and different incident neutron energies.

5.2 Effects of incident neutron energy on the light charged particle yields

The recommended UKFY3 yields for the three systems with most information on the variation of yields with neutron energy are shown in Table 5.3 and Table 5.4 for alpha and tritium yields respectively.

Table 5.3: Alpha yields from UKFY3

Nuclide	Thermal	Fast (~0.6 MeV)	High (14MeV)
U233	$0.2065 \pm 4.1\%$	$0.2003 \pm 10.8\%$	$0.1980 \pm 10.6\%$
U235	$0.1699 \pm 3.6\%$	$0.1980 \pm 8.6\%$	$0.1667 \pm 5.3\%$
Pu239	$0.2080 \pm 3.3\%$	$0.2029 \pm 8.7\%$	no measured data

Table 5.4: Tritium yields from UKFY3

Nuclide	Thermal	Fast (~0.6 MeV)	High (14MeV)
U233	$0.009691 \pm 14.3\%$	no measured data	$0.02480 \pm 22.6\%$
U235	$0.009314 \pm 3.8\%$	$0.01352 \pm 11.7\%$	$0.01742 \pm 20.7\%$
Pu239	$0.01442 \pm 5.3\%$	$0.01413 \pm 15.9\%$	no measured data

These results for alpha yields suggest that (within the experimental uncertainty) only the yield for ^{235}U between thermal and fast varies significantly. Similarly for tritium, only ^{235}U between thermal and fast shows significant differences. The ^{235}U ternary yield data for fast neutron induced fission contains discrepant data and thus these results are suspect.

Thus it is useful to consider the experiments which measure the relative yields of ternary particles at monoenergetic neutron energies to the yield at thermal energies. Absolute yield measurements were not converted to ratio data for this analysis as this could introduce experimental biases into the results. These results were extracted from the UKFY3 RFYDB file. Figure 5.1 shows measurements of the alpha yield for ^{235}U and ^{239}Pu against energy relative to the thermal yield.

Figure 5.1 Alpha yield as a function of energy for ^{235}U and ^{239}Pu .

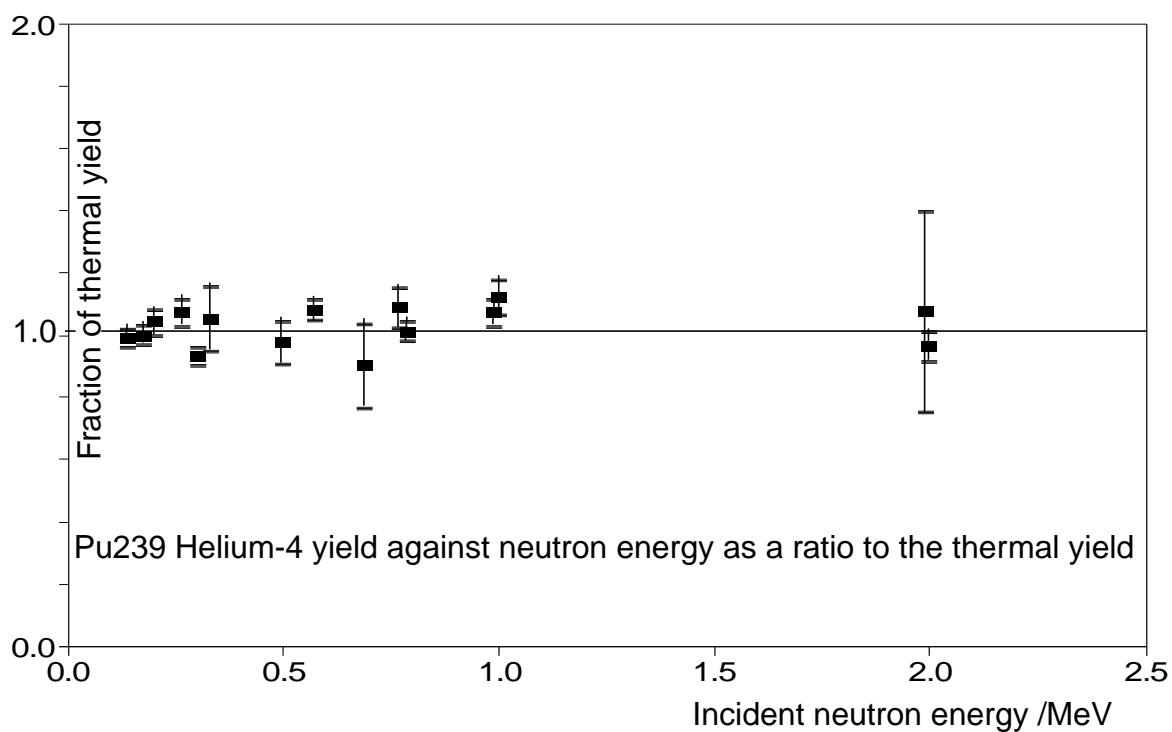
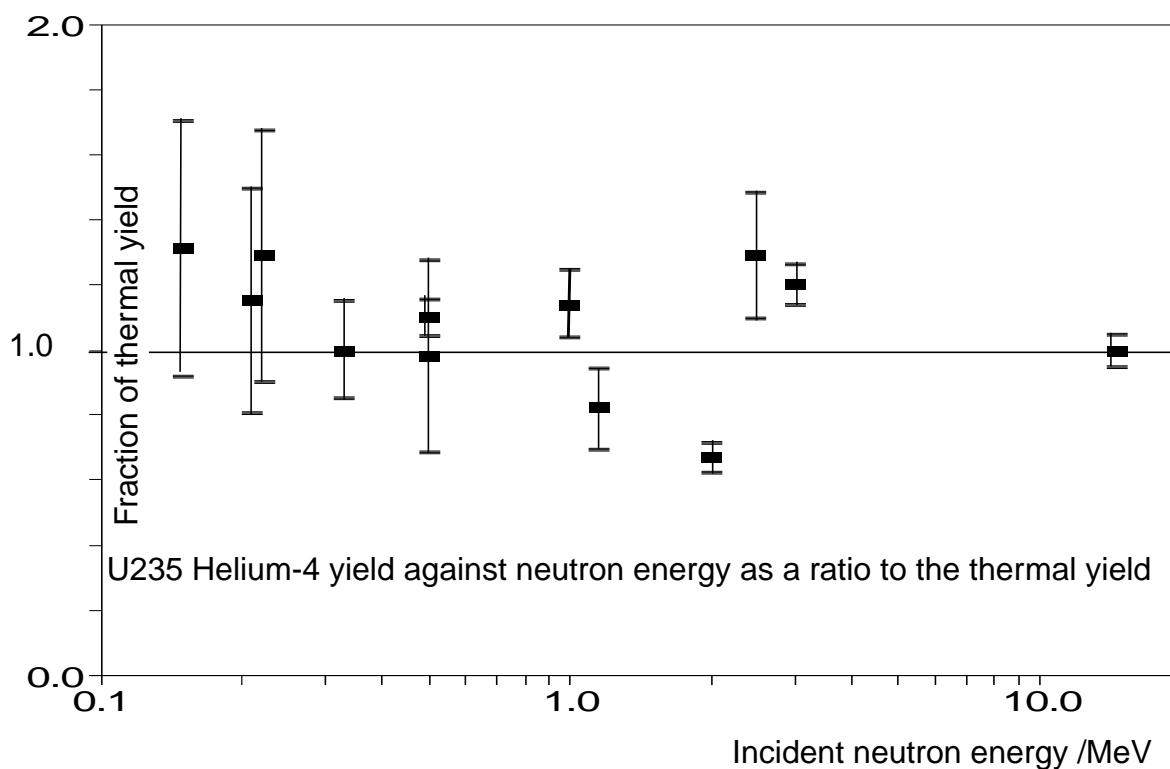
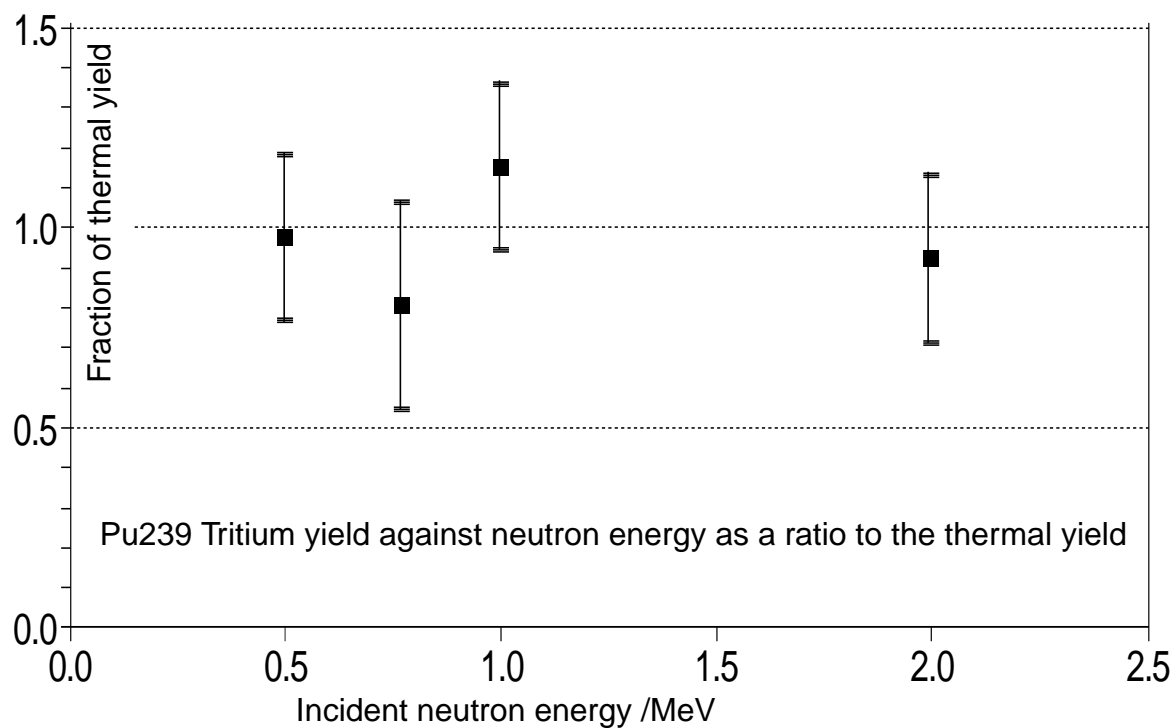
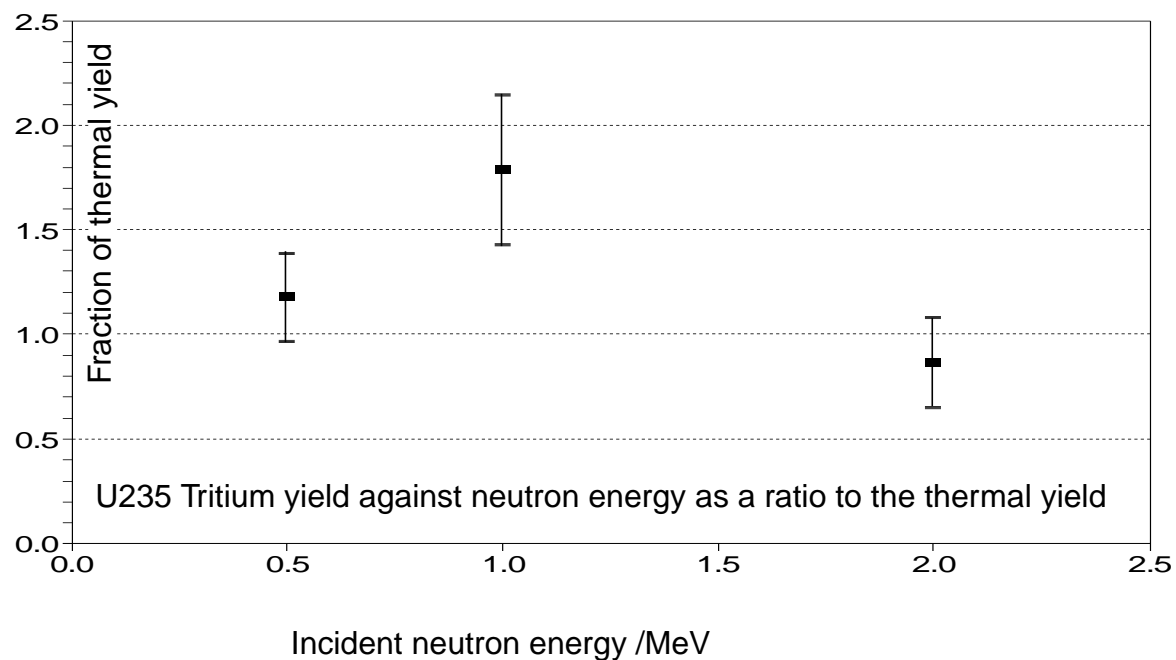


Figure 5.2 Tritium yields as a function of energy



For ^{235}U between 0 and 1 MeV, and at 14 MeV there is no significant differences from the thermal value. However in the region from 1 to 3 MeV the data suggest some possible structure. Only one of these datum significantly varies from the thermal value by more than two standard deviations. Until this difference is confirmed by further measurement it is difficult to exclude an assumption that the data does not vary with energy. It should be noted that between 4 and 14 MeV there is no data. Thus more measurements are needed to determining the yield variation in the region from 2 to 14 MeV.

The ^{239}Pu data, although confined to neutron energies between thermal and 2 MeV and also at 14 MeV show excellent agreement with the thermal yield value.

From the results in Figure 5.1 it can be concluded that there is little evidence that the alpha yield varies significantly with energy between 0 and 14 MeV.

Figure 5.2 shows a similar comparison for tritium yields. However when measurements that used a Gaussian subtraction method to determine the tritium yield were removed only the work of Ouasti^[5.10] remains. Ouasti used the improved particle identification technique. These results show no significant variation between 0 and 2 MeV, which is the most important region for yields in fission reactors. Thus it can be hypothesized that the ternary yields are energy independent between thermal and 14 MeV. It should be remembered that as second chance fission or higher modes become important the fissioning compound nucleus will change and this will alter the yields.

5.3 Modelling light charged particle yields

There have been several attempts to model the light charged particle yields using empirical methods. These techniques are based upon the experimental data and functions of parameters of the compound, or target, nucleus. In the past, several models have been suggested for the alpha yields, primarily through fitting the measured yields to functions of the compound nucleus mass A and charge Z .

Nobles^[5.11] suggested the total ternary yield (alphas, tritons etc.) varied to approximately

[5.10] R.Ouasti, Thesis, University of Bordeaux CENBG 8801, 2228.

±30% as:

$$Y = 0.561 \frac{Z^2}{A} - 18.299 \quad \text{Eqn (3.1)}$$

The Z^2/A term is the fissility parameter related to the “surface tension” like term in liquid drop model^[5.1].

Halpern^[5.12] tried to model the total ternary yield using an expression of the form:

$$Y = m(A + \beta Z) \quad \text{Eqn (3.2)}$$

He found that β equal to -4 and $m= 0.125$ gave a best fit.

For UKFY2^[1.4] both fits to $4Z-A$ and Z^2/A were tried. It was found that the alpha yields fitted, to ±20%, using the expression $Y(^4\text{He})=0.0647 Z^2/A - 2.1292$. The tritium yields were shown to fit best as a constant ratio to the alpha yield as $Y(^3\text{H})=0.06554 Y(^4\text{He})$ to ±25%.

The following work is based upon the new results from the analysis of the UKFY3 database. The ternary yield results from Appendix A.2 are summarized in Table 5.5.

From the UKFY3 recommended data it can be seen that many alpha and triton yields have been measured. However very few of these have more than two independent measurements. Also not all significant systems have both alpha and triton yields. Thus it is necessary to model the yields and then extrapolate and interpolate on the basis of the modelling to estimate the yields for the other fissioning systems.

[5.11] “Long range particles from nuclear fission” R.A.Nobles. Phys. Rev. 126, 1508 (1962)

[5.12] “Three fragment fission”, I.Halpern in Annual review of Nuclear Science Vol. 21 E.Segre, editor (1971)

Table 5.5: Recommended measured UKFY3 light charged particle yields

Neutron Energy	System	Mass	yield per 100 fissions	Standard deviation (%)	number of measurements
Thermal	U233	1	6.542E-03	40.2	1
Thermal	U235	1	1.711E-03	10.8	3
Thermal	Pu239	1	4.080E-03	10.0	1
Fast	U235	1	1.174E-02	51.1	1
High	U233	1	9.018E-03	41.4	1
High	U235	1	6.335E-03	40.4	1
High	U238	1	2.001E-03	100.5	1
High	Np237	1	1.902E-02	41.4	1
Spontaneous	Cf252	1	6.086E-03	23.4	2
Spontaneous	Cf250	1	9.000E-03	25.0	1
Spontaneous	Fm256	1	7.000E-03	30.0	1
Spontaneous	Cm244	1	1.221E-02	41.0	1
Thermal	U233	2	8.466E-04	15.6	1
Thermal	U235	2	8.400E-04	17.9	2
Thermal	Pu239	2	1.347E-03	14.2	2
Spontaneous	Cf252	2	1.500E-03	20.0	1
Thermal	U233	3	9.691E-03	14.3	4
Thermal	U235	3	9.314E-03	3.8	15
Thermal	Pu239	3	1.442E-02	5.3	5
Thermal	Pu241	3	1.410E-02	10.0	1
Fast	U235	3	1.352E-02	11.7	4
Fast	Pu239	3	1.413E-02	15.9	1
High	U233	3	2.480E-02	22.6	1
High	U235	3	1.742E-02	20.7	1
High	U238	3	6.499E-03	22.1	1
High	Np237	3	3.329E-02	22.6	1
Spontaneous	Cf252	3	2.244E-02	3.9	8
Spontaneous	Cf250	3	2.700E-02	20.0	1

Table 5.5: Recommended measured UKFY3 light charged particle yields

Neutron Energy	System	Mass	yield per 100 fissions	Standard deviation (%)	number of measurements
Spontaneous	Fm256	3	3.900E-02	15.0	1
Spontaneous	Cm244	3	2.197E-02	22.0	1
Thermal	U233	4	2.065E-01	4.1	9
Thermal	U235	4	1.699E-01	3.6	12
Thermal	Pu239	4	2.080E-01	3.3	8
Thermal	Pu241	4	2.015E-01	10.0	2
Fast	U233	4	2.003E-01	10.8	1
Fast	U235	4	1.980E-01	8.6	4
Fast	Pu239	4	2.029E-01	8.7	2
High	Th232	4	7.181E-02	36.4	2
High	U233	4	1.957E-01	10.6	1
High	U235	4	1.667E-01	5.3	3
High	U238	4	8.226E-02	9.5	4
High	Np237	4	2.010E-01	10.6	1
Spontaneous	Pu240	4	3.190E-01	10.0	1
Spontaneous	Pu242	4	2.740E-01	10.0	1
Spontaneous	Cf252	4	3.102E-01	6.3	4
Spontaneous	Cf250	4	3.980E-01	10.0	1
Spontaneous	Fm256	4	4.742E-01	8.3	2
Spontaneous	Fm257	4	3.994E-01	7.1	2
Spontaneous	Cm244	4	2.849E-01	9.1	3
Spontaneous	Cm242	4	3.601E-01	12.1	2
Thermal	U233	6	2.153E-03	19.0	3
Thermal	U235	6	2.668E-03	6.9	5
Thermal	Pu239	6	4.098E-03	6.8	3
Spontaneous	Cf252	6	5.304E-03	8.7	4
Thermal	U233	7	7.640E-05	15.6	1
Thermal	U235	7	6.890E-05	40.0	1

Table 5.5: Recommended measured UKFY3 light charged particle yields

Neutron Energy	System	Mass	yield per 100 fissions	Standard deviation (%)	number of measurements
Thermal	Pu239	7	1.400E-04	10.0	1
Thermal	U233	8	3.717E-05	15.6	1
Thermal	U235	8	7.292E-05	16.2	3
Thermal	Pu239	8	6.870E-05	10.0	1
Spontaneous	Cf252	8	1.530E-04	14.5	2
Thermal	U233	9	7.434E-05	15.6	1
Thermal	U235	9	4.071E-05	7.0	5
Thermal	Pu239	9	1.140E-04	10.0	1
Thermal	U233	10	8.880E-04	15.6	1
Thermal	U235	10	5.201E-04	4.9	6
Thermal	Pu239	10	1.050E-03	10.0	1
Thermal	Pu239	11	7.520E-05	10.0	1
Thermal	U235	12	1.261E-05	23.9	2
Thermal	Pu239	12	4.730E-05	22.7	1
Thermal	U235	13	3.360E-06	40.0	1
Thermal	Pu239	13	2.790E-05	30.8	1
Thermal	U235	14	1.578E-04	15.4	2
Thermal	Pu239	14	3.010E-04	10.0	1
Thermal	U235	15	2.528E-05	12.8	3
Thermal	Pu239	15	7.520E-05	37.1	1
Thermal	Pu239	16	7.520E-05	45.7	1
Thermal	U235	17	2.379E-06	30.2	1
Thermal	U235	18	9.531E-07	39.0	3
Thermal	U235	20	5.551E-08	195.2	3
Thermal	Pu239	20	1.720E-05	50.0	1
Thermal	U235	21	2.146E-04	20.3	1

For UKFY3 many variations of functions based upon Z and A were fitted ($mZ^2/A + c$, $mZ + c$, $mA + c$, $m(3Z-A) + c$, $m(4Z-A)+c$, $m(5Z-A) + c$, $m(5Z-2A) +c$, $m(6Z-A)+c$, $m(7Z-A)+c$,

Table 5.6: Fit of light charged particle yields to mA+uZ+c and minimized χ^2

Mass	No. of yields	m	u	c	compound or target nucleus A and Z	%ssd ^a	max fd ^b	χ^2	maximum $\frac{y_i - y_{calc}}{\sigma_i}$	Birge factor
1	12	-7.34248E-04	2.65548E-03	-6.92273E-02	T	18.1	1.204	17.84	2.04	1.408
1	12	-1.25635E-03	3.62711E-03	-3.85114E-02	C	13.2	0.849	11.51	1.68	1.131
2	4	-3.33654E-05	2.24928E-04	-1.19789E-02	T	5.5	0.141	1.470	1.00	1.212
2	4	-3.04722E-05	2.10178E-04	-1.13758E-02	C	5.5	0.143	1.480	1.00	1.217
3	14	-8.01834E-04	4.34694E-03	-0.201201	T	7.9	0.633	31.36	2.80	1.689
3	14	-1.20919E-03	5.16755E-03	-0.183667	C	7.1	0.552	28.84	2.63	1.620
4	20	-2.07685E-02	7.97179E-02	-2.27349	T	3.1	0.292	58.44	-4.02	1.854
4	20	-1.87692E-02	7.52467E-02	-2.39449	C	4.5	-0.54	115.4	-5.73	2.606

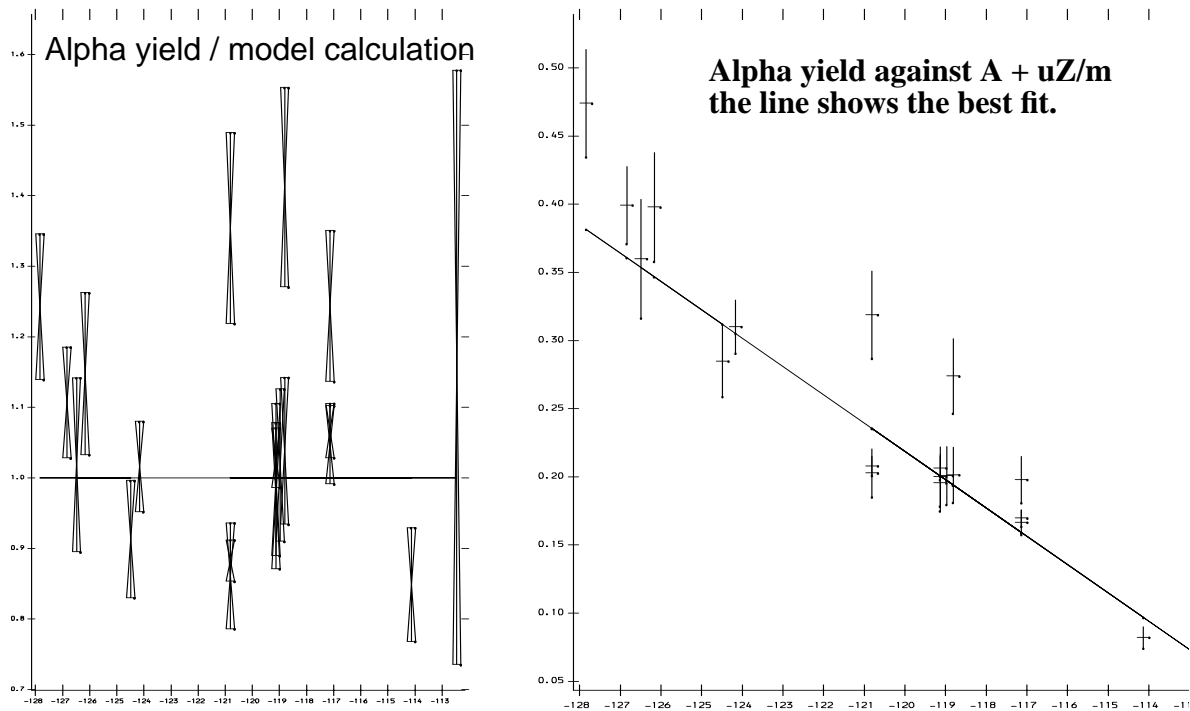
a. %SSD is defined as
$$100 \sqrt{\frac{1}{n(n-1)} \sum \frac{(y_i - y_{calc})^2}{y_i^2}}$$

b. MAXFD is defined as the maximum
$$\frac{y_i - y_{calc}}{y_i}$$

$m(7Z-2A) + c$, $mA+uZ+c$ and $mA+uZ$). Also the effect of fitting to the target nucleus mass and charge, rather than the compound nucleus was tried. The best fit with a minimum χ^2 was found in all cases to be the function $Y=mA+uZ+c$. This was the case where there was sufficient data to fit this function which there were for masses one to four. As the energy dependence was shown above to be minimal all the data were merged; fitting the separate energies did not give any better fit. These results for masses one to four are summarized in Table 5.6

Table 5.7 shows the mass four yields are best fitted by using the target nucleus parameters and the calculated yields have an estimated percentage uncertainty (%SSD) of 3.1%. This should be multiplied by the Birge factor to give a standard deviation of 5.8% of the calculated value. The fit is shown in Figure 5.3 along with a plot of the experimental yields divided by the model calculation.

Figure 5.3 Fit of alpha yields to $mA+uZ+c$.



The fits shown in Figure 5.3 can be used to predict all the unmeasured alpha fission yields required for the UKFY3 evaluation. However the fits for masses 1, 2 and 3 when

extrapolated all predict some negative yields for fissioning systems that are required for UKFY3. Thus the ratios of the other ternary yields to the alpha yields were investigated. Table 5.7 shows the recommended yields from Table 5.5, for masses in the range of one to ten, divided by the respective recommended alpha particle yield.

For each light charged particle mass the ratios of each yield to the alpha fission yield appear similar, independent of the fissioning system, thus a χ^2 fit to a constant ratio was tried, which is effectively a weighted mean of the ratios. The same procedures as employed with the experimental data analysis were applied. The weighted mean and the internal and external standard deviations were calculated. Table 5.8 gives these parameters for each mass from one to ten. The maximum of the internal and external standard deviation was accepted as the recommended error quoted in the table as a percentage. The maximum difference between the experimental and calculated yields expressed as a multiple of the experimental standard deviation, $(y_i - y_{calc})/\sigma_i$, is also shown.

The experimental yield data for masses 1, 2 and 3 are shown in Figures 5.4, 5.5 and 5.6.

These figures and Table 5.8 show that it can be assumed that the hydrogen yields are a constant fraction of the alpha yield, and independent of mass and charge of the fissioned nuclide.

To conclude: for the UKFY3 evaluation the recommended data from the analysis summarized in appendix A.1 were adopted.

The missing ^4He yields were calculated from the $Y = mA + uZ + c$ formula with a 5.8% standard deviation. The missing ^1H , ^2H and ^3H yields were then calculated using the ^4He yields and ratios given in Table 5.8 with the fractional standard deviations calculated by quadrature.

Table 5.7: Recommended UKFY3 light charged particle yields relative to the α yield

Neutron Energy	System	Mass	yield per 100 alpha particles	Standard deviation (%)
Thermal	U233	1	3.16804	40.4085
Thermal	U235	1	1.00706	11.3842
Thermal	Pu239	1	1.96154	10.53043
Fast	U235	1	5.92929	51.8186
High	U233	1	4.60807	42.7355
High	U235	1	3.80024	40.7462
High	U238	1	2.43253	100.9480
High	Np237	1	9.46269	42.7355
Spontaneous	Cf252	1	1.96196	24.2332
Spontaneous	Cf250	1	2.26131	26.9258
Spontaneous	Fm256	1	1.47617	31.1270
Spontaneous	Cm244	1	4.28571	41.9977
Thermal	U233	2	0.409976	16.1298
Thermal	U235	2	0.494408	18.2584
Thermal	Pu239	2	0.647596	14.5784
Spontaneous	Cf252	2	0.483559	20.9688
Thermal	U233	3	4.69298	14.8762
Thermal	U235	3	5.48205	5.23450
Thermal	Pu239	3	6.93269	6.24340
Thermal	Pu241	3	6.99752	14.1421
Fast	U235	3	6.82828	14.5207
Fast	Pu239	3	6.96402	18.1246
High	U233	3	12.6725	24.9624
High	U235	3	10.4499	21.3677
High	U238	3	7.90056	24.0554

Table 5.7: Recommended UKFY3 light charged particle yields relative to the α yield

Neutron Energy	System	Mass	yield per 100 alpha particles	Standard deviation (%)
High	Np237	3	16.5622	24.9624
Spontaneous	Cf252	3	7.23404	7.40945
Spontaneous	Cf250	3	6.78392	22.3607
Spontaneous	Fm256	3	8.22438	17.1432
Spontaneous	Cm244	3	7.71148	23.8078
Thermal	U233	6	1.04262	19.4373
Thermal	U235	6	1.57034	7.78267
Thermal	Pu239	6	1.97019	7.55844
Spontaneous	Cf252	6	1.70986	10.7415
Thermal	U233	7	3.69976E-02	16.1298
Thermal	U235	7	4.05533E-02	40.1617
Thermal	Pu239	7	6.73077E-02	10.53043
Thermal	U233	8	1.80000E-02	16.1298
Thermal	U235	8	4.29194E-02	16.5952
Thermal	Pu239	8	3.30288E-02	10.53043
Spontaneous	Cf252	8	4.93230E-02	15.8095
Thermal	U233	9	3.60000E-02	16.1298
Thermal	U235	9	2.39612E-02	7.87147
Thermal	Pu239	9	5.48077E-02	10.53043
Thermal	U233	10	4.30024E-01	16.1298
Thermal	U235	10	3.06121E-01	6.08030
Thermal	Pu239	10	5.04808E-01	10.53043

Table 5.8: Weighted means of ratio to α yields

mass	weighted mean	internal sd	external sd	recommended % error from mean	max diff/expt error
1	1.58184E-02	1.98492E-03	2.53297E-03	16.0	-2.018
2	4.83424E-03	6.92095E-04	4.39668E-04	14.3	0.896
3	6.89694E-02	5.49694E-03	5.20911E-03	8.0	1.934
4	1.00000	6.43791E-02	0.	6.4	0.
6	1.39646E-02	2.03853E-03	2.06317E-03	14.8	-1.200
7	4.33226E-04	8.18369E-05	8.13437E-05	18.9	1.260
8	2.61057E-04	4.01731E-05	6.46611E-05	24.8	1.664
9	3.08327E-04	5.30162E-05	7.18898E-05	23.3	1.547
10	3.78596E-03	6.32407E-04	5.76288E-04	16.7	0.884

Figure 5.4: Ratio of ^1H yield to ^4He yield

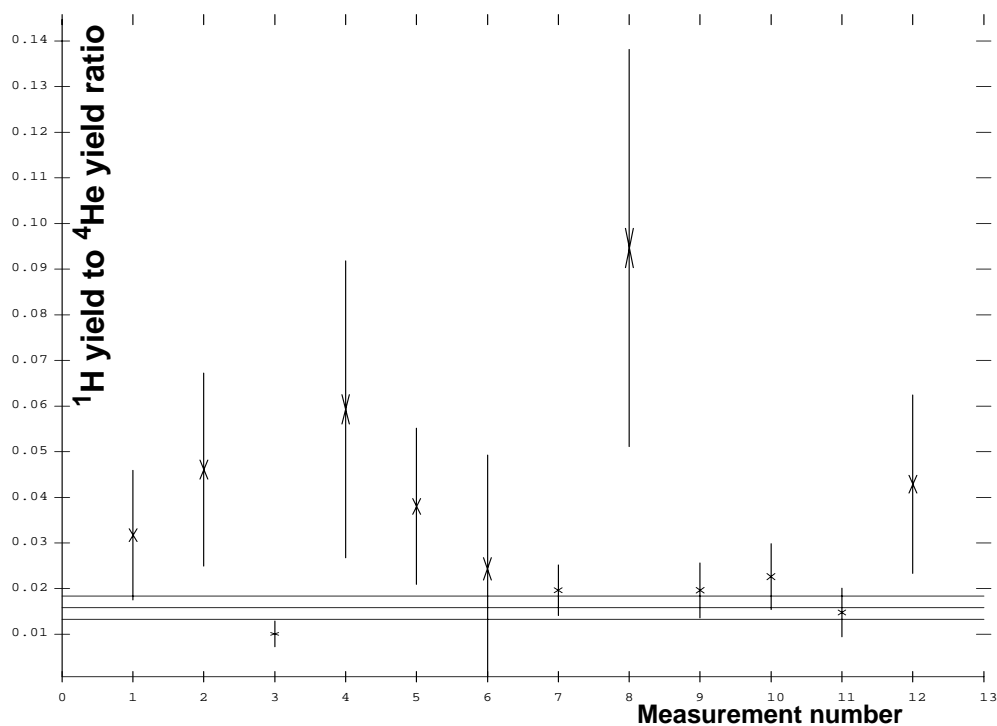


Figure 5.5: Ratio of ^2H yield to ^4He yield

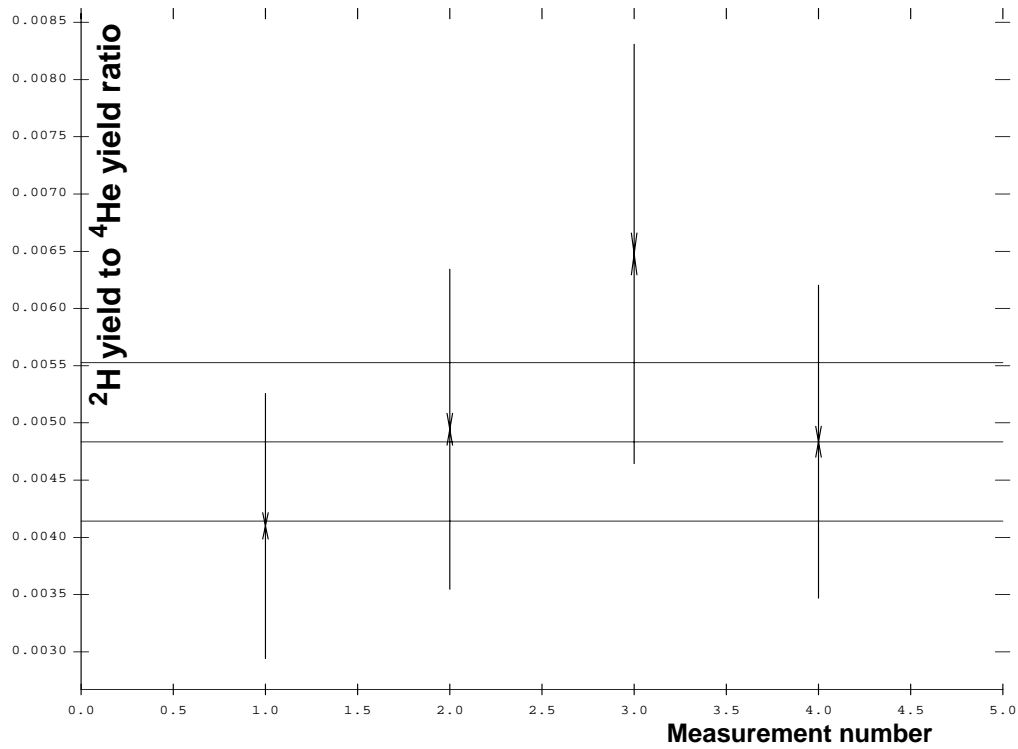
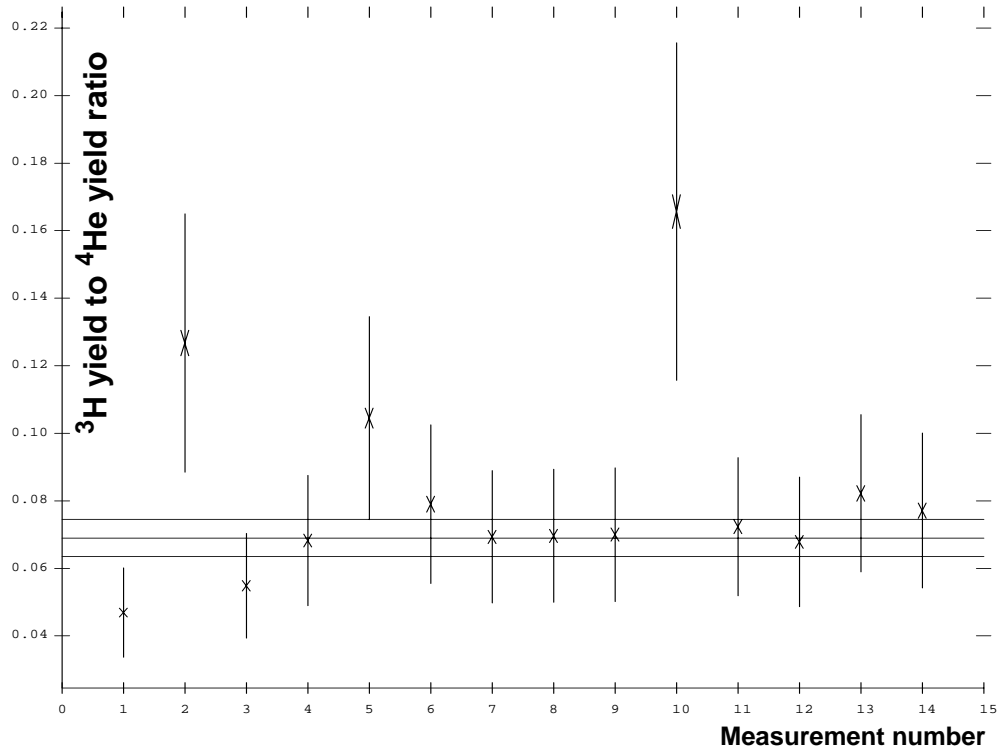


Figure 5.6: Ratio of ^3H yield to ^4He yield



6. FRACTIONAL INDEPENDENT YIELDS

6.1 Introduction

In the proceeding chapters chain and ternary yields have been discussed. In considering these cases the charge distribution of the fragments has been of minimal interest. However, this distribution can be very important practically as isobars, different products with the same mass but varying nuclear charge, can have considerably different properties. The half-lives may ranging from milli-seconds to many millions of years. Also the decay modes, emitted radiation and energy released per decay can be very different. The charge distribution and the chain yields are significant in determining the distribution of yield in (A,Z) space and thus the yield of each nuclide generated. Clearly these yields are an important component in any calculation of the source terms for determination of properties such as the chemical inventory of irradiated fuel, its decay heat or radiation emission.

The different chemistry of the products will determine their mobility and chemical behaviour, and thus this information is important in any shielding or radio-toxicity calculation. For example if we consider ^{85}Kr which is a beta emitter with a 10.72 year half-life. This is a major fission product which due to its chemistry, being an inert gas, is released from any chemical or mechanical processing of spent fuel. However, because it is inert it does not become absorbed into the food chain and thus gives a low dose to the population. On the other hand ^{129}I , another short-range beta emitting product with a similar yield to krypton-85, has a much lower activity as it has a half-life of 15.69 million years; it is also easily absorbed into biological material. Thus it is of far greater importance in assessing the collective population dose from the reprocessing of spent reactor fuel.

The chemistry of fission products will also determine their diffusion within the irradiated fuel matrix. The fission products generated in the fuel can affect the fuel matrix directly causing, along with neutron damage, fuel swelling and cracking. The shielding and containment of fission products in fuel and reactor pressure vessels will depend upon how easily radioactive fission products can escape through the fuel cladding, especially if

the fuel is damaged. In calculations of radioactive release from reactor accidents the mobility of fission products, especially as a function of temperature, is of great importance.

In the case of reprocessing where the fuel is sheared and reprocessed (for example in the PUREX process) the fission product chemistry will determine what fraction of each product will end up in each chemical process stream, whether in the gaseous or liquid waste streams or as a contaminant in one of the product streams (typically uranium or plutonium).

6.2 Semi-empirical models of charge distribution

As discussed in chapter 4 there is no theoretical nuclear model which can be used to calculate the mass distribution from fission with any degree of success without empirical determination of some parameters. The most promising models based upon the work of Brosa, Grossman and Müller^[6.1] do not determine the charge of the fragments. Thus an empirical approach is required.

The first semi-empirical models to consider the charge distribution of fission product fragments were based upon the “unchanged charge distribution”. This is based upon the assumption that the charge distribution of the compound nucleus has insufficient time to respond to the changes in the nucleus and thus the charge-to-mass ratio of the products will be the same as the pre-scission compound nucleus. Thus the most probable charge of the post scission but pre-prompt neutron emission fragment of mass A, called $Z_p(A)$, is given by

$$Z_p(A) = \frac{Z_f}{A_f} \cdot A \quad \text{Eqn (6.1)}$$

Models based upon this assumption, including those with improvements are called Z_p

[6.1] Physics reports (Review Section of Physics Letters) 197, No. 4, p162-262. “Nuclear Scission”, U.Brosa, S.Grossman and A. Müller (1990).

models. These models have been developed by A.C.Wahl. In early work in this area Wahl et al^[6.2] used $Z_p(A)$ as the maximum of a lumped Gaussian distribution of yield over Z for a given A with a width (charge variation), σ . The Gaussian is normalized to one for each mass chain; the expected value of the yield for a particular A and Z is given by integrating the Gaussian between $Z-0.5$ and $Z+0.5$ as follows:

$$FI(A, Z) = \int_{Z-0.5}^{Z+0.5} \frac{1}{\sqrt{2\pi}\sigma} e^{-0.5\left(\frac{Z-Z_p(A)}{\sigma}\right)^2} dZ \quad \text{Eqn (6.2)}$$

As more experimental data became available and the width and $Z_p(A)$ were fitted for individual mass chains it led to the observation of two phenomena. Firstly, if this simple model is used the width appeared to have an oscillatory nature with a cycle of 2 mass units. This was subsequently explained by Wahl as the preferential production of even-even nuclides compared to odd-odd. This is called the odd-even effect.

For any mass chain the mass number is the sum of protons and neutrons; thus there are two possible combinations of even and odd protons and neutrons for both even and odd mass chains. These are shown in Table 6.1. Thus, for each mass, there are two parameters that are needed to define the odd-even effect; these are the probabilities of producing the different even and odd combinations. It should be noted that these odd-even multiplicative factors will alter the summation for the total from 1.0; thus it is necessary to multiply the yields by a factor so that the yields are re-normalised to 1.0.

Table 6.1: Possible combinations of protons and neutrons for even and odd mass nuclides.

mass	number of protons	number of neutrons
even	even odd	even odd
odd	even odd	odd even

[6.2] Phys. Rev. 126, 1112. A.C.Wahl et al (1962).

The second observed phenomenon was that the measured $Z_p(A)$, the average charge for a mass chain, was higher than the unchanged charge distribution calculation for the light fragments and lower for the heavy fragments. Also, this difference varied smoothly with mass number. It should be noted that because of charge conservation during fission the effects on the low mass peak mirror the effects on the high mass peak.

These features are described by Wahl's latest Z_p model^[6.4]. Wahl developed a parameterization to model the above effects and the variation of charge distribution around symmetry^[6.3]. He used this later in an extensive study of charge distribution for ^{235}U , ^{233}U , ^{239}Pu and ^{252}Cf .^[6.4]

In Wahl's latest Z_p model the distribution is modelled as the difference between two error functions. As the integral of a normal distribution $f(t)$ can be shown^[3.1] to be

$$\int_0^x f(t) = \frac{1}{2} \operatorname{erf}\left(\frac{x}{\sqrt{2}}\right) \quad \text{Eqn (6.3)}$$

then the integral of a normal distribution between $z+0.5$ and $z-0.5$, as in Eqn (6.2), will be:-

$$\frac{1}{2} \left(\operatorname{erf}\left(\frac{z+0.5}{\sqrt{2}}\right) - \operatorname{erf}\left(\frac{z-0.5}{\sqrt{2}}\right) \right) \quad \text{Eqn (6.4)}$$

Thus Wahl's Z_p model of fractional independent yield, FI, can be described by:

$$\text{FI}(A, Z) = \frac{1}{2} F(A, Z) N(A) (\operatorname{erf}(V) - \operatorname{erf}(W)) \quad \text{Eqn (6.5)}$$

where $F(A, Z)$ describes the odd-even effect and $N(A)$ normalizes to 1 the summation of all the elements of each mass A to 1.0 for each mass chain.

[6.3] J. Radioanal. Chem. 55, 111. A.C.Wahl (1980).

[6.4] Atomic and Nuclear Data Tables 39, 1-156. "Nuclear charge distribution and delayed neutron yields for thermal neutron induced fission of ^{235}U , ^{233}U , ^{239}Pu and for spontaneous fission of ^{252}Cf ", A.C.Wahl (1988).

The V and W are defined by;

$$V = \frac{Z(A) - Z_p(A) + 0.5}{\sigma_z(A)\sqrt{2}} \quad , \quad \text{Eqn (6.6)}$$

$$W = \frac{Z(A) - Z_p(A) - 0.5}{\sigma_z(A)\sqrt{2}} \quad , \quad \text{Eqn (6.7)}$$

The similarity of Eqn (6.2) with Eqn (6.5) using Eqn (6.4) thus becomes apparent.

The Z_p model is extended from the simple formation of Eqn (6.1) to allow for variation with a correction term ΔZ which, for the high mass peak, is defined as;

$$Z_p(A_H) = A'_H \frac{Z_f}{A_f} + \Delta Z(A'_H) \quad , \quad \text{Eqn (6.8)}$$

Similarly for the low mass peak;

$$Z_p(A_L) = A'_L \frac{Z_f}{A_f} + \Delta Z(A'_{Hc}) \quad A'_{Hc} = A_f - A'_L \quad \text{Eqn (6.9)}$$

Where A' is defined as the fragment mass after prompt neutron emission and A is the initial fragment mass, where

$$A' = A - v(A) \quad , \quad \text{Eqn (6.10)}$$

The $v(A)$ function is the average neutron emission from a fragment of mass A . Wahl calculates this from the chain yield distribution by a modification of the summation method of Terrell^[6.5]. If we define the symmetrical mass as half the compound nucleus mass, the sum of the chain yields $S_L(A_1)$ from A_1 to the symmetrical mass, $S(A)$, can be

[6.5] Phys. Rev. 127, 880. J.Terrell (1962)

calculated for the low mass peak as

$$S_L(A_1) = \sum_{A=A_1}^{\text{symmetry}} Y(A) \quad \text{Eqn (6.11)}$$

and similarly for the high mass peak $S_H(A_f - A_1)$

$$S_H(A_f - A_1) = \sum_{A=A_f - A_1}^{\text{symmetry}} Y(A) \quad \text{Eqn (6.12)}$$

Then the difference between $S_H(A_1)$ and $S_L(A_1)$ gives the average neutron emission for each mass split. From the conservation of mass the complementary masses and mass of emitted neutrons will equal the compound nucleus mass i.e.

$$A_L + A_H + \bar{\nu}_p = A_f \quad \text{Eqn (6.13)}$$

Figure 6.1 shows the $S_H(A_1)$ and $S_L(A_1)$ calculated from the UKFY3 chain yields for ^{235}U thermal neutron induced fission. From this graph the mass differences between the two mass peaks, the neutron loss, can be generated.

Wahl then assumes that symmetrical fission produces four neutrons; a value consistent with the difference between the observed fragment kinetic energy and calculations assuming no neutron emission^[6.6]. If we consider the ratio, R_H , of neutron emission from the high mass peak to the total; at symmetry this must equal R_L and as $R_H + R_L = 1$ then $R_H = 0.5$. Using this and the results from Figure 6.1 it is possible to estimate the $\nu(A)$ function. The calculation of $\nu(A)$ for ^{235}U thermal neutron induced fission by Wahl^[6.4] is shown in Figure 6.2.

[6.6] Z.Phys. A 309, 253. D.Belhafaf et al (1983).

Figure 6.1: S_H and S_L calculated from the ^{235}U thermal neutron induced fission.

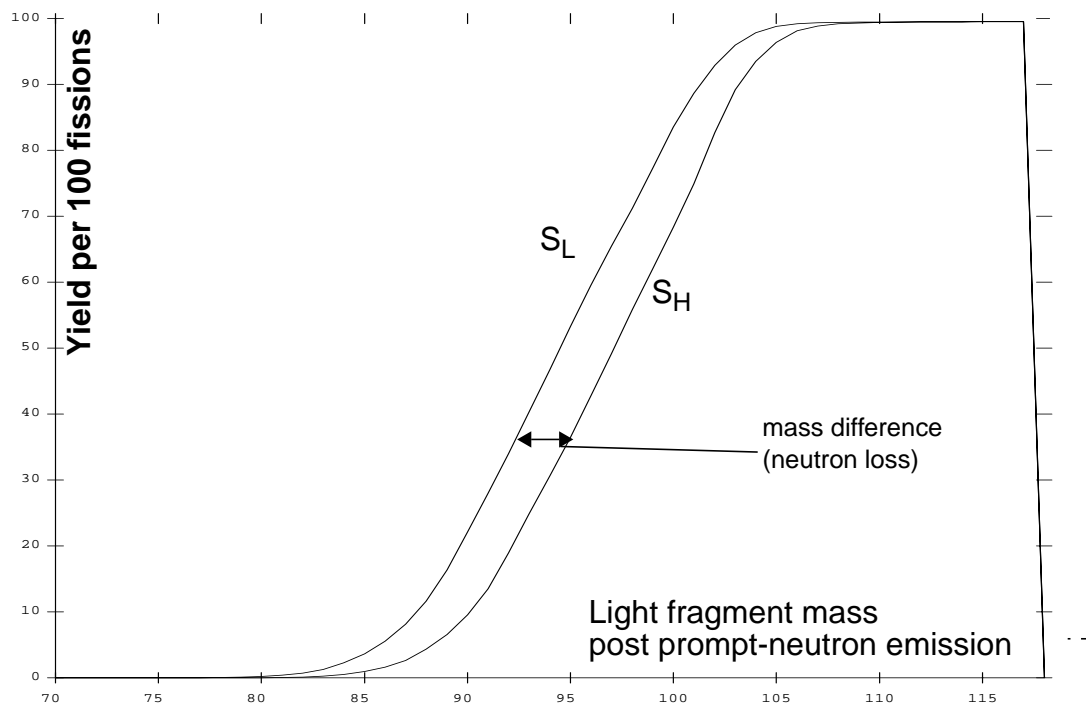
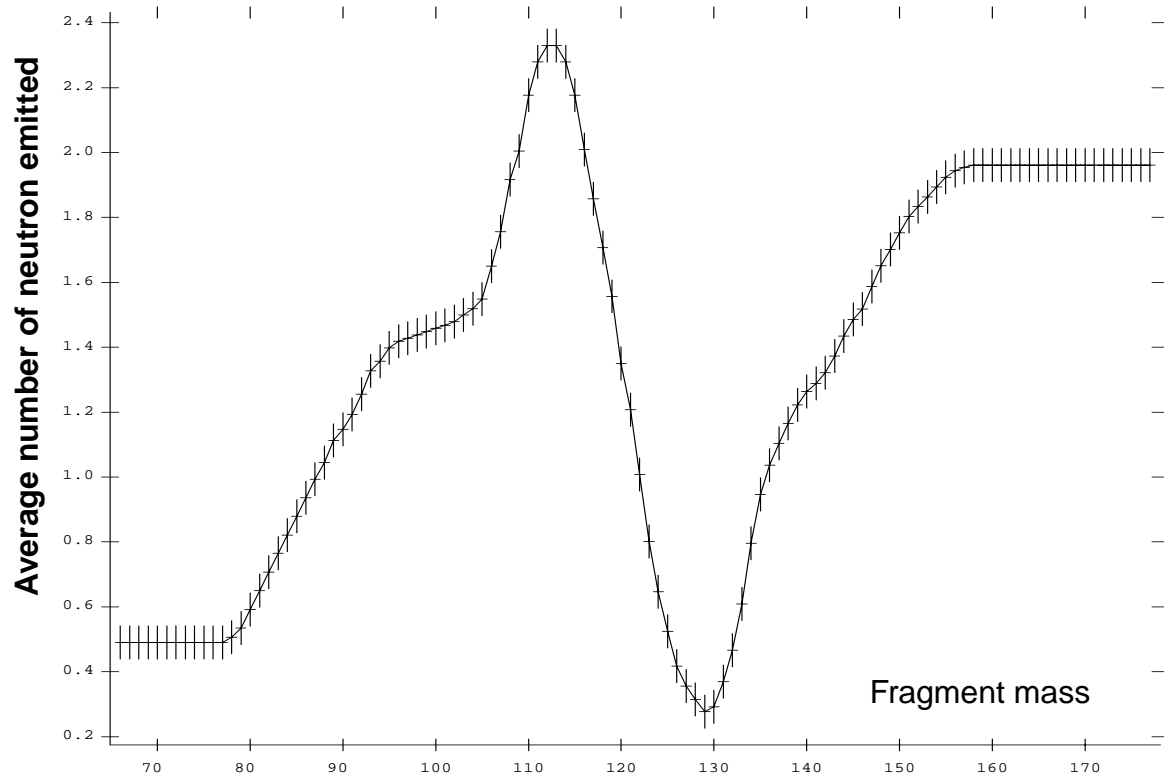


Figure 6.2: $\nu(A)$ for ^{235}U thermal neutron induced fission



Wahl's method can be used to determine the $\nu(A)$ function for any fissioning system where the chain yield distribution has either been measured or can be estimated.

The odd-even effect term, $F(A,Z)$, is modelled by Wahl as a function of two parameters \bar{F}_Z and \bar{F}_n . If the nuclear charge is even the proton term, \bar{F}_Z , is used else the reciprocal $1/\bar{F}_Z$ is used. Similarly with the neutron term \bar{F}_n . Table 6.2, below, gives the $F(A,Z)$ function for even and odd numbers of neutrons and protons.

Table 6.2: $F(A)$ as a function of \bar{F}_Z and \bar{F}_n

$F(A,Z)$	proton number Z	neutron number N
$\bar{F}_Z \bar{F}_n$	even	even
$\frac{\bar{F}_Z}{\bar{F}_n}$	even	odd
$\frac{\bar{F}_n}{\bar{F}_Z}$	odd	even
$\frac{1}{\bar{F}_Z \bar{F}_n}$	odd	odd

The ΔZ function of the model is approximated by a straight line function defined by the value of ΔZ at the post-prompt neutron emission mass 140 with a slope $\frac{\delta \Delta Z}{\delta A'_H}$.

$$\text{i.e.} \quad \Delta Z(A'_H) = \Delta Z(A'=140) + \frac{\delta \Delta Z}{\delta A'_H} [A'_H - 140] \quad \text{Eqn (6.14)}$$

Near symmetry Wahl^[6.7] found the ΔZ , width and odd-even effect varied from the above equations. The model showing the approximation of the observed ΔZ for the high mass

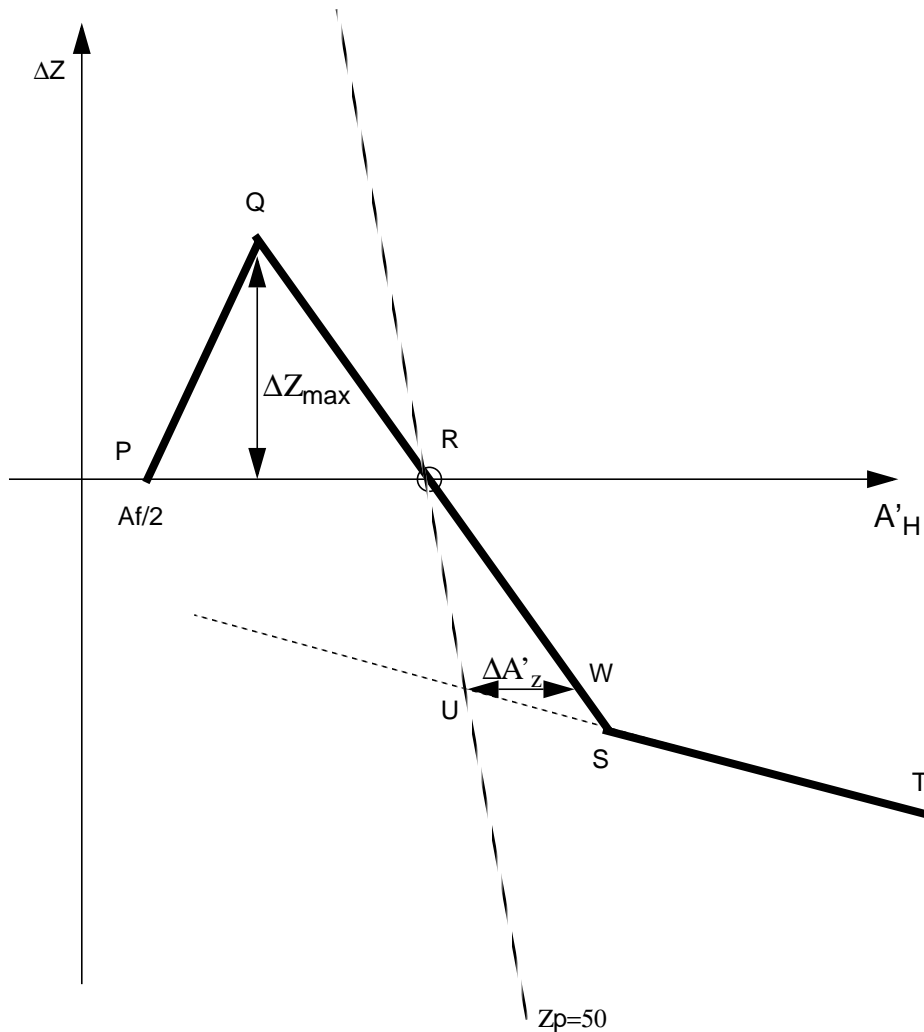
[6.7] Phys. Rev. C, 32, 184. A.C.Wahl (1985).

peak is shown in Figure 6.3.

The model based upon Wahl's analysis of his experimental database showed the ΔZ function to be described by two straight lines, PQ and QS, in the region near symmetrical fission (i.e. $A_f/2$), and one straight line outside of this region, ST.

The $\Delta Z(A_H)$ must, due to charge conservation, be equal to $-\Delta Z(A_{H_C})$. Thus at the joining of these two regions the ΔZ must equal zero. Therefore the ΔZ at $A_f/2$, point P, must be zero. Point R is defined from the empirical observation that where $Z_p=50$ the function ΔZ is indistinguishable from zero. These are the fixed points from which the other points are defined.

Figure 6.3: Variation of ΔZ near symmetry



Starting at the most asymmetric fission region, i.e. A'_H is at its highest value, the ΔZ is described by defined by Eqn (6.8). The line QR is defined by the value of ΔZ_{\max} and $\Delta A'_Z$. $\Delta A'_Z$ is the change in mass from the intersection of the $Z_p=50$ function and Eqn (6.8), and line QS. The point S is defined as intersection of Eqn (6.8) with the line obtained by extending from QR.

Wahl observed that the charge distribution width falls from $\overline{\sigma_Z}$ between Q and S, he defined the reduced width as $\overline{\sigma_{50}}$. Also Wahl's modelling showed $F(A,Z)$ to be approximately equal to 1.0, i.e. no odd-even effect, from P to S.

The ΔZ function is defined by the points P and R where ΔZ equals zero, and the ΔZ_{\max} and $\Delta A'_Z$ parameters combined with Eqn (6.8). As referred to above in the section on the mass yields due to complementary element charge conservation these effects are mirrored below symmetry. This is based upon the conservation of charge, before beta decay, in the splitting of the compound nucleus i.e. the charge in all the fragments must equal that of the compound nucleus.

6.3 Fitting the UKFY3 database to the Z_p model

The UKFY3 fractional independent yields were fitted to the Wahl Z_p model using Fortran routines from the NAG library^[6.8]. The method of fitting used are that of Gill and Murray^[6.9].

From an initial guess of the 8 parameters $x^{(1)} = [x_1 \ x_2 \ \dots x_8]$ of $FI(A,Z)$ from Eqn (6.5) the fractional independent yields of the measured data is calculated and then the residuals are generated. By perturbing the elements of x , a direction or gradient matrix, p , with elements $\left[\frac{\partial R}{\partial x_1} \ \dots \ \frac{\partial R}{\partial x_8} \right]$ is generated which contains the sensitivities of R , the sum of difference squared to changes in x at $x^{(1)}$. From this an improved estimate, $x^{(2)}$, is

[6.8] Numerical Algorithms Group library mark 15, NAG Ltd., Wilkinson House, Jordan Hill Road, Oxford, United Kingdom, OX2 8DR.

[6.9] J. Numer. Anal., 15, pp. 977-992. "Algorithms for the solution of the nonlinear least-squares Problem", P.E.Gill and W.Murray. (1978).

generated by minimizing $R(x^{(1)} + \alpha p)$ with respect to α . Then, by iteration, improved estimates of x are determined using $x^{(k+1)} = x^{(k)} + \alpha^{(k)} p^{(k)}$.

The $v(A)$ function used was taken from the ^{235}U thermal values reported by Wahl^[6.4].

For UKFY2^[1.4] the use of the Z_p model had incorrectly assumed that the $\Delta A'_z$ parameter was the mass difference between R and S^[6.10], rather than as reported by Wahl the distance between R and W. Fortunately, when the model was corrected, the difference in the χ^2 values of the fits between the erroneous and corrected models did not change above the second decimal place.

In the UKFY2 analysis fractional independent yield data with low values were mostly discrepant. Thus a lower limit was set to remove these from the fit. For the UKFY3 the χ^2 value from least-squares fits was found to be sensitive to the lowest fractional independent value used in the fit.

However it was noticed whilst looking at the residuals of the fits that occasionally the same mass and charge yields were given twice in the data set; this occurred where both the total and the sum of isomer yields (ground, first metastable etc.) were available. Several of these repeated yields differed considerably, adding significantly to the total χ^2 . Thus the following procedure was defined: where a yield was repeated a first fit was used to determine the more discrepant of the two yields; this one was then rejected, and a second fit produced using the remaining single measurement. This was done even though, in general, it was felt that removing experimental data just because it did not fit a model was never really justified. However, using the model to reject the most discrepant of **repeated** measurements was felt justifiable as these usually produce large discrepancies in the data and have large statistical uncertainties. Such a procedure should, however, only be used with great caution. The results of fitting the UKFY3 data by both methods is shown in Table 6.3.

[6.10] Private communication from A.C.Wahl (1993).

Table 6.3 Fitting to U235T using the UKFY2 routine and the new UKFY3 routine

Minimum fractional independent yield	number of measured yields after discrepant point removal	number of measured yields in database before discrepant point removal	χ^2 for UKFY2 model on UKFY3 data	No. of points differing by factor of two from model	Revised model χ^2	No. of points differing by factor of two from model
0.5	48	54	1.90	0	1.54	0
0.2	118	118	2.36	1	1.98	0
0.1	133	149	2.48	5	2.24	2
0.05	162	184	2.88	6	2.55	3
0.02	179	211	3.01	8	2.54	4
0.01	191	231	3.31	13	2.59	6
0.005	198	241	3.39	17	2.66	6
0.001	205	253	5.52	17	2.69	7
0.0	210	275	11.19	58	2.75	7

Having shown the new method gives a much better fit following removal of discrepant data, the new parameters were compared with previously published parameters. These are given in Table 6.4.

These results show no significant differences in the parameters between the UKFY3 results and Wahl fits, greater than three standard deviations. But the UK fits have larger uncertainties, especially for parameters determining the ΔZ in the mass region near symmetry. The results show the uncertainties of the different UK fits to be similar, this is probably due to the fact that the UKFY3 database was developed from UKFY2. Wahl's experimental database is independent of the UK file, although both are obviously based on those results published in the open literature. But the two files are processed differently and adjustments to the experimental data due to improved standard yield data, or corrected decay data etc., will be different. Also the two files will not necessarily contain all the results analysed in the other.

Table 6.4 Fits for thermal neutron induced fission of U235 from this and previous works.

Parameter	Wahl (1988)	UKFY2 (1990)	UKFY3 (UKFY2 method) (1994)	UKFY3 (Wahl model) (1994)
$\Delta Z(A'=140)$	-0.511 ± 0.005	-0.523 ± 0.012	-0.5173 ± 0.013	-0.5329 ± 0.009
$\frac{\delta \Delta Z}{\delta A'_H}$	-0.008 ± 0.001	-0.008 ± 0.002	-0.0063 ± 0.0014	-0.0066 ± 0.0009
$\bar{\sigma}_z$	0.531 ± 0.004	0.5460 ± 0.0112	0.5334 ± 0.011	0.5368 ± 0.0042
$\bar{\sigma}_{50}$	0.33 ± 0.02	0.35 ± 0.02	0.3538 ± 0.021	0.3449 ± 0.023
\bar{F}_z	1.27 ± 0.01	1.2776 ± 0.026	1.269 ± 0.026	1.294 ± 0.024
\bar{F}_N	1.07 ± 0.01	1.077 ± 0.022	1.079 ± 0.022	1.077 ± 0.020
$\Delta A'_z$	0.9 ± 0.2	0.941 ± 0.260	0.998 ± 0.25	0.7 ± 0.43
ΔZ_{\max}	0.7 ± 0.1	0.69 ± 0.24	0.695 ± 0.23	0.6614 ± 0.64
reduced ^a χ^2	1.9	2.61	2.88	2.69
minimum fly	-	0.05	0.05	-
number of measurements	258 ^b	145	162	210

a. Reduced χ^2 is defined as $\left(\frac{1}{n} \sum \frac{(y_i - y_{\text{calc}})^2}{\sigma_i} \right)^{\frac{1}{2}}$

b. Including 21 measurement which are limits

The UKFY3 fitting routine was then applied to the other fissioning systems with more than 30 experimentally measured yields; the corresponding $v(A)$ function was estimated by multiplying the ^{235}U thermal neutron fission values by the ratio of the system's $\bar{\nu}_p$ value over the ^{235}U thermal neutron fission value. This approximation has been shown during the fitting procedure for UKFY2 to have little effect on χ^2 .

The three fissioning systems of ^{235}U thermal, fast and 14MeV (high energy) neutron induced fission were fitted, the results being shown in Table 6.5. An attempt to fit all the parameters of the model failed for all but the thermal neutron fission of ^{235}U . The parameters which did not converge in the other systems were fixed to the ^{235}U values and the fitting procedure repeated. The parameters where the values from the thermal neutron fission of ^{235}U were used are shown in the following table in brackets. It should be noted that these parameters are those defined around symmetry which have low yields and are thus difficult to measure.

Table 6.5 Parameters from fitting ^{235}U at thermal, fast and High energies.

Parameter	U235T	U235F	U235H
$\Delta Z(A'=140)$	-0.5329 ± 0.009	-0.418 ± 0.1	-0.229 ± 0.1
$\frac{\delta \Delta Z}{\delta A'_H}$	-0.0066 ± 0.001	-0.022 ± 0.001	-0.010 ± 0.001
$\overline{\sigma}_z$	0.5368 ± 0.0042	0.503 ± 0.002	0.620 ± 0.009
$\overline{\sigma}_{50}^a$	0.3449 ± 0.023	(0.3449)	0.169 ± 0.05
\overline{F}_z	1.294 ± 0.024	1.046 ± 0.02	1.05 ± 0.02
\overline{F}_N	1.077 ± 0.02	1.046 ± 0.02	1.06 ± 0.02
$\Delta A'_z^a$	0.7 ± 0.43	(0.7)	(0.7)
ΔZ_{\max}^a	0.6614 ± 0.64	(0.6614)	(0.6614)
reduced χ^2	2.69	2.02	2.29
minimum fit	-	0.05	-
number of measurements	210	48	30

a. values in brackets could not be fitted directly and the U235 thermal neutron induced fission results were used with these values kept constant during the fit.

Of the other systems, only ^{229}Th , ^{233}U and ^{239}Pu for thermal neutron induced fission were fitted successfully. These results are shown in Table 6.6.

Table 6.6 Parameters from fitting U233, Pu239 and Th229 yields for thermal neutron fission.

Parameter	U233T	Pu239T	Th229T
$\Delta Z(A'=140)$	-0.573 ± 0.01	-0.493 ± 0.05	-0.713 ± 0.01
$\frac{\delta \Delta Z}{\delta A'_H}$	-0.014 ± 0.003	-0.013 ± 0.002	-0.011 ± 0.001
$\overline{\sigma_z}$	0.571 ± 0.004	0.566 ± 0.002	0.522 ± 0.0002
$\overline{\sigma_{50}}^a$	0.47 ± 0.07	0.556 ± 0.004	(0.3449)
$\overline{F_z}$	1.259 ± 0.02	1.149 ± 0.02	1.60 ± 0.02
$\overline{F_N}$	1.054 ± 0.02	1.051 ± 0.02	1.070 ± 0.02
$\Delta A'_z{}^a$	(0.7)	(0.7)	(0.7)
$\Delta Z_{\max}{}^a$	(0.6614)	(0.6614)	(0.6614)
reduced χ^2	3.16	2.13	1.67
minimum fit	0.05	0.05	0.05
number of measurements	100	85	48

a. values in brackets could not be fitted directly and the U235 thermal neutron induced fission results were used with these values kept constant during the fit.

Thus six systems have been successfully fitted using the experimental data in the UKFY3 database. However to extend these fits to encompass the 39 systems required for applications it is necessary to interpolate and extrapolate these parameters to derive values appropriate to the other cases.

From the results $\frac{\delta \Delta Z}{\delta A'_H}$, $\overline{\sigma_z}$, $\overline{\sigma_{50}}$, $\overline{F_N}$, $\Delta A'_z$ and ΔZ_{\max} did not show significant variation or could only be fitted for one system, and thus weighted means of -0.01, 0.5, 0.4, 1.06, 0.7 and 0.6614 respectively are recommended. The $\overline{F_z}$ parameter for fast and high

energy neutron induced fission of ^{235}U appears to be constant at 1.05, but for thermal fission shows variation with nuclear charge, which can be approximated by a straight line

$$\bar{F}_Z = 1.29 - 0.07(Z_f - 92) \quad \bar{F}_Z \geq 1.0 \quad \text{Eqn (6.15)}$$

In a similar fashion $\Delta Z(A'=140)$ shows variation with nuclear charge, which can be approximated for different neutron energies by the following:

$$\Delta Z(A'=140) = -0.55 + 0.03(Z_f - 92) \quad \text{For Thermal} \quad \text{Eqn (6.16)}$$

$$\Delta Z(A'=140) = -0.42 + 0.03(Z_f - 92) \quad \text{For Fast} \quad \text{Eqn (6.17)}$$

$$\Delta Z(A'=140) = -0.23 + 0.03(Z_f - 92) \quad \text{For High Energy} \quad \text{Eqn (6.18)}$$

$$\Delta Z(A'=140) = -0.55 + 0.03(Z_f - 92) \quad \text{For Spontaneous} \quad \text{Eqn (6.19)}$$

It should be noted that the energy and nuclear charge dependencies are assumed independent of each other as only one fission nuclide (^{235}U) has been measured at more than one neutron energy.

Thus, it is possible using the above parameters to estimate the charge distribution parameters for any fissioning system. It should be noted, however, that interpolated or extrapolated values will be less accurate than fitted values.

As only six systems have been actually fitted and the remainder rely on extrapolation or interpolated results it is useful to have a test of the cases using interpolated or extrapolated data to justify the parameters. One test that is highly sensitive to the charge distribution is a summation calculation of the total delayed neutron per fission. This process involves the calculation of $\bar{\nu}_d$ by summing the expected delayed neutron yield based on the P_n value for individual precursors for which the yield is based on the parameters. The results of calculations using these parameters are discussed in chapter 10.

6.4 Other independent yield models

The only other model that is currently used to describe independent yields is the Wahl A_p' model^[6.4]. This is similar to the Z_p model but with a Gaussian distribution over product mass rather than charge. The A_p' model consists of 15 parameters but in Wahl's work this model gave a slightly worse reduced χ^2 for the thermal neutron induced yield of ^{235}U . Wahl also used the number of model calculations within one standard deviation of the experimental results to test the fit. This showed a slight improvement for the A_p' model for this one fissioning system. However for all the other fitted systems the Z_p model showed improvements for both statistics. Due to time constraints this model was therefore not studied.

However recent work by Wahl^[6.11] has shown that the A_p' model can describe some unusual features recently observed experimentally at extreme asymmetric masses. These experiments show that the charge distribution appears to have two separate peaks for very asymmetric masses. When this new experimental data is published it will be interesting to examine the A_p' model to see if it then gives an improvement in the region of extreme asymmetric masses.

6.5 Discussion

At this point it is interesting to discuss the trends found for the Z_p model and to compare these with those developed by Wahl. It is also possible to speculate as to the cause of these charge distribution phenomena.

Wahl^[6.12] used an extrapolation technique based upon the function:

$$P = \alpha + \beta(Z_F - 92) + \gamma(A_F - 236) + \delta(\bar{\nu}_p - 2.42) \quad \text{Eqn (6.20)}$$

where P is the parameter function being extrapolated. The α term being constant, the β

[6.11] Private communication from A.C.Wahl. (1994).

[6.12] "Nuclear mass and charge distributions from fission" by A.C.Wahl, presented at the "50 years with nuclear fission" meeting at Gaithersburg, U.S.A on the 25-28 April 1989.

being charge dependent, the γ being mass dependent and the δ being related to $\overline{v_p}$ which is related to the incident neutron energy (and thus the compound nucleus excitation).

Wahl demonstrated trends in three parameters of the Z_p model as shown in Table 6.7

Table 6.7 Wahl fitting of Z_p parameters to Eqn (6.20)

Parameter	α	β	γ	δ
$\overline{\sigma}_Z$	0.534 ± 0.004	0.016 ± 0.006	-0.007 ± 0.003	0.051 ± 0.015
$\Delta Z(A'=140)$	-0.506 ± 0.012	-0.062 ± 0.020	0.019 ± 0.009	0.068 ± 0.038
\overline{F}_Z	-1.269 ± 0.013	-0.016 ± 0.012	~ 0.0	-0.143 ± 0.039

Within the parameter uncertainties; the UKFY3 fitting could not determine any mass dependence of the parameters whereas Wahl found minor effects.

Wahl found a trend for $\overline{\sigma}_Z$ whereas the few systems fitted in this analysis did not show a consistent trend in mass, charge or energy for this parameter.

Like Wahl the \overline{F}_Z function was found to decrease with increasing excitation energy and increasing nuclear charge. However the $\Delta Z(A'=140)$ function of Wahl decreased with increasing charge and increased with increasing energy. These are the opposite to the effect seen in the UKFY3 fitting.

These effects, however, are of the order of the uncertainties of the parameters and, considering the small range of mass and charge over which fitting was possible for UKFY3, these differences are therefore not unreasonable. It would be useful in future work to seek to extend the range of mass and charge, the most likely candidate system being ^{252}Cf spontaneous fission. This system having a significant number of measurements, but insufficient to produce a reasonable fit. This system would significantly increase the mass and charge ranges of the nuclei undergoing fission allowing more careful studies of these effects on the Z_p parameters.

Any theoretical model that attempts to explain the charge distribution must explain the

trends modelled by the Wahl Z_p model. Thus, if we consider the main terms individually, it is interesting to make qualitative comments on current theories.

The width in the charge distribution could be viewed as a consequence of random neck rupture. Using the Brosa model the neck region where rupture can occur will have a certain mass. If the charge to mass ratio in the neck is similar to that in the overall compound nucleus then the symmetrical channel which has a greater mass width will have a greater charge width. However this disagrees with the results of Wahl and this work where the symmetrical splitting has a smaller width than the asymmetrical. The charge width, using the unchanged charge distribution, could also be calculated as the width of the mass distribution multiplied by the charge to mass ratio for ^{235}U neutron induced fission. This would suggest a charge width of 2.6, which is a factor of five larger than that observed experimentally. This suggests that the neck must be relatively deficient in protons compared to the two fragments.

Turning to the deviation from the Wahl (1988) Z_p model parameter ΔZ . If the charge to mass ratios of the fragments are the same as the compound nucleus, then ΔZ must be zero. However this is not seen except at $A_f/2$ and at $Z_p=50$ (the shell model 50 proton shell closure).

Some of these effects can be explained qualitatively using the following simple model. If the fissioning nucleus is modelled as two conducting spheres joined by a thin wire with the charge as a solely surface charge. Then the charge, if free to distribute between the fragments, can be approximated as being distributed between the two spheres in ratio to the surface area^[6.13], if neck effects are ignored.

As the total mass is proportional to the radius of the nucleus then the total mass of the fissioning nucleus A_f is equal to the volumes of the two fragments (assuming the neck

[6.13] "The Feynman lectures on Physics, Volume II", R.P.Feynman, R.B. Leighton and M.Sands (1966).

has insignificant volume)

$$\alpha \left(\frac{4}{3} \pi r_h^3 + \frac{4}{3} \pi r_l^3 \right) \quad \text{Eqn (6.21)}$$

where α is the density, r_h is the radius of the heavy fragment and r_l is the radius of the light fragment.

As the mass of the light fragment is given by

$$A_l = \alpha \frac{4}{3} \pi r_l^3 \quad \text{Eqn (6.22)}$$

thus the radius of the light fragment is:

$$r_l = \sqrt[3]{\frac{3A_l}{4\pi\alpha}} \quad \text{Eqn (6.23)}$$

The charge on the light fragment is given by

$$Z_l = \beta 4\pi r_l^2 \quad \text{Eqn (6.24)}$$

where β is the charge density of the surface of the spheres.

Thus

$$Z_l = \beta (4\pi) \left(\frac{3A_l}{4\pi\alpha} \right)^{\frac{2}{3}} \quad \text{Eqn (6.25)}$$

Hence the ratio of the light to the heavy fragment charges is given by

$$\frac{Z_l}{Z_h} = \frac{\beta(4\pi)\left(\frac{3A_l}{4\pi\alpha}\right)^{\frac{2}{3}}}{\beta(4\pi)\left(\frac{3A_h}{4\pi\alpha}\right)^{\frac{2}{3}}} = \left(\frac{A_l}{A_h}\right)^{\frac{2}{3}} \quad \text{Eqn (6.26)}$$

Thus, as charge is conserved, $Z_f = Z_l + Z_h$;

$$\frac{Z_f - Z_h}{Z_h} = \left(\frac{A_l}{A_h}\right)^{\frac{2}{3}} \quad \text{Eqn (6.27)}$$

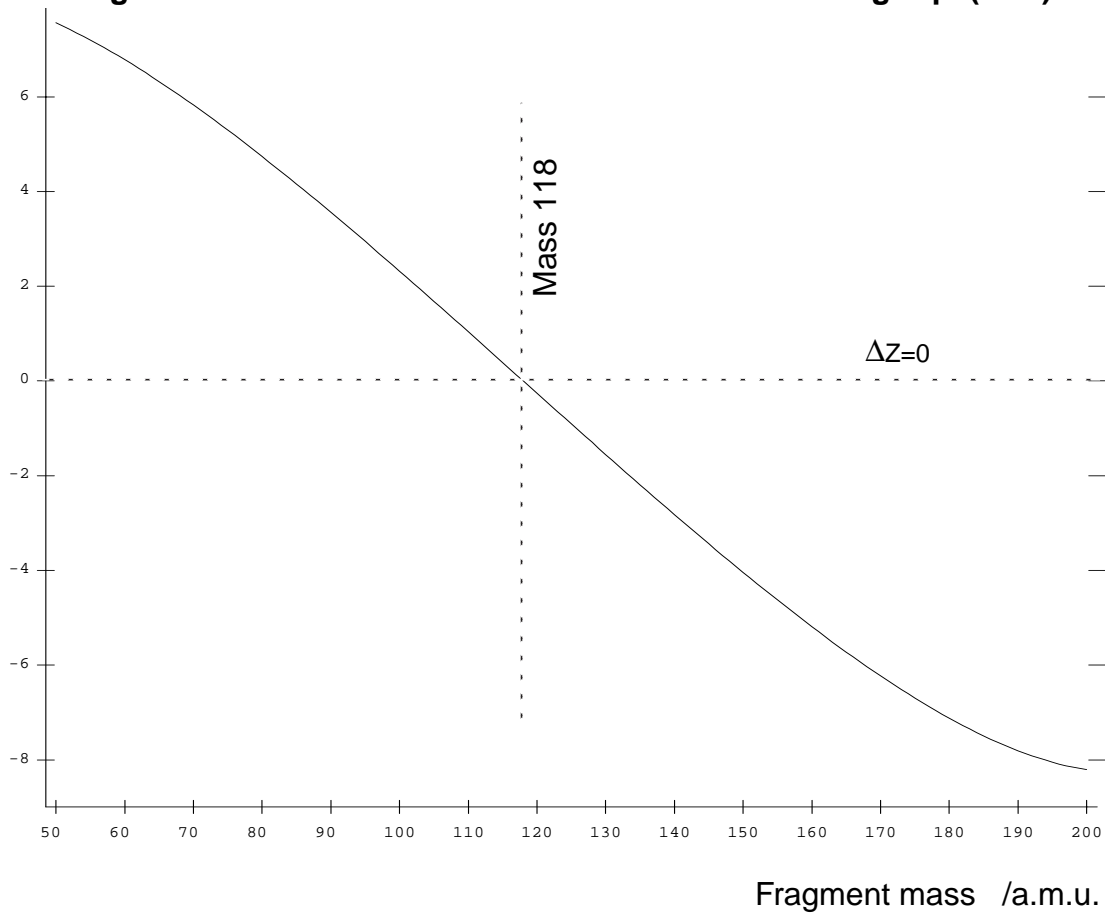
Which simplifies to

$$Z_h = \frac{Z_f}{\left(\frac{A_l}{A_h}\right)^{\frac{2}{3}} + 1} \quad \text{Eqn (6.28)}$$

Thus, for a given mass splitting, the charge can be calculated and hence the mass to charge ratio together with its deviation from the unchanged charge distribution can be determined.

If we consider the thermal neutron fission yields of ^{235}U with the mass split of 96 and 140, Eqn (6.28) give a Z_h of 51.75 and Z_l of 40.25. This gives the ΔZ at mass 140 to be -2.82. As mass is also conserved before the post-scission prompt neutron emission, the ΔZ can be calculated for different mass splits.

Figure 6.4: Calculation of ΔZ for fission of ^{235}U using Eqn (6.28)



This simple model has several interesting features. Firstly the heavy fragment is charge deficient compared to the compound nucleus as shown by experiment. Secondly the data form an almost straight line, as has been shown by Wahl to apply in the asymmetrical region. However the simple model gives a calculated ΔZ which is a factor of six too large and the slope of the ΔZ line is sixteen times the value from experiment.

If on the other hand surface charge is not the total nuclear charge but just a fraction, then the ΔZ will be reduced by this factor. Thus if only a sixth of the charge were mobile and near the surface of the nucleus, modelled as a liquid drop, the effect would now be near the experimental value. However the slope would still be over-estimated by around 50%; this could be explained by the abrupt changes in ΔZ near symmetry shown in Figure 6.3 which appear to be a result of nuclear shell effects.

This model of a conducting sphere has many differences from a real compound nucleus

which consists of a finite number of particles. The coulomb force is dominated by the strong nuclear forces and thus only a small fraction of the charge is on the surface.

The odd-even effect also appears to be directly related to the influence of shell effects on the binding of the proto-fragments. However these odd-even effects, related to the formation of proto-fragments which then fission, have yet to be completely explained by nuclear theory.

7 Independent Yield Isomeric Splitting

7.1 Introduction

In the previous chapters the mass and charge distributions of fission product yields have been examined. To complete the determination of independent yields it is necessary to consider the isomeric states of the product nuclei. The formation of the isomeric state, I , is described in this work by the fraction of the total independent yield of (A,Z) that is formed as the isomer, I . Alternatively the ratio of the independent yields for the metastable and ground states can be used, but this is not useful when more than one isomer of the nuclide exists.

Initially it is necessary to describe and define the isomeric states. Each nucleus of mass A and charge Z will have a set of possible states each with a defining set of quantum numbers as described, for example, by the “Shell Model”^[7.1]. Each of these states will have a characteristic energy level. The state with the lowest energy level is called the ground state (from the German “grund” meaning fundamental). The excited states, with more internal energy than the ground state, can undergo transitions towards the ground state by emitting photons, or to a state of another nuclide by emitting particles.

If there is insufficient energy for an excited nucleus to emit particles directly, i.e. it is in a bound state, then either a particle can quantum-mechanically tunnel from the nucleus (alpha decay) or a photon can be emitted. Emitted photons will carry away from the nucleus excitation energy and angular momentum but not mass. The photon must carry away integral units of angular momentum, so a nucleus can lose excitation energy by emitting a photon if the transition occurs between states which differ by whole units of angular momentum. The probability of such a single transition between two states decreases with increasing difference in angular momentum and decreasing energy difference between the states^[1.7].

Consider fission fragments immediately after fission. The highly excited fragments which

[7.1]“Quantum physics of atoms, molecules, solids, nuclei and particles”, R.Eisberg and R.Resnick, John Wiley and Sons (1974) ISBN 0-471-23464-8

have too many neutrons for stability, high internal energy and high angular momentum will first evaporate off prompt neutrons, each taking ~8 MeV in binding energy. When the fragments have insufficient energy to emit further neutrons the excited nuclei will undergo a cascade of rapid gamma decays towards the ground state. These transitions will occur preferentially between states that differ by one unit of angular momentum until either the nucleus obtains the ground state configuration or only the slower higher order angular momentum transitions with low excitation energy differences are possible.

The excited nuclei can either decay rapidly to the ground state or become “trapped” in states where transitions to lower states have low energy and high angular momentum differences. There is a wide range of state lifetimes from picoseconds to millions of years, but no clear dividing line between “rapid” and “slow” transitions. However, by convention and taking account of the practicalities of measuring decay properties of these states, states with half-lives greater than 1 millisecond are considered as separate identities and are called isomers, or metastable (near stable states).

These metastable states can either undergo slow gamma transitions towards the ground state, or decay by particle emission or electron capture to excited states of other nuclei. If the different possible decay modes have similar probabilities of decay per unit time there is competition between these modes, governed by the rates of internal state transition and quantum mechanical phenomena such as particle interaction.

The different isomers of a nucleus can have considerably different decay properties i.e. decay modes, average decay energies, branching ratios, photon (or particle) emissions and half-lives. The decay data from the JEF2.2 file^[1,8] show isomeric states can vary in half-life from 1.01 ms ($^{184\text{m}}\text{Pt}$) to 3.0 million years ($^{210\text{m}}\text{Bi}$).

There can be also more than one metastable state for a nucleus. Where two metastable states exist, they are usually called the first and second metastable states, and are denoted by m and n respectively. The state numbering is in ascending order of excitation energy from the ground state. This ordering is sometimes difficult to determine where lack of experimental data has not allowed a full determination of the level structure. The JEF2.2 file includes 471 first excited states and 34 second excited states, many of these

isomeric nuclei being within the fission product region.

Isomeric states and their relative yields from nuclear reactions are very important for calculations of nuclide inventory, decay heat and emitted radiations. For integral properties of fission products the individual isomeric splits are not directly important except where only a few fission products contribute to the total result. This may be at long times or, more importantly, for isomers at short times where the integral property is dominated by a few individual nuclides due to their activities. An example of this is the beta decay heat between 10 and 10000 seconds where James^[7.2] whilst studying the effect of decay branching ratios on decay heat calculations for fission bursts showed that for the total decay heat output in this time region the dominant factor was the decay branching of one fission product,¹³⁴I.

Another example of isomeric splitting comes from studies of minor actinide “incineration”. A ground and metastable state of ²⁴²Am both exist and which are formed by neutron capture from ²⁴¹Am^[7.3]. The capture reaction, to both states, has a 2200m/s cross-section of 630.7 barns, for the production of both states. The metastable state decays 99.5% by internal transition to the ground state with a half-life of 141 years. The ground state then decays much faster with a half-life of 16 hours with 82.7% going to ²⁴²Cm and 17.3% to ²⁴²Pu. These nuclides and their daughters contribute to the long and short lived components of spontaneous fission and, depending upon chemical composition, (α,n) reactions. A significant fraction of the neutron emission from the “incinerated” minor actinides after irradiation will depend upon the ratio of the ²⁴¹Am capture reaction to the metastable state. A higher branching to ^{242m}Am will “hold-up” the production of the neutron emitters reducing neutron emission in the short term (under a hundred years) but increasing the emission at longer times. This isomeric splitting ratio will thus directly affect the shielding and handling precautions involved in actinide incineration. These safety precautions will directly affect the cost of such procedures and

[7.2] “The calculation of sensitivities of nuclear inventories and decay power”, M.F. James. NEACRP-302 ‘L’ p289-301 (1987)

[7.3] “Some remarks about the ²⁴¹Am capture cross-sections and branching ratios”, S.Cathalau, R.Soule and A. Benslimane. Private communication (1994).

may determine if this route is a viable method of disposing of actinide waste from the nuclear industry.

7.2 Experimental isomeric splitting data in the UKFY3 database

There exist few experimental data on the independent yields to different isomeric states, but there are a large number of fission products with isomeric states. The JEF2.2 file contains 388 fission product nuclides with two isomers and 21 with three. Thus some model is necessary to produce a complete set of $R(A,Z,I)$ so that independent yield sets can be calculated.

The UKFY3 database contains independent yields for 81 nuclides where at least one metastable state yield as well as the ground state yield has been measured. As discussed in the previous chapter the fractional independent yield analysis has shown a large proportion of discrepant data, especially for yields of isomeric states. Some of these discrepancies may depend upon the identification of the isomeric states. However checks of the data from the measurement as entered into the database and further subsequent checking has failed to clear up such errors. It should be born in mind that some references do not describe the measurements with sufficient detail to be able to see the effect on their analyses of using the latest state designations. Apart from incorrectly identified states, differences can come either from the experimental procedures or the nuclear data used during the course of the measurement (such as branching ratios, half-lives and P_γ 's).

In the UKFY3 database only 17 of the 81 nuclides with multiple isomers have more than one experimental measurement of each state. These multiple measurements allow an external standard deviation to be calculated to act as a check of the data. The ratio of the independent yield of the higher isomer to the total independent yield of the isomer and ground state of a nuclide calculated for these 17 nuclides from UKFY3 are shown in Table 7.1

Table 7.1: Isomeric splitting from the analysed UKFY3 database

System	nuclide	metastable/ Total	Standard deviation
U233T	131-Te-52	0.6755	0.0922
U233T	132-I-53	0.4143	0.0583
U233T	133-Te-52	0.6549	0.1841
U233T	135-Xe-54	0.5866	0.1141
U233T	148-Pm-61	0.7773	0.0907
U235T	128-Sn-50	0.1991	0.1128
U235T	128-Sb-51	0.5606	0.1280
U235T	130-Sb-51	0.5011	0.1202
U235T	131-Te-52	0.6796	0.0900
U235T	132-Sb-51	0.4404	0.0898
U235T	132-I-53	0.3855	0.0629
U235T	133-Te-52	0.6515	0.0966
U235T	134-I-53	0.2922	0.0219
U235T	135-Xe-54	0.6434	0.0579
U235T	136-I-53	0.8026	0.1735
U235T	148-Pm-61	0.0005	0.0008
Pu239T	135-Cs-54	0.6055	0.0658

In the experimental database there also exist direct measurements of the fractional independent yield of metastable relative to the total nuclide yield. These are shown in Table 7.2, the measurement reference numbers are those given in appendix A.5.

Table 7.2 Direct measurements of isomeric splitting ratios

Fissioning nuclide	mode of fission	Product	M/(G+M)	% error	Reference number
Th232	Thermal neutron	134-I-53	0.4700	10.0	2114
Th232	25MeV γ	134-I-53	0.5700	15.0	2083
Th232	Thermal neutron	136-I-53	0.7100	10.0	2114
U233	Thermal neutron	132-I-53	0.2920	30.0	2064
U233	Thermal neutron	134-I-53	0.4920	7.0	2064
U233	Thermal neutron	138-Cs-55	0.5294	3.5	2006
U235	Thermal neutron	90-Rb-37	0.8969	5.0	12945
U235	Thermal neutron	95-Nb-41	0.7519	2.3	2037
U235	Thermal neutron	132-Sb-51	0.1942	34.8	20878
U235	Thermal neutron	132-I-53	0.4460	10.0	2064
U235	Thermal neutron	132-I-53	0.7319	6.8	2037
U235	Thermal neutron	133-Xe-54	0.2593	124.8	30666
U235	25MeV γ	134-I-53	0.5300	10.0	2083
U235	Thermal neutron	134-I-53	0.4120	10.0	2064
U235	Thermal neutron	135-Xe-54	0.6428	2.0	20848
U235	Thermal neutron	135-Xe-54	0.6897	7.2	30666
U238	25MeV γ	134-I-53	0.5200	15.0	2083
Pu239	Thermal neutron	132-Sb-51	0.7519	3.0	20878
Pu239	Thermal neutron	132-I-53	0.4030	10.0	2064
Pu239	Thermal neutron	134-I-53	0.3940	12.0	2064
Pu239	Thermal neutron	135-Xe-54	0.6552	4.1	20848
Pu239	Thermal neutron	138-Cs-55	0.1687	42.2	2006
Pu239	Thermal neutron	138-Cs-55	0.6875	3.8	20848
Pu241	Thermal neutron	132-Sb-51	0.2260	20.0	2075
Pu241	31MeV α	132-Sb-51	0.4630	10.0	2075
Pu241	38MeV α	132-Sb-51	0.4390	20.0	2075
Pu241	Thermal neutron	132-I-53	0.4500	10.0	2064
Pu241	Thermal neutron	134-I-53	0.3620	10.0	2064
Pu241	Thermal neutron	138-Cs-55	0.3500	23.4	2006
Cm245	Thermal neutron	132-I-53	0.4820	10.0	2064
Cm245	Thermal neutron	134-I-53	0.3620	17.6	2064
Cf249	Thermal neutron	132-Sb-51	0.6780	5.2	20878
Cf252	Spontaneous	90-Rb-37	0.7778	3.2	21579
Cf252	Spontaneous	132-I-53	0.5250	10.0	2064
Cf252	Spontaneous	133-Te-52	0.7778	30.0	2073
Cf252	Spontaneous	134-I-53	0.5490	12.0	2064
Cf252	Spontaneous	138-Cs-55	0.5652	9.8	21579

It should be noted that the yields in this table do include discrepant data.

The experimental isomeric splitting data in these two tables can be used to test predictive models.

7.3 Madland and England (M&E) model

The only basic model that currently exists which aims to predict the splitting of the independent yields between isomers without detailed information on nuclear structure is that developed by Madland and England^{[7.4][7.5]}.

To calculate the isomeric ratios precisely would require calculations of the nuclear cascade from the initial fission fragments to the long lived isomeric states^[7.5]. This would require a complete knowledge of the fission fragments, their neutron and gamma emission probabilities and a complete description of the isomeric states of the final nuclides. Although it would be possible to complete such calculations for a few nuclides if reasonable assumptions were made about the fission fragment properties, for most fission product nuclides too few level data exist.

Madland and England therefore developed an approach based upon a statistical model calculation of the fission fragments' average angular momentum. They assumed that $R(A,Z,I)$ is determined by integrals over the distribution $P(J)$ of levels of spin J in the fragment.

The statistical model ^{[7.6][7.7]} predicts

$$P(J) = \text{constant} \times (2J + 1) e^{-\left[\frac{\left(J + \frac{1}{2}\right)^2}{\langle J^2 \rangle} \right]} \quad \text{Eqn (7.1)}$$

where $J_{\text{rms}} = (\langle J^2 \rangle)^{1/2}$ characterizes the angular momentum of the initial fragment.

[7.4] "The influence of isomeric states on independent fission yield production", D.G.Madland and T.R.England. Nuclear Science and Engineering, 64, 859-865 (1977)

[7.5] "Distribution of independent fission product yields to isomeric splitting", D.G.Madland and T.R.England. LA-6595-MS. (1976)

[7.6] H.A.Bethe, Rev. Mod. Phys., 9, 84 (1937).

[7.7] C.Bloch, Phys. Rev., 93, 1094 (1954).

Two further assumptions are needed for the calculation of the isomeric splitting. Firstly, that the parameter J_{rms} is assumed to be constant for all fragment masses in the neutron induced fission of all actinide systems, but to vary with incident energy. Secondly, the branch mechanism is that fragments with J values near to that of the isomeric state value, J_m , gamma decay to the isomeric state and similarly for those near the ground state. The fragments exactly between J_g and J_m divide equally between the two states. The mechanism is dependent on the observation that transitions between states with the smaller ΔJ are always strongest. Madland and England also noted that their model ignores neutron emission from the fragments and quantum mechanical selection rules for transitions.

Thus if $J_m > J_g$ then

$$\frac{y(A, Z, m)}{y(A, Z, g) + y(A, Z, m)} = \frac{\int_{J_c}^{\infty} P(J) dJ}{\int_{0 \text{ or } 1/2}^{\infty} P(J) dJ} \quad \text{Eqn (7.2)}$$

or conversely if $J_m < J_g$

$$\frac{y(A, Z, g)}{y(A, Z, g) + y(A, Z, m)} = \frac{\int_{J_c}^{\infty} P(J) dJ}{\int_{0 \text{ or } 1/2}^{\infty} P(J) dJ} \quad \text{Eqn (7.3)}$$

The isomeric splitting ratio $R(A, Z, I)$ can thus be calculated. The ratio will depend upon whether $J_m < J_g$ or $J_m > J_g$, the fission product mass is odd or even, and $|J_m - J_g|$ is odd or even.

J_c is determined such that fragments exactly between the states divide equally between both. If A is even then the lower limit of the integral is 0 or if odd then 1/2. Also if $|J_m - J_g|$ is odd then $J_c = 1/2 (J_m + J_g + 1)$ or conversely if $|J_m - J_g|$ is even then $J_c = 1/2 (J_m + J_g + 2)$.

Thus eight separate cases must be considered to determine $R(A, Z, m)$ either directly

from Eqn (7.2) if $J_m > J_g$, or as $1 - R(A,Z,g)$ from Eqn (7.3) if $J_m < J_g$. Madland and England^{[7.5][7.4]} derive eight formulae to calculate the ratio, $r(A,Z) = y(A,Z,m)/y(A,Z,g)$.

These formulae, converting to $R(A,Z,m)$, are given in Table 7.3

Table 7.3: Formulae to calculate $R(A,Z,m)$

$J_m > J_g$	A	$ J_m - J_g $	Formulae to calculate $R(A,Z,m)$
yes	odd	even	F_1
yes	odd	odd	F_2
yes	even	even	F_3
yes	even	odd	F_4
no	odd	even	$1-F_1$
no	odd	odd	$1-F_2$
no	even	even	$1-F_3$
no	even	odd	$1-F_4$

where the functions F_1 , F_2 , F_3 and F_4 are given by:

$$F_1 = e^{\left(\frac{1}{\langle J^2 \rangle}\right)} \left(e^{-\frac{1}{\langle J^2 \rangle} \frac{J_m + J_g + 3^2}{2}} + \frac{1}{\langle J^2 \rangle} \frac{J_m + J_g + 1}{2} e^{-\frac{1}{\langle J^2 \rangle} \frac{J_m + J_g + 1^2}{2}} \right) \quad \text{Eqn (7.4)}$$

$$F_2 = e^{\left(\frac{1}{\langle J^2 \rangle}\right)} \left\{ e^{-\left(\frac{1}{\langle J^2 \rangle}\right) \left(\frac{J_m + J_g + 2}{2}\right)^2} \right\} \quad \text{Eqn (7.5)}$$

$$F_3 = e^{-\left(\frac{1}{\langle J^2 \rangle}\right)\left(\frac{J_m + J_g + 2}{2}\right)\left(\frac{J_m + J_g + 4}{2}\right)} + \frac{1}{\langle J^2 \rangle}\left(\frac{J_m + J_g + 1}{2}\right)e^{-\left(\frac{1}{\langle J^2 \rangle}\right)\left(\frac{J_m + J_g}{2}\right)\left(\frac{J_m + J_g + 2}{2}\right)}$$

Eqn (7.6)

$$F_4 = e^{\left(\frac{1}{\langle J^2 \rangle}\right)} \left\{ e^{-\left(\frac{1}{\langle J^2 \rangle}\right)\left(\frac{J_m + J_g + 1}{2}\right)\left(\frac{J_m + J_g + 3}{2}\right)} \right\}$$

Eqn (7.7)

Madland and England determined the J_{rms} by examining ten experiments where thermal neutron induced fission yield measurements had been made for several systems with the metastable state having a spin of 11/2 and the ground state 3/2. As these should all give the same result from their formulae the measured $r(A,Z)$ values were averaged and the J_{rms} value calculated that would give the empirical result. This produced a value of $J_{rms}=7.5 \pm 0.5$ for thermal fission.

Trends in the ^{133}Xe isomeric splitting with neutron energy described in the work of Wolfsberg^[7.8] were interpreted as showing that J_{rms} is proportional to the square root of the neutron kinetic energy and binding energy and thus J_{rms} was determined as 7.5, 7.5, 8.0, 9.0 and 10.0 for neutron energies of 0.0, 0.5, 2.0, 10.0 and 14.0 MeV respectively.

Madland and England used their method and information on the spins of fission product isomers to calculate the $R(A,Z)$ values for a range of nuclides at different incident neutron energies. These results are published in their Los Alamos report^[7.5].

[7.8] "Estimated values of fractional yields from low energy fission and a compilation of measured fraction yields", Laboratory report LA-5553-MS, Los Alamos Laboratories. D.G.Madland and T.R.England (1974)

7.4 The application of the Madland and England model for UKFY2 and UKFY3

The Madland and England formulae were used with the spin values of the isomers from the JEF2.2 decay data file to calculate the $R(A,Z,m)$ values for all fission products at thermal, fast and 14MeV neutron energies with J_{rms} values of 7.5, 8.0 and 10.0 respectively^[1.4].

As described above JEF2.2 includes 21 nuclides with three isomeric states. These were simply calculated by considering the high, medium and low isomer spin values in pairs. The $R(A,Z,high)$ was calculated using a small extension to the M&E model.

As from the definitions the $R(A,Z,I)$ the triplet's high spin ratio is

$$R(A, Z, high) = \frac{y(A, Z, high)}{y(A, Z, low) + y(A, Z, medium) + y(A, Z, high)} \quad \text{Eqn (7.8)}$$

which will be the same as the doublet

$$R(A, Z, high) = \frac{y(A, Z, high)}{y(A, Z, medium) + y(A, Z, high)} \quad \text{Eqn (7.9)}$$

Thus using M&E to calculate the split between the high and medium state gives the value of $R(A,Z,high)$. Similarly the $R(A,Z,low)$ split can be calculated using the medium and low state spins. Finally as the sum of the three splits is unity the $R(A,Z,medium)$ split is calculated as $1 - (R(A,Z,high)+R(A,Z,low))$.

Where the spins of one, or more, of the states were unknown the split was assumed to be 50/50. Similarly where two of the three states had unknown spins 33.3/33.3/33.3 was assumed. It should be noted that if only one of a triplet of states has an unknown spin then it may still be possible to determine a result using the model provided the middle spin is known. In which case one of the $R(A,Z,I)$ values can be determined, but the other two are estimated by splitting the remaining yield.

7.5 Extension of the Madland and England model by Rudstam

Rudstam^[7.9] has recently developed the M&E model by explicitly treating some of the assumptions in detail. In the M&E model it is assumed that fragments with a J nearer to a particular state will feed that state. Rudstam assumes that the probability of a transition that will decrease the excited nucleus spin by one unit of angular momentum is proportional to the density of nuclear states of spin (J-1), and similarly that the probability that the spin will increase is proportional to the density of spin states (J+1). Only transitions of one are assumed due to their much greater probability compared to higher order transitions.

The ratio of the number of nuclear states of spin (J-1) to those of spin (J+1) is denoted by Z(J), defined as

$$Z(J) = \frac{2J-1}{2J+3} e^{\frac{(4J+2)}{J_{nuc}^2}} \quad \text{Eqn (7.10)}$$

where J_{nuc} is a constant for each nuclide.

The relative probability of decreasing the spin state is $Z/(1+Z)$ and as the sum of probabilities for increasing and decreasing must sum to 1 the probability of increasing is $1/(1+Z)$. However this will lead to erroneous results if the excitation of the state and the fragment excitation are not taken into account. Rudstam quotes the example of ¹³¹In which has an isomeric state 4 MeV above the ground state. Thus, as few fragments will have sufficient energy to populate this state, its yield will be greatly reduced from that which would be predicted.

The energy effect is modelled by Rudstam by considering all energies as being equally likely, if the energy is below the maximum fragment energy, E_{max} . This maximum is assumed by Rudstam to be equal to the neutron separation energy, which he approximates to 50 keV, as more excitation will lead to neutron emission. The ground

[7.9] G. Rudstam. Proceedings of a Specialists' meeting on fission product nuclear data, Tokai, Japan, 25-27th May 1992. NEA/NSC, DOC(92)9 p.27 (1992).

state will always be fed if the fragment excitation is below the isomer's excitation E_x . This will happen with a probability of E_x/E_{\max} .

If the spin of the low spin isomer is J_{low} , and $J_{\text{low}}=J-1$, this isomer can be reached by the emission of 1, 3, 5, 7,... gamma rays. The probability of this is proportional to:

$$\frac{Z(J)}{1 + Z(J)} [1 + S_2 + S_4 + \dots] \quad \text{Eqn (7.11)}$$

where the S_2 term has the form $Z/(1+Z)^2$ and the S_4 term $(Z/(1+Z)^2)^2$ etc. These terms will reduce rapidly due to limitations of the available energy.

Similarly if $J_{\text{low}}=J-2$ the probability is given by

$$\frac{Z(J)}{1 + Z(J)} \times \frac{Z(J-1)}{1 + Z(J-1)} [1 + S_2 + S_4 + \dots] \quad \text{Eqn (7.12)}$$

Similar relations are valid for the high spin isomer but with the $Z/(1+Z)$ term replaced by $1/(1+Z)$.

Now as S_2 and S_4 are small terms these can be neglected. Thus $R(A,Z,I)$ can be calculated using the following assumptions. Firstly that if the low-spin isomer is the ground state all $P(J)$ for J smaller than or equal to J_{low} will be assumed to feed the low-spin isomer. Secondly, in the spin range $J_{\text{low}} < J < J_{\text{high}}$ the probabilities are calculated using the functions above. Since in all cases one of the isomers must be reached the sum of the probabilities to both the high and low spin isomers must equal unity. Finally for $J > J_{\text{high}}$ the high spin isomer is assumed to be fed unless the available energy is smaller than E_x .

The $R(A,Z,\text{low})$ is thus given by

$$\sum_{J \leq J_{\text{low}}} P(J) + \frac{E_x}{E_{\text{max}}} \sum_{J \geq J_{\text{low}}} P(J) + \frac{E_{\text{max}} - E_x}{E_{\text{max}}} \sum_{k = J_{\text{low}} + 1}^{J_{\text{high}} - 1} P(k) + N(k) \prod_{m = J_{\text{low}} + 1}^k \frac{Z(m)}{1 + Z(m)} \quad \text{Eqn (7.13)}$$

where $N(k)$ is given by

$$N(k) = \frac{1}{\left(\prod_{m = J_{\text{low}} + 1}^k \frac{Z(m)}{1 + Z(m)} + \prod_{m = k}^{J_{\text{high}} - 1} \frac{1}{1 + Z(m)} \right)} \quad \text{Eqn (7.14)}$$

Similarly if the high spin state is the ground state $R(A,Z,\text{high})$ is given by

$$\sum_{J \geq J_{\text{high}}} P(J) + \frac{E_x}{E_{\text{max}}} \sum_{J \leq J_{\text{high}} - 1} P(J) + \frac{E_{\text{max}} - E_x}{E_{\text{max}}} \sum_{k = J_{\text{low}} + 1}^{J_{\text{high}} - 1} P(k) + N(k) \prod_{m = J_{\text{low}} + 1}^k \frac{Z(m)}{1 + Z(m)} \quad \text{Eqn (7.15)}$$

Rudstam notes that this modified model leaves two parameters J_{rms} and J_{nuc} that need to be determined.

From a database of experimental measurements for the isomeric splitting from thermal neutron induced fission of ^{235}U he fitted the two parameters for even mass nuclides and odd-mass nuclides. The fitting used a least-squares minimization. The resulting J_{rms} values were very similar, 6.5 and 6.0 respectively, so he took the mean 6.25. The J_{nuc} for odd mass nuclides was determined to be 6.0 but 2.0 for even mass nuclides.

It should be noted that J_{rms} and J_{nuc} may be system and neutron energy dependent and

thus these parameters cannot be extended to other systems without more study which would require further measurements. Note that in M&E J_{rms} was extended on very little evidence.

Rudstam^[7.10] is currently analysing new experimental results for fast fission of ^{238}U which will allow further study of the model and an examination of the variation of the parameters to be made.

7.6 Comparison of the models with experimental data

The Madland and England model and the modifications to this by Rudstam have been described. Three sets of calculations of isomeric splitting have been mentioned; the original Madland and England calculations of 1976^[7.5], calculations using the M&E model and JEF2.2 spin assignments^[1.4], and the new method of Rudstam^[7.9].

The UKFY3 experimental yields for isomeric splitting shown in Table 7.1 and Table 7.2 for thermal neutron fission of ^{235}U were used to test these three sets of calculations. These were used for the comparison as this system had a significant number of measurements and Rudstam's results are only available for this fissioning system. It should be noted that the experimental data are inconsistent for some of these nuclides.

Table 7.4 shows the results of the comparison. The measured yields, the three sets of calculations and the ratios of calculated over experiment for these three sets are shown. As can be easily seen from the table none of the calculations fit the data particularly well.

To test the goodness of fit a χ^2 test was used which had the usual form

$$\chi^2 = \sum \frac{(x_{\text{calculated}} - x_{\text{measured}})^2}{\sigma_x^2} \quad \text{Eqn (7.16)}$$

where σ^2 is the estimated measurement standard deviation

[7.10] Private communication from G. Rudstam, Studsvik, Sweden (1993)

Table 7.4: Comparison of thermal neutron fission of ^{235}U measurements with calculations.

Nuclide	Experiment: and UKFY3 evaluated results (E)	C1 Madland and England [7.5] (C1)	M&E model with JEF2.2 spins [1.4] (C2)	C3 Rudstam [7.9] (C3)	C1/E	C2/E	C3/E
Rb90	0.8969 ± 0.0448	0.8079	0.808	0.659	0.901 ± 0.045	0.901 ± 0.045	0.735 ± 0.037
Nb95	0.7519 ± 0.0170	0.1877	0.188	-	0.250 ± 0.006	0.250 ± 0.006	
Sn128	0.1991 ± 0.1128	-	0.701	0.209		3.52 ± 1.99	1.05 ± 0.59
Sb128	0.5606 ± 0.1280	0.6305	0.630	0.192	1.12 ± 0.26	1.12 ± 0.26	0.343 ± 0.078
Sb130	0.5011 ± 0.1202	0.6305	0.576	0.190	1.26 ± 0.30	1.15 ± 0.28	0.38 ± 0.09
Te131	0.6796 ± 0.0900	0.7103	0.517	-	1.05 ± 0.14	0.76 ± 0.10	
Sb132	0.4404 ± 0.0898 0.1942 ± 0.0675	-	0.576	0.190		1.31 ± 0.27 2.97 ± 1.03	0.431 ± 0.088 0.98 ± 0.34
I132	0.3855 ± 0.0629 0.4460 ± 0.0446 0.7319 ± 0.0495	-	0.643	-		1.67 ± 0.27 1.44 ± 0.14 0.879 ± 0.059	
Te133	0.6515 ± 0.0966	0.7103	0.707	0.590	1.09 ± 0.16	1.09 ± 0.16	0.91 ± 0.13
Xe133	0.2593 ± 0.3236	0.7103	0.707	0.603	2.7 ± 3.4	2.7 ± 3.4	2.3 ± 2.9
I134	0.2922 ± 0.0219 0.5300 ± 0.0530 0.4120 ± 0.0412	0.4243	0.424	0.183	1.45 ± 0.11 0.80 ± 0.08 1.03 ± 0.10	1.45 ± 0.11 0.80 ± 0.08 1.03 ± 0.10	0.626 ± 0.05 0.345 ± 0.035 0.444 ± 0.044
Xe135	0.6434 ± 0.0579 0.6428 ± 0.0130 0.6897 ± 0.0496	0.7103	0.707	0.575	1.104 ± 0.099 1.105 ± 0.022 1.030 ± 0.074	1.099 ± 0.099 1.100 ± 0.022 1.025 ± 0.074	0.894 ± 0.080 0.895 ± 0.018 0.834 ± 0.060
I136	0.8026 ± 0.1735	-	0.643	0.391		0.80 ± 0.17	0.49 ± 0.11
Pm148	0.0005 ± 0.0008	0.7008	0.701	0.388	1402 ± 2243	1402 ± 2243	776 ± 1242
reduced χ^2					54819	36571	14671
reduced χ^2 (ignoring the Pm148 measurement)					90.63	63.54	12.71

As two of the sets do not have available values for all of the listed isomers the reduced χ^2 is used to allow the comparison to be made. The reduced χ^2 is defined in this case as χ^2 divided by the number of measurements.

As the ^{148}Pm result is poorly modelled by all the calculations and contributes most of the χ^2 for all sets of calculations I have also calculated χ^2 without this measurement to better judge the differences. The ^{148}Pm yield which has a very small value is still over predicted by Rudstam's calculation by three orders of magnitude, as he noted in his paper^[7.9].

Although the Rudstam results give a considerable reduction of reduced χ^2 the values are still too high to be more than a guide to the value.

7.7 Conclusion and recommendations for the UKFY3 evaluated file

Table 7.4 shows that the results of Rudstam^[7.9] gives a considerable improvement over the one parameter model but still does not fit the data particularly well. Rudstam suggests using experimental data, where it is available, as this will be better than any modelling.

The improvement between the Madland and England values and the calculations in this work are due solely to improvements in the determination of the spins of the isomeric states by more recent decay data measurements.

As the calculations using the Madland and England model and the spin information in the JEF2.2 decay data file can be used to predict the splitting for all the nuclides in all fissioning systems it was decided to use these for calculating UKFY3. There were two alternative methods that were considered. Firstly, use of Rudstam's modifications to the model, however this requires his two parameters to be determined for each fissioning system and currently this has been done only for the thermal neutron fission of ^{235}U . The second alternative is to use the experimental data that exists; however these data contain many discrepancies. Due to time constraints it was not possible to review the experimental data in detail. Thus it was decided that the Madland and England model would be used for UKFY3.

8 Production of UKFY3

8.1 Introduction

In the previous chapters the experimental fission yield data of UKFY3 has been analyzed and modelled. This chapter describes the production of a complete evaluated file from this data. This procedure consisted of three steps. First the experimental data was statistically analyzed. Second the experimental data and models developed from this data were used to produce complete sets of chain and fractional independent yields. Thirdly these data were processed into an adjusted fission product yield file in ENDF-6 format^[8.1]; by being combined, adjusted for physical constraints and then formatted.

The production of UKFY3.0 involved many FORTRAN programmes (23972 lines of source code) that were written during this project. The details of the running of computer codes are given in Appendix A.6.

8.2 Analysis of the data

The experimental data detailed in chapter 2 were processed by the methods described in chapter 3. This procedure was implemented in a code called ANALYSE. This code was used to analyse the data repeatedly for ten iterations, as described in section 3.3.2.

The analysis was checked for convergence by comparing the output files containing the recommended data at each iteration. For UKFY3 the analysis converged at the fifth cycle. The tabulated results of the analysis were then formatted for the appendices using the FOUTPUT code.

8.3 Production of complete data sets of chain and fractional independent yields for UKFY3.0

The analysed data were then combined with model estimates to produce complete ‘unadjusted’ independent yield sets for the same 39 fissioning systems as used for the UKFY2 evaluation. They were chosen based upon FISPIN calculations performed by

[8.1] Report BNL-NCS-44945 “ENDF-102 Data formats and procedures for the evaluated nuclear data file ENDF-6”, July 1990, edited by P.F.Rose and C.L.Dunford.

M.F. James^[8.2] which estimated the fractional fission rates of actinides during and following typical irradiations. Those chosen are shown in Table 8.1^[1.4] and are the nuclides which contributed greater than 0.1% at any time for typical fuels (uranium metal, uranium dioxide and mixed oxide fuels) and for ratings and irradiations for each fuel type that could be achievable in the near future.

Table 8.1 Fissioning systems^a included in UKFY3.0

Maximum fractional fission rate			Spontaneous fission
>10%	1-10%	0.1-1%	
nuclides: 5	2	12	3
U233 TFH U235 TFH U238 FH Pu239 TF Pu241 TF	Pu240 F Cm245 TF	Th232 FH U234 F U236 F Np237 TF Np238 TF Pu238 TF Pu242 F Am241 TF Am242m TF Am243 TF Cm243 TF Cm244 TF	Cf252 S Cm242 S Cm244 S

a. The modes by which fission is possible are signified by the following:
T-Thermal neutrons, F- Fast neutrons, H- 14 MeV neutrons and S- Spontaneous fission

The chain yield files were produced by MKCHAIN code. This code reads the recommended chain yield data produced in the analysis for each of the required systems and then uses the five gaussian model described in chapter 4 to fill the gaps in the experimental data. Where fitting to this model had been possible the fitted values were used to fill gaps, otherwise the UKFY2 extrapolated model parameters were used. The model data in the gaps were forced to agree with the experimental data at the edges of the gaps by a re-normalization factor. This re-normalization factor was linearly interpolated across the gap. The wings of the distribution were re-normalized using the last experimental data points. The program produced a complete file of the chain yields and uncertainties for each fissioning system and also produced a graphs of the chain

[8.2] Private communication from M.F.James, Winfrith, U.K. (1989).

yields against product mass. An example of the graphical output is shown in Figure 8.1.

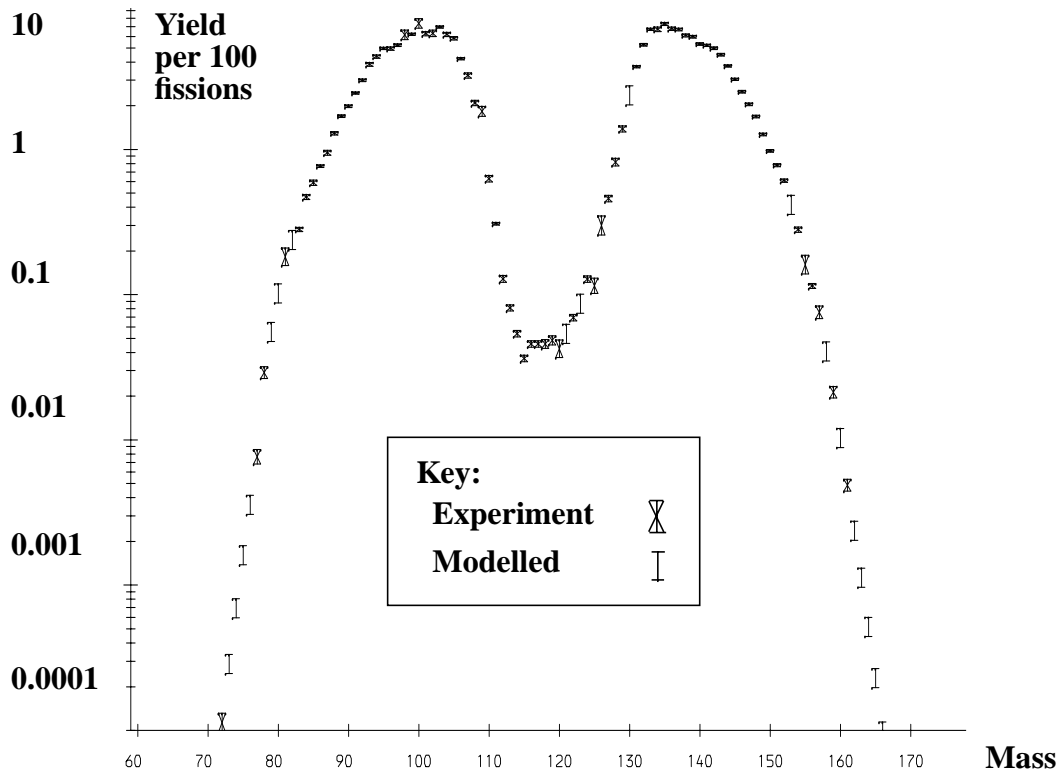


Figure 8.1: Complete chain yield distribution for plutonium-239 fissioned by thermal neutrons, one standard deviation error bars plotted.

For the fractional independent yields a similar procedure using the Wahl Z_p model was used. However due to the large amount of discrepant fractional independent yield data only the model data were used. This was calculated using the same procedures as in the fitting routines described in chapter 6. The fitted parameters or, in their absence, interpolated or extrapolated parameters were used to produce complete fractional independent yield sets by the MKFIND code.

8.4 Calculation of chain and cumulative yields

Given a set of independent yields, in order to generate the cumulative yields it is necessary to follow the fission product decays as all the products and their daughters decay to stability. By definition, the cumulative yield of a nuclide (A, Z, I) is the sum of its own independent yield $y(A, Z, I)$ and the yields of other nuclei decaying to the required nuclide.

Thus, the cumulative yield $c(A,Z,I)$ is given by

$$c(A, Z, I) = y(A, Z, I) + \sum_{(A', Z', I')} b(A', Z', I' \rightarrow A, Z, I) c(A', Z', I') \quad \text{Eqn (8.1)}$$

where $b(A', Z', I' \rightarrow A, Z, I)$ is the fraction of the precursor nuclide (A', Z', I') that decays to (A, Z, I) .

If fission products decay simply by β decay, i.e. there is no transition between mass chains, then for each chain only decay and branching within that mass chain would need to be considered. In practice, however, delayed neutron emission and α decay does occur for the fission products which results in the mass and chain yields changing. Thus, to calculate a chain yield, the branching from higher mass chains needs to be considered. In addition, the existence of isomeric states of fission product nuclides add a further complication as the decay chain can split producing multiple paths of decay.

Provided the cumulative yields of the direct precursors (A', Z', I') have been previously calculated and the decay branching fractions are known the $c(A, Z, I)$ can be calculated using Eqn (8.1). Thus, if the fission products are numbered in such a way that no nuclide later in the list decays to one earlier in the sequence then all yields can be calculated by applying Eqn (8.1) in ascending order up the list.

The ordering of the fission products for such calculations must obey certain constraints. Firstly, as no decay process occurs which leads to gain in mass number, the fission products must be ordered in descending mass order. Secondly, within each mass, the β^- decaying nuclides must be ordered by increasing Z . Similarly the EC/β^+ nuclides must be ordered by decreasing Z ; both sets therefore have the stable nuclides last. Finally, as isomeric transitions descend in energy the states of an isotope (A, Z) must be in order of descending energy levels. These conditions lead to a simple prescription for ordering the fission products.

However, it must be noted that a few nuclides exist that decay by both β^- and EC/β^+ modes. The daughters of such nuclides can then possibly undergo the other form of β

decay. A typical example of this problem is a parent nuclide with both ground and metastable states, with the ground state being stable. If the metastable to ground state transition is forbidden by quantum mechanical selection rules and the metastable state beta decays either way then one, or both, of the daughters can subsequently β decay to the stable ground state of the parent. In such a case the list of fission products cannot be ordered simply by their decay mode. Thus, for this evaluation the initial ordering of nuclides from JEF2.2 was checked to ensure that no decays occurred in the wrong direction in the list. In special cases the list was manually edited.

The chain yields can then be calculated simply by summing the resultant cumulative yields of all stable nuclides within each mass chain (this allows for cases where there are several stable nuclei in a particular mass chain). It must be noted, however, that several fission products exist that α decay; these have half-lives of greater than one million years. If this type of decay is incorporated into the calculation it will subtract the appropriate branching from the chain yield for the parent mass and add to the mass chain four masses below. In practice, however, no yield measurement will observed this transfer of yield due to the human time-scales of the experiment. The JEF2.2 file ^{[1.8],[4.1]} contains 36 fission products with half-lives greater than one thousand years, fifteen greater than 10^{10} years. Of the fission products with half-lives greater than one hour just eight decay to different mass chains, in all cases by α emission. These are listed in Table 8.2.

Table 8.2: Fission product nuclides with half-lives greater than a one hour which α decay.

Nuclide	Half-life /years
58-Ce-142	4.99658E+16
60-Nd-144	2.09858E+15
62-Sm-146	1.03002E+08
62-Sm-147	1.05927E+11
62-Sm-148	6.97138E+15
62-Sm-149	2.00003E+15
64-Gd-150	1.79003E+06
64-Gd-152	1.07926E+14

Thus the decision has been taken, in view of the very long half-lives that the alpha branches of these nuclides should be ignored in the calculation of cumulative and chain yields as it would otherwise interfere with the process of adjustment of yields which is described below. It should be noted that in the very long term cumulative yields of these few nuclides and their daughters will be erroneous. For calculation of these systems the independent yields must be used plus the solution of the full radioactive decay equations. These calculations are usually carried out by a computer code such as FISPIN or ORIGEN^[2.1]. These nuclides are not regarded as a problem given the small number of cases.

8.5 Adjustment of the fission yield files

The adjustment of the fission product yields consists of two stages. The first is related to the definition of mass and chain yields, while the second relates to the physical laws governing fission.

8.5.1 Adjustment of measured chain yields to mass yields

The yield of any nuclide, from Eqn (1.2), is given as:

$$y(A, Z, I) = Y(A) \times f(A, Z) \times R(A, Z, I) \quad \text{Eqn (8.2)}$$

However the chain yield, $Ch(A)$, has been determined in the process just described, not $Y(A)$. If $Y(A)$ is approximated as being equal to $Ch(A)$ then calculation of yields down the chain by following through the branching fractions of the decay of fission products, as described above, will lead to values which differ from the experimental set.^[8.3] This is because some fission product decays, primarily delayed neutron emission, transfer some of the yield to lower mass chains. Thus a set of $Y(A)$ needs to be produced which will give rise to the $Ch(A)$ set when the decays are followed.

The procedure developed in 1993 for the final version of UKFY2 defined a correction term, $\alpha(A)$, where

$$Y(A) = \alpha(A)Ch(A) \quad \text{Eqn (8.3)}$$

If we consider a mass chain a , the nuclides with independent yields $y(a, Z, I)$ decay towards stability. As decay occurs some of the mass yield $Y(a)$ may be lost to lower mass chains and some added to this mass chain from the chains above. Directly after fission the sum of yields for the mass chain is $Y(a)$; by subtracting the loss from the chain, $out(a)$, and adding the gain to the chain, $in(a)$, the chain yield $Ch(a)$ is obtained. Thus,

$$Y(a) - out(a) + in(a) = Ch(a) \quad \text{Eqn (8.4)}$$

Given an initial $Y(a)$ the cumulative yields can be calculated by following through the decays with their respective branching ratios. The resulting estimate of the chain yield $Ch'(a)$ for the $Y(a)$ values, can thus be calculated along with $out(a)$ and $in(a)$.

[8.3] Private communication Jean Blachot, CEN Grenoble and Alan Tobias NE Berkley.

Thus if $Y(a)$ is estimated using an initial guess, α_0 , of the value of α , then

$$\alpha_0 \text{Ch}(a) - \text{out}(a) + \text{in}(a) = \text{Ch}'(a) \quad \text{Eqn (8.5)}$$

Thus an improved estimated α value, α_1 , is required such that $\text{Ch}'(a)$ is equal to $\text{Ch}(a)$:

$$\alpha_1 \text{Ch}(a) - \text{out}(a) + \text{in}(a) = \text{Ch}(a) \quad \text{Eqn (8.6)}$$

Thus rearranging Eqn (8.5) and Eqn (8.6) and then dividing these gives:

$$\alpha_1 = \alpha_0 \left(\frac{\text{Ch}(a) - \text{in}(a) + \text{out}(a)}{\text{Ch}'(a) - \text{in}(a) + \text{out}(a)} \right) \quad \text{Eqn (8.7)}$$

The vector $\alpha(A)$ can thus be calculated. However, in practice, the $\text{in}(A)$ and $\text{out}(A)$ will change with improved knowledge of $Y(A)$ i.e. of $\alpha(A)$. Thus it is necessary to iterate until the $\alpha(A)$ converge. Following convergence, $Y(A)$ and thus the independent yields $y(A, Z, I)$ can be calculated which are consistent with the measured chain yields.

8.5.2 Adjustment relating to physical laws

The second phase of the adjustment procedure is a least-square fit of the evaluated yields to physical constraints which apply to the independent yields. These are defined by the physical laws governing the fission process during the period after prompt neutron emission but before any of the fission products can decay (β^- , β^+ , n , α etc.).

The first constraint is for fission events that do not include light charged particle emission; in which case:

$$\sum_A Y(A) = 2.0 \quad \text{Eqn (8.8)}$$

The second, and related constraint, is that the sum of the yields of the heavy mass peak must equal one, there being both a heavy and a light fragment produced in any fission

event. This can be described by the equation;

$$\sum_{A > \frac{A_f}{2}} Y(A) = 1 \quad \text{Eqn (8.9)}$$

The third constraint is the conservation of mass. When the mass of all the products, both fission products and neutrons, are summed before and after prompt neutron emission for fission events not involving emission of a light charged particle

$$\sum_A AY(A) = A_f - \bar{\nu}_p \quad \text{Eqn (8.10)}$$

where $\bar{\nu}_p$ is the average number of prompt neutrons emitted after fission. For the general case this becomes

$$\sum_A AY(A) = A_f - \bar{\nu}_p - A_{LCP} \quad \text{Eqn (8.11)}$$

where A_{LCP} is the total mass carried away by light charge particle emission.

The fourth constraint is similar, being based on the sum of charge of the products before any radioactive decay

$$\sum_{ZA} Z f(A, Z) Y(A) = Z_f - Z_{LCP} \quad \text{Eqn (8.12)}$$

where Z_f is the charge of the compound nucleus and Z_{LCP} is the total charge carried away by light charge particle emission. It should be noted that for fission induced by charge-less particles, such as neutrons and photons, the compound nucleus charge is the target-nucleus charge.

These four constraints apply to the overall distribution of mass, charge and yield. However, constraints also apply to individual yields; for example, for any individual fission event the fragments must carry away charge equal to the charge of the compound

nucleus. Thus, summing over the mass of the “complementary” elements Z_1 and Z_2 which are produced in one fission event must obey the condition

$$Z_1 + Z_2 = Z_f \quad \text{Eqn (8.13)}$$

and must thus have equal yields. This gives by extension:

$$\sum_A f(A, Z)Y(A) = \sum_A f(A, Z_f - Z)Y(A) \quad \text{for all } Z < \frac{Z_f}{2} \quad \text{Eqn (8.14)}$$

The method of adjustment and the FORTRAN subroutine used in the UKFY2 and UKFY3 evaluation was developed by James^[8.4]. The method is described in detail by James^[1.4]. Firstly the procedure minimizes the four global constraints. Then the set of complementary element constraints are minimized beginning with the pair with the largest combined yield and then in decreasing order. The number of constraints to apply is determined by the reduced χ^2 . The constraints are successively applied until this value is around one or the reduced χ^2 is a minimum. It should also be noted that no yields were allowed to be adjusted below zero; if any yield goes below zero the subroutine halts the programme with an error.

In forcing the yields to fit the constraints, the reduced χ^2 parameter provides an overall measure of the success of the adjustment when compared with the initial yields and uncertainties. A reduced χ^2 of one shows the adjustment is just consistent with the initial set of uncertainties. The independent yield uncertainties are a function of the chain yield and the fractional independent yields uncertainties. The chain yields uncertainties are either derived from the analysis of experimental results or are estimated if modelled values are used. Chain yields of systems which could be fitted were found, on average, to have residuals less than 15% of the measured yield and thus an uncertainty of 15% was assumed. If the system could not be fitted then the values based upon model parameters were used. Studies of yields generated using these extrapolated parameters and measured yields showed a 30% estimate of uncertainty was justified. The fractional

[8.4] Private communication, M.F.James, Winfrith, U.K. (1989)

independent yield modelling was assumed to have an uncertainty of 30%, so that adjustments could be made of up to three standard deviations before sending yields negative. Thus the reduced χ^2 can be used to test the estimated uncertainty of the data, and this was used to adjust the uncertainties of the adjusted data by the method of Birge [3.2]. In addition the least-squares fit process produces a covariance matrix that can subsequently be used to calculate uncertainties of derived parameters such as the cumulative yields.

Table 8.3 shows the final UKFY3.0 mismatches output by the FITFYS code for the constraints after adjustment of the yields from thermal neutron induced fission of ^{235}U . Each of the constraints are defined such that they should equal zero. The results of the FITFYS show the constraints are well fitted. The χ^2 value in this fit is very low which could mean the quoted uncertainties are approximately five times too large, which is unlikely considering the uncertainties on the experimental data and the Z_p model fits.

The $\bar{\nu}_p$ values used for the UKFY2 and UKFY3.0 evaluations are given in Table 8.4. These values are taken in preferred order from E.J.Axton^[8.5], JEF1^[8.6] and S.F.Mughabghab^[8.7]. As in some cases only the $\bar{\nu}$ were determined the delayed $\bar{\nu}_d$ values taken from R.J.Tuttle^[8.8] were used to convert total to prompt.

[8.5] E.J.Axton. Report GE/PH/01/86 from Geel, Belgium (1986).

[8.6] Joint evaluated file version 1, available from the NEA Data Bank.

[8.7] "Neutron Cross-sections Part B Z=61-100", S.F.Mughabghab, Academic Press, New York (1984).

[8.8] R.J.Tuttle, Nuclear Science and Engineering, 56, 37 (1975).

Table 8.3: Final mismatches for the UKFY3 adjustment of yields from the thermal neutron fission of ^{235}U

Constraint number	Constraint	Value of fitted constraint	
1	$\sum_A Y(A) - 2$	-3.962E-15	
2	$\sum_{A > \frac{A_f}{2}} Y(A) - 1$	-4.851E-15	
3	$\sum_A A Y(A) - A_f + \bar{\nu}_p + A_{LCP}$	-2.010E-05 +/- 3.0E-04 $\bar{\nu}_p$ calculation: CALC = 2.41688 +/- 0.00030 EXPT = 2.41690 +/- 0.00360	
4	$\sum_{ZA} (Z.f(A, Z)Y(A)) - Z_f + Z_{LCP}$	-4.016E-07	
COMPLEMENTARY ELEMENTS. CONSTRAINTS:8 pairs fitted. Sum of fitted yields = 1.886			
Constraint number	Element pairs	Sum of complementary element yields	SUM OF EL. YIELDS HEAVY YIELD-LIGHT YIELD
5	Z= 54& 38	3.965E-01	-4.086E-16
6	Z= 52& 40	3.620E-01	-1.422E-16
7	Z= 56& 36	3.129E-01	1.170E-16
8	Z= 53& 39	2.375E-01	3.528E-16
9	Z= 55& 37	2.288E-01	4.656E-16
10	Z= 51& 41	1.483E-01	1.667E-19
11	Z= 57& 35	1.140E-01	9.696E-17
12	Z= 58& 34	8.565E-02	-8.777E-17
*CHI-SQ=6.588E-01 FOR 12 D.O.F., REDUCED CHI-SQ =5.490E-02 BIRGE FACTOR RB=2.343E-01			

Table 8.4: $\bar{\nu}_p$ values used for UKFY2 and UKFY3

Nuclide	Thermal	Fast	High	Spontaneous
^{232}Th		2.269 ± 0.01	4.008 ± 0.02	
^{233}U	2.4884 ± 0.004	2.5153 ± 0.01	4.2959 ± 0.02	
^{234}U		2.7464 ± 0.05		
^{235}U	2.4169 ± 0.036	2.4648 ± 0.01	4.3844 ± 0.02	
^{236}U		2.6869 ± 0.05		
^{238}U		2.7355 ± 0.007	4.4280 ± 0.012	
^{237}Np	2.5218 ± 0.05	2.600 ± 0.07		
^{238}Np	2.772 ± 0.05	2.846 ± 0.05		
^{238}Pu	2.8909 ± 0.02	2.965 ± 0.05		
^{239}Pu	2.876 ± 0.0051	2.9443 ± 0.015		
^{240}Pu		3.2268 ± 0.01		
^{241}Pu	2.9307 ± 0.006	3.0025 ± 0.015		
^{242}Pu		3.219 ± 0.015		
^{241}Am	3.213 ± 0.032	3.255 ± 0.07		
$^{242\text{m}}\text{Am}$	3.260 ± 0.024	3.302 ± 0.07		
^{243}Am	3.214 ± 0.038	3.256 ± 0.07		
^{242}Cm				2.532 ± 0.012
^{243}Cm	3.430 ± 0.047	3.475 ± 0.08		
^{244}Cm	3.48 ± 0.08	3.526 ± 0.08		2.69 ± 0.01
^{245}Cm	3.711 ± 0.06	3.756 ± 0.08		
^{252}Cf				3.7590 ± 0.0048

8.6 Production of the UKFY3.0 file

The production of the UKFY3.0 file consisted of taking the analysed data with gaps filled by models and adjusting the independent yield to fit the constraints. To determine the number of constraints to apply the code FITFYS_SCAN was run. This produced a list of the reduced χ^2 and mismatches at each step of the adjustment as 25 constraints were applied one after the other. The number of constraints to apply were chosen to be such

that the reduced χ^2 was not significantly greater than one but the largest possible number of constraints applied.

Table 8.5: Number of constraints applied in the adjustment of UKFY3

Nuclide	Thermal neutron induced fission		Fast neutron induced fission		High energy (14 MeV) neutron induced fission		Spontaneous fission	
	No.	reduced χ^2	No.	reduced χ^2	No.	reduced χ^2	No.	reduced χ^2
²³² Th			9	4.742	11	4.633		
²³³ U	15	1.095	12	0.8952				
²³⁴ U			12	1.173				
²³⁵ U	12	0.0549	12	1.118	12	1.462		
²³⁶ U			11	0.2868				
²³⁸ U			11	2.963	11	4.982		
²³⁷ Np	11	5.164	13	2.212				
²³⁸ Np	11	2.843	13	3.087				
²³⁸ Pu	7	1.741	17	4.330				
²³⁹ Pu	14	0.9654	11	3.067				
²⁴⁰ Pu			10	1.276				
²⁴¹ Pu	10	3.090	13	2.72				
²⁴² Pu			12	2.033				
²⁴¹ Am	8	1.455	13	3.863				
^{242m} Am	13	2.606	13	2.433				
²⁴³ Am	13	3.183	13	2.659				
²⁴² Cm							15	3.068
²⁴³ Cm	12	3.313	13	2.396				
²⁴⁴ Cm	13	2.577	13	3.434			14	4.729
²⁴⁵ Cm	14	6.026	13	1.788				
²⁵² Cf							17	1.348

It should be noted that the better the consistency of the data due to good modelling and well defined measured data, the lower the reduced χ^2 . Thus a small value suggests the modelling and the estimates of uncertainties are good. A large value, especially when applying the global constraints, suggests that the modelling or data is unrealistic.

Table 8.4 shows the number of constraints that it was decided to apply for the production of the UKFY3 evaluated file and the resultant reduced χ^2 . It should be noted that the system with the best defined and modelled data is the ^{235}U thermal neutron induced fission yield set. This has the minimum reduced χ^2 value of all the systems, however this value is surprisingly low.

The code FITFYS was then run using the selected number of constraints given in Table 8.5. This code produces complete sets of adjusted independent yields.

To produce the complete sets of independent and cumulative yields the code DECAY_PROG was used. This reads in the adjusted independent yields with the isomeric splitting ratios and JEF2.2 decay data to produce the cumulative yields.

This code produces ENDF-6 formatted data sections which include the adjusted independent and cumulative yields with their associated uncertainties. To generate the cumulative yield uncertainties the code uses the covariance matrix from the least-squares fit to produced the uncertainties on the cumulative yields using a matrix technique developed by M.F.James^[1.4].

8.6.1 Calculation of cumulative yields and their uncertainties

If the fission products are numbered by the ordering described above then Eqn (8.1) can be rewritten as:

$$c_i = y_i + \sum_j b_{j \rightarrow i} c_j \quad \text{Eqn (8.15)}$$

or in a matrix form

$$c = y + \bar{b}c \quad \text{Eqn (8.16)}$$

This can be rearranged to give

$$(1 - \bar{b})c = y \quad \text{Eqn (8.17)}$$

or

$$c = Qy \quad \text{Eqn (8.18)}$$

where

$$Q = (1 - \bar{b})^{-1} \quad \text{Eqn (8.19)}$$

Then if a change δy in y produces a change δc in c ,

$$\langle \delta c \delta \bar{c} \rangle = Q \langle \delta y \delta \bar{y} \rangle \bar{Q} \quad \text{Eqn (8.20)}$$

The variance of c_i is thus given by

$$\langle \delta c_i^2 \rangle = \sum_{j, k} Q_{i, j} Q_{i, k} \langle \delta y_j \delta y_k \rangle \quad \text{Eqn (8.21)}$$

The covariance terms are calculated in the DECAY_PROG code by calling the FITFYS routine as a subroutine. The Q matrix therefore needs to be determined to calculate the variances on the cumulative yields. The Q matrix is calculated from the decay data; its definition in Eqn (8.19) implies that it is a lower triangular matrix with $Q_{ij} = 0$ if $j > i$, diagonal terms $Q_{ii}=1$ and, for $j < i$,

$$Q_{ij} = \sum_{k=j+1} b_{j \rightarrow k} Q_{ik} \quad \text{Eqn (8.22)}$$

If, for a given value of i , Q_{ij} is calculated successively for $j=i-1, i-2, \dots, 1$, the values of Q_{ik} on the right hand side of Eqn (8.22) will always be known.

Since the entire independent yield of nuclide i contributes to its cumulative yield, $Q_{i,i} = 1$. Also, if none of nuclide j decays through i , then $Q_{i,j}$ is equal to zero; thus, in the specified ordering, such that no nuclide decays to a nuclide lower in the list, $Q_{i,j}$ is zero if $j > i$.

The Q matrix was calculated using the JEF2.2 decay data by the code MAKEP.

The final step in the production of the library was formatting of the data from separate ENDF-6 data structures produced by the DECAY_PROG code into a single complete ENDF-6 library. This was done by the MKUKFY3 code. The resultant library was checked to ensure that it obeyed the appropriate ENDF-6 conventions and physical constraints by using the ENDF-6 checking, listing and plotting codes PSYCHE, LISTEF, PLOTEF and CHECKR^[8.9].

[8.9] ENDF/B-6 utility codes received from the NEA Data Bank.

9 Testing and Benchmarking of Evaluated Files.

9.1 Introduction

In the previous chapter the production of the UKFY3.0 evaluated file was described. The confidence which can be held in the validity of this, or any other evaluated nuclear data file, depends upon the tests that are applied to the data. These tests can be of two types. The first type are tests of internal consistency which are based upon the intrinsic physics or the empirical data on which the evaluation is based. The second type is where the data is used to model a phenomenon based upon a real situation and the results of these calculations are compared with experimental measurements. The first type can be referred to as internal tests and the second as external tests.

It should be noted that in any test care must be taken as to what parameter or procedure is being tested. An example of this problem is in confirming the conservation of charge for independent yields in the file. A close agreement between (i) the sum over all yields of the product of the independent yield and the fission product charge with (ii) the charge of the compound nucleus can be used to test fission product evaluations. However, as in all the other current evaluations of fission yields, charge conservation is forced by adjustment: therefore the only conclusion that can be drawn is that the processing codes are operating successfully. It is not possible to draw any conclusions from this test on the validity of the data.

The range of internal tests are limited to the physical laws that apply and comparisons of the experimental yields input to the evaluation with the adjusted outputs.

The range of external tests that can be applied is as large as the range of applications for fission product yields. However these tests will inevitably involve a wide range of other nuclear data. For example to calculate the fission product inventory within a spent fuel rod it is necessary to know both initial composition of the rod, the rod's irradiation history and the relevant nuclear data (the actinide cross-sections, fission products yields, fission product cross-sections and half-lives of the materials present). Any discrepancy between calculation and measurement could result from each of the different types of nuclear data, or from the approximations inherent in the computer model and code used to

calculate the inventory. Also, parameters such as decay heat, photon and particle emission subsequently derived from the calculated inventory will thus be dependent both upon the many types of data used both to calculate the inventories and the data used to calculate the property in question such as half-lives, P_γ , P_n , average energy per decay etc.

These external tests of validity for a specific application are often called benchmarks. In safety related calculations a series of benchmarks are used to justify to the legally appointed regulators that a procedure is safe. An example of this is criticality safety calculation for the transport of spent nuclear fuel.

An important point to high-light for any testing is the consistency of all the files used. A simple example of data consistency would be the measurement of a fission yield by a characteristic gamma-ray emission. If the P_γ is over-estimated then the yield derived from the measurement will be under-estimated. However if the small yield is used with the large P_γ then a further estimation of gamma emission will approximate to that measured experimentally. This is a case of correlation between the measured yield and the P_γ that cancels out when re-calculating the measured gamma emission.

An important example of consistency related to fission yield evaluation is the decay data set used within the evaluation procedure. If the decay data set used with the yields for inventory calculations has different P_n values from that used in the generation of the yield file then the internal consistency of the independent yields with the experimental chain yields will be lost and those long lived-fission products which have delayed neutron emitting precursors will be incorrectly calculated. This is even though these long-lived radio-nuclides are the most accurately measured.

Also, if the decay data set does not contain all the fission products in the yield set then the inventory calculations cannot estimate the spent fuel inventory correctly. The JEF2.2 and UKFY3 files are adjusted so that when used with the JEF2.2 decay data file they will reproduce the measured chain yields.

9.2 Internal consistency of the evaluated files

The first test of the file is that the evaluated file agrees with the experimental data that is input to the evaluation and, for well known yields, with previous evaluations. This is especially important for the yields of “standard” nuclides used in the measurement of other yields, and for nuclides that are of special interest for applications purposes. The comparison below considers a set of yields that includes the measurement standards ^{99}Mo and ^{140}Ba , along with a short list of nuclides important for applications: ^3H , ^{140}La , ^{148}Nd , ^{85}Kr , ^{106}Ru , ^{134}Cs , ^{137}Cs and ^{129}I .

^3H , ^{85}Kr and ^{129}I are radio-nuclides which are the most important releases to the environment from spent fuel reprocessing. These yields are thus important for estimating the radiation dose uptake to the populace from future reprocessing.

^{140}La , which has virtually the same yield as the ^{140}Ba , is short-lived with a half-life of 1.68 days and is fed by the ^{140}Ba decay with a half-life 12.7 days. This nuclide is important in that it emits a high energy gamma-ray of 1.6 MeV which is easy to detect from a fuel rod. It is used to verify that fuel rods about to be reprocessed have been sufficiently cooled that they do not contain the short-lived, highly active and volatile iodines, the presence of which could increase employee radiation dose uptake. A second use of this nuclide is in reactor experiments. As the equilibrium level of ^{140}La , and thus the 1.6 MeV gamma-ray emission, is related to the average neutron flux it allows estimate of a reactor’s neutron flux to be made during experiments.

^{148}Nd is chosen as it is used for destructive burnup assay while the ^{106}Ru , ^{134}Cs and ^{137}Cs are commonly used for non-destructive gamma-ray spectrometry burnup assay. It should be noted that ^{134}Cs is mostly formed by neutron capture of other fission products and thus the fission yield of this nuclide is less important in the calculations.

The cumulative yields of these nuclides are compared for the three main fissioning systems in current reactors; the thermal neutron fission of ^{235}U and ^{239}Pu , and the fast neutron fission of ^{238}U . These yields are shown in Table 9.1, Table 9.2 and Table 9.3 respectively. The comparison is made between the best estimate of the value based on

the experimental results used in the UKFY2 and UKFY3 evaluations, and the value in the JEF2.2, UKFY3 and ENDF/B-VI evaluated files. A “-” in the tables signifies that no experimental, or calculated, value is available from the respective source.

Table 9.1: Different estimates of cumulative yields, per 100 fissions, for the thermal fission of ^{235}U .

Nuclide	UKFY2 Evaluation	UKFY3 Evaluation	JEF2.2 File	UKFY3.0 File	ENDF/B-VI File
$^3\text{H} \times 10^2$	1.004 ± 0.02	0.931 ± 0.04	1.004 ± 0.03	0.931 ± 0.05	-
^{85}Kr	1.327 ± 0.012	1.327 ± 0.012	1.327 ± 0.033	1.329 ± 0.061	1.319 ± 0.005
^{99}Mo	6.161 ± 0.049	6.126 ± 0.055	6.177 ± 0.066	6.160 ± 0.050	6.109 ± 0.061
^{106}Ru	0.407 ± 0.009	0.409 ± 0.009	0.407 ± 0.015	0.4092 ± 0.018	0.402 ± 0.005
^{129}I	0.779 ± 0.032	0.707 ± 0.032	0.782 ± 0.031	0.708 ± 0.032	0.543 ± 0.005
$^{134\text{g}}\text{Cs}^{\text{a}} \times 10^5$	1.66 ± 0.27	1.66 ± 0.27	2.031 ± 0.76	1.210 ± 0.66	0.771 ± 0.49
^{137}Cs	6.236 ± 0.062	6.211 ± 0.056	6.244 ± 0.539	6.246 ± 0.247	6.188 ± 0.031
$^{140}\text{Ba}^{\text{b}}$	6.268 ± 0.063	6.341 ± 0.057	6.277 ± 0.075	6.375 ± 0.025	6.220 ± 0.031
^{148}Nd	1.674 ± 0.015	1.680 ± 0.010	1.675 ± 0.017	1.680 ± 0.067	1.674 ± 0.006

a. shielded nuclide, only independent yield measured

b. cumulative yield of barium and lanthanum mass 140 are indistinguishable within uncertainty.

Table 9.2: Different estimates of cumulative yields, per 100 fissions, for the thermal fission of ^{239}Pu .

Nuclide	UKFY2 Evaluation	UKFY3 Evaluation	UKFY2 File	UKFY3.0 File	ENDF/B-VI File
$^3\text{H} \times 10^2$	1.471 ± 0.037	1.442 ± 0.076	1.471 ± 0.056	1.442 ± 0.114	-
^{85}Kr	0.566 ± 0.011	0.59 ± 0.24	0.568 ± 0.013	0.593 ± 0.025	0.574 ± 0.002
^{99}Mo	6.183 ± 0.049	6.205 ± 0.050	6.179 ± 0.36	6.181 ± 0.374	6.212 ± 0.087
^{106}Ru	4.199 ± 0.067	4.209 ± 0.076	4.184 ± 0.069	4.184 ± 0.085	4.350 ± 0.087
^{129}I	1.388 ± 0.068	1.388 ± 0.068	1.403 ± 0.067	1.411 ± 0.067	1.371 ± 0.056
$^{134\text{g}}\text{Cs}^{\text{a}} \times 10^5$	-	-	56 ± 15	68 ± 25	67 ± 43
^{137}Cs	6.506 ± 0.012	6.700 ± 0.074	6.509 ± 0.523	6.724 ± 0.539	6.607 ± 0.033
$^{140}\text{Ba}^{\text{b}}$	5.296 ± 0.053	5.320 ± 0.053	5.285 ± 0.053	5.319 ± 0.104	5.354 ± 0.075
^{148}Nd	1.694 ± 0.025	1.684 ± 0.015	1.689 ± 0.025	1.679 ± 0.033	1.642 ± 0.008

a. shielded nuclide, only independent yield measured

b. cumulative yield of barium and lanthanum mass 140 are indistinguishable within uncertainty.

Table 9.3: Different estimates of cumulative yields, per 100 fissions, for the fast fission of ^{238}U .

Nuclide	UKFY2 Evaluation	UKFY3 Evaluation	UKFY2 File	UKFY3.0 File	ENDF/B-VI File
$^3\text{H} \times 10^2$	no value ^a	no value ^a	16.2± 6.3	1.03± 0.32	-
^{85}Kr	0.814 ± 0.124	0.850± 0.094	0.92± 0.14	0.91± 0.18	0.743± 0.007
^{99}Mo	6.242 ± 0.087	6.253± 0.087	6.23± 0.62	6.20± 0.71	6.168± 0.086
^{106}Ru	2.573 ± 0.167	2.542± 0.104	2.55± 0.27	2.48± 0.37	2.490± 0.035
^{129}I	0.619 ± 0.03	0.618± 0.030	0.623± 0.048	0.624± 0.060	1.011± 0.081
$^{134g}\text{Cs}^b \times 10^5$	no value	no value	0.019± 0.009	0.011± 0.007	0.064 ± 0.041
^{137}Cs	5.992± 0.090	6.088± 0.091	6.01± 0.25	6.29± 0.33	6.053± 0.061
$^{140}\text{Ba}^c$	5.783± 0.035	5.943± 0.053	5.74± 0.41	6.09± 0.71	5.815± 0.041
^{148}Nd	2.281± 0.032	2.281± 0.032	2.28± 0.15	2.25± 0.26	2.113± 0.015

- a. There is one measurement of this yield (0.162±0.063), but the measurement is average of several different analyses which differed by orders of magnitude. Thus this data is not used, although it is included in Appendix A.1.
b. shielded nuclide, only independent yield measured
c. cumulative yield of barium and lanthanum mass 140 are indistinguishable within uncertainty.

To examine the adjustment of the UKFY3 yields and to compare the different evaluated files to the UKFY3.0 evaluation the results above are shown below as a fraction of the evaluated UKFY3 values. Values which differ by more than one (or three) standard deviation from the UKFY3 evaluation are highlighted by stars.

Table 9.4: Comparison of cumulative yields, per 100 fissions, for the thermal fission of ^{235}U relative to the UKFY3 value.

Nuclide	UKFY2 Evaluation	UKFY3 Evaluation	UKFY2 File	UKFY3.0 File	ENDF/B-VI File
^{85}Kr	1.0000	1.0000 ± 0.0090	1.0000	1.0015	0.9940
^{99}Mo	1.0057	1.0000 ± 0.0090	1.0083	1.0056	0.9972
^{106}Ru	0.9951	1.0000 ± 0.0220	0.9951	1.0005	0.9829
^{129}I	1.1018*	1.0000 ± 0.0453	1.1061*	1.0014	0.7680***
^{137}Cs	1.0040	1.0000 ± 0.0090	1.0053	1.0056	0.9963
$^{140}\text{Ba}^a$	0.9885	1.0000 ± 0.0090	0.9899	1.0054	0.9809*
^{148}Nd	0.9964	1.0000 ± 0.0060	0.9970	1.0000	0.9964

- a. cumulative yield of barium and lanthanum indistinguishable within uncertainty.
* differs from UKFY3 by more than one UKFY3 standard deviation *** differs by greater than three

Table 9.5: Comparison of cumulative yields, per 100 fissions, for the thermal fission of ^{239}Pu relative to the UKFY3 value.

Nuclide	UKFY2 Evaluation	UKFY3 Evaluation	UKFY2 File	UKFY3 File	ENDF/B-VI File
^{85}Kr	0.9593	1.0000 ± 0.4068	0.9627	1.0051	0.9729
^{99}Mo	0.9965	1.0000 ± 0.0081	0.9958	0.9961	1.0011
^{106}Ru	0.9976	1.0000 ± 0.0181	0.9941	0.9941	1.033*
^{129}I	1.0000	1.0000 ± 0.0490	1.011	1.017	0.9878
^{137}Cs	0.9710*	1.000 ± 0.0110	0.9715*	1.0036	0.9861*
$^{140}\text{Ba}^a$	0.9955*	1.000 ± 0.0010	0.9934*	0.9998	1.0064***
^{148}Nd	1.0059	1.0000 ± 0.0089	1.0030	0.9970	0.9751

a. cumulative yield of barium and lanthanum indistinguishable within uncertainty.

* differs from UKFY3 by more than one UKFY3 standard deviation *** differs by greater than three

Table 9.6: Comparison of cumulative yields, per 100 fissions, for the fast fission of ^{238}U relative to the UKFY3 value.

Nuclide	UKFY2 Evaluation	UKFY3 Evaluation	UKFY2 File	UKFY3 File	ENDF/B-VI File
^{85}Kr	0.9576	1.0000 ± 0.1106	1.0824	1.0706	0.8741*
^{99}Mo	0.9982	1.0000 ± 0.0139	0.9963	0.9915	0.9864
^{106}Ru	1.0122	1.0000 ± 0.0409	1.0031	0.9756	0.9795
^{129}I	1.0016	1.0000 ± 0.0485	1.0081	1.0097	1.6359***
^{137}Cs	0.9842*	1.0000 ± 0.0149	0.9871	1.0332*	0.9943
$^{140}\text{Ba}^a$	0.9731*	1.0000 ± 0.0089	0.9658*	1.0247*	0.9785*
^{148}Nd	1.0000	1.0000 ± 0.0140	0.9996	0.9864	0.9263***

a. cumulative yield of barium and lanthanum indistinguishable within uncertainty.

* differs from UKFY3 by more than one UKFY3 standard deviation *** differs by greater than three

As can be seen from these tables only in the fast neutron fission of ^{238}U have the UKFY3 values been adjusted by more than one standard deviation. These results suggest that for this fissioning system the region around mass 140, on the high mass peak, may be underestimated in the UKFY3 analysis of experimental data, or that the estimated uncertainty is too low. A large portion of the measurements for these two nuclides (^{137}Cs and ^{140}Ba) are based upon a single reference by Ford and Norris^[9.1] which collected

[9.1] Report LA-6129. "A compilation of yields from neutron fission of ^{232}Th , ^{235}U , ^{238}U etc." G.P.Ford and A.E.Norris, Los Alamos, U.S.A. (1976)

together previously unpublished Los Alamos measurements. Although no direct duplications of measurements could be found in the UKFY3 database it is possible some of this data is duplicated or correlated, thus giving rise to an over-optimistic estimate of the uncertainties.

The comparisons between ENDF/B-VI and UKFY3.0 mostly show agreement within three standard deviations. However some of these important nuclides (^{129}I , ^{140}Ba and ^{148}Nd) differ by more than three standard deviations for some of these systems. This suggests that detailed study of these discrepancies should be made and, if this fails to identify a cause, new experimental results should be commissioned.

The second type of internal test is checking that physical conservations maintained during the fission process are conserved in the file. Table 9.7 shows tests of the global constraints for these three main fissioning systems. These constraints are that: the sum of all independent yields sums to two (ignoring the ternary yields), charge is conserved and mass is conserved. The mass conservation is tested by calculating the mass lost, which should equal the average number of prompt neutrons emitted during fission.

Table 9.7: Test of global constraints for UKFY3.0 file

Fission system	Sum of binary yield - 2.0	Sum of yield charge	Calculated $\bar{\nu}$	Evaluated $\bar{\nu}$ from Table 8.4
U235T	2.62×10^{-6}	92.0000	2.4167	2.4169 ± 0.036
U238F	5.12×10^{-6}	92.0109	2.7274	2.7355 ± 0.007
Pu239T	2.38×10^{-6}	93.9999	2.8757	2.8760 ± 0.0051

However as in this work these constraints are forced by the adjustment procedure this only shows how well the adjustment procedure is processing the data when producing the evaluated files.

9.3 External consistency of the evaluated files

As discussed above external tests can be very wide ranging but are also very dependent on the other nuclear data used. Two types of calculations were chosen to test the evaluated fission yield data, both of which only require the decay data to be known. The first test is calculation of delayed neutron emission. This is dominated by a set of nuclides with half-lives of less than a minute. The second is the calculation of decay heat from fission products; this covers both short and long lived nuclides. In both cases very low values of neutron flux were assumed in the modelling so that cross-section effects could be ignored.

9.3.1 Delayed neutron calculations

If we consider delayed neutron emission from fission products, the governing phenomenon is the decay of a fission product that leaves a daughter nucleus with sufficient excitation energy to throw off a neutron. For nuclides where this occurs the fraction of decays that produce a neutron is called the P_n value; these nuclides are short-lived and on the neutron rich side of the line of stability.

The total number of delayed neutrons per fission, $\bar{\nu}_d$, and the time dependence of the delayed neutron emission rate are important parameters for reactor design and safety studies, as they determine the kinetic response and behaviour of reactors. There exist three ways of determining $\bar{\nu}_d$; firstly experimentally from integral measurements e.g. Keepin^[9.2], secondly from summation calculations e.g. Liaw et al^[9.3] using cumulative fission yields and P_n branching ratios; and thirdly by a more empirical method, proposed by Pai et al^[9.4] and modified by Tuttle^[9.5], based upon systematics of the delayed neutron production with mass and charge of the fissioning compound nucleus.

The time dependence of delayed neutron emission can be determined by experiment or

[9.2] G.R.Keepin, Physics of Nuclear Kinetics, Addison-Wesley(1965).

[9.3] J.R.Liaw and T.R.England: Trans. Amer. Nucl. Soc. 28, 750 (1978).

[9.4] H.L.Pai: Ann. Nucl. Energy, 3, 125(1976).

[9.5] R.J.Tuttle in Proc. consultants' meeting on delayed neutrons properties, Vienna, 26-30 March(1979).

by summation calculations using the P_n branching ratios, half-lives and inventories of the fission products following an irradiation e.g. the work of Brady and England^[9.6]. The proposed use of reprocessed fuel containing significant quantities of higher actinides has led to requests for the values of $\bar{\nu}_d$ for these nuclides so that their effects on the kinetic response of reactors can be estimated for safety studies. As experiments with these materials are often difficult due to the lack of reasonably sized samples and thus reported experiments are rare in the literature, the summation method may be the most reliable way for these $\bar{\nu}_d$'s to be estimated if it can be shown to be more accurate than the empirical extrapolation method of Pai^[9.4] and Tuttle^[9.5]. However the uncertainties in the yields and branching ratios of the delayed neutron emitters must be reviewed in order to decide whether the summation method is significantly accurate for practical use.

The delayed neutron emitters exist on the extremely neutron rich side of the independent fission yield distribution, where few fission product yield measurements have been made except for the more common actinides such as ^{235}U and ^{239}Pu . Thus the models used to predict the charge distribution of the fission yields will have a significant effect on the $\bar{\nu}_d$. Also the different chain yield distributions for the fission of the higher actinides mean that some precursors, relatively unimportant for ^{235}U fission, become much more significant. Especially important is the movement of the light mass peak towards higher mass as the mass of the fissioning nuclide increases. However, measurements of the P_n values have been based mainly upon ^{235}U fission so theoretical estimates of the P_n branching ratios become much more important when considering the higher actinides.

The neutron emission is a result of β^- decay producing a daughter which has sufficient energy to throw off a neutron. The probability of a nuclide emitting a neutron as a result of a β^- decay is referred to as the P_n . The fission products present determine the delayed neutron emission rate, n_{emit} , from the activity of these precursors:

$$n_{\text{emit}}(t) = \sum P_{ni} \lambda_i N_i(t) \quad \text{Eqn (9.1)}$$

[9.6] M.C.Brady and T.R.England: Nucl. Sci. Eng. 103 129(1989).

where P_{ni} is the P_n for nuclide i , λ_i is the decay constant of i , and $N_i(t)$ is the number of i present at time t after the irradiation. N_i is determined by the initial fuel composition and the irradiation this receives. Therefore to generate the delayed neutron emission rate the irradiation must be specified and a calculation made of the inventory at each time t . However, the total delayed neutron emission rate per fission, $\bar{\nu}_d$, can be calculated by integrating over all time for a single fission. Thus

$$\bar{\nu}_d = \sum_i P_{ni} R_i = \sum_i P_{ni} c_i \quad \text{Eqn (9.2)}$$

The total decays of nuclide i per fission, R_i , is equal to the cumulative fission product yield of i ; thus, for a pure sample of an actinide, if the cumulative yields, c_i are known the $\bar{\nu}_d$ can be calculated. Alternatively, if we consider a very long irradiation where all the fission products have reached equilibrium then the activity of each is the cumulative yield, thus producing the same formula. This equivalence is due to the definition of the cumulative yield.

The uncertainty in the calculated $\bar{\nu}_d$ can be estimated from Eqn (9.2), by partial differentiation and assuming c and P_n are independent, as:

$$\sigma_{\bar{\nu}_d}^2 = \sum_i P_{ni}^2 \sigma_{c_i}^2 + \sum_i \sigma_{P_{ni}}^2 c_i^2 \quad \text{Eqn (9.3)}$$

9.3.1.1 Summation calculations of $\bar{\nu}_d$.

From Eqn (9.2) and Eqn (9.3) values of $\bar{\nu}_d$ with uncertainties are easily calculated from the UKFY2, JEF2.2 and the UKFY3 datafiles with the respective decay data sets. In all cases the decay data used to generate the cumulative yields were those used for the calculations. The $\bar{\nu}_d$ values given in the following tables are quoted per 100 fissions.

Table 9.8 shows the results for UKFY3 with the officially released JEF2.2 decay data. For each fissioning system the $\bar{\nu}_d$ value with its calculated uncertainty is shown alongside the most recent evaluations and the ratio of calculated over measured.

The evaluated values are based upon experiment and taken from the following sources; the evaluations of Tuttle (1979)^[9.5], Tuttle (1975)^[9.7] and Manero (1972)^[9.8], and where these evaluations do not contain data the experimental values reported by Benedetti^[9.9] and Waldo^[9.10] were used.

Table 9.8 contains previous results using the UKFY2(1991) evaluated file and a pre-release version of the JEF2.2(1991) decay data. These results have been reported previously^[9.11].

Table 9.8 shows an updated set of these results using the final JEF2.2 fission yields and decay data, which were extensively modified from the preliminary versions used in the calculations for Table 9.8. The JEF2.2 files were released in August 1993.

As can be seen from Table 9.8 there is a tendency to over-predict $\bar{\nu}_d$ for masses below 238 and under-predict those above. But if we look at the six main systems which could be fitted to the Wahl Z_p model then UKFY3 appears to either improve over the previous versions or not to change significantly. These results of calculated to evaluated experimental (C/E) values for these six fissioning systems are shown in Table 9.11. The evaluated uncertainties are given as one standard deviation and are also given in brackets as a percentage of the value. For the main systems a recent study^[9.12] based upon the currently available experimental data considered the previous evaluated uncertainties to be low, and suggested larger values which should be associated with the results. The uncertainties of the other experimental values measured relative to these are thus also brought into question.

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Table 9.8 Calculation of $\bar{\nu}_d$ using the UKFY3 fission yields with JEF2.2 decay data

Nuclide	neutron energy	calculated $\bar{\nu}_d$	Measured $\bar{\nu}_d$ ^a	Calculated/Measured
Thorium-232	Fast	7.03334 +/- 9.57E-01	5.47 +/-0.12 T	1.29±0.14
Thorium-232	14 MeV	3.56795 +/- 9.40E-01	2.85 +/-0.13 V	1.25±0.27
Uranium-233	Thermal	0.79953 +/- 8.40E-02	0.664+/-0.018 T	1.20±0.11
Uranium-233	Fast	1.16914 +/- 1.11E-01	0.729+/-0.019 T	1.60±0.09
Uranium-233	14 MeV	0.65902 +/- 1.34E-01	0.422+/-0.025 V	1.56±0.21
Uranium-234	Fast	1.52247 +/- 1.97E-01	1.06 +/-0.12 T	1.44±0.17
Uranium-235	Thermal	1.65122 +/- 1.17E-01	1.654+/-0.042 T	1.00±0.08
Uranium-235	Fast	1.86154 +/- 1.48E-01	1.714+/-0.022 T	1.09±0.08
Uranium-235	14 MeV	1.00089 +/- 1.01E-01	0.927+/-0.029 V	1.09±0.11
Uranium-236	Fast	2.77807 +/- 3.59E-01	2.31 +/-0.26 T	1.20±0.17
Uranium-238	Fast	4.64905 +/- 3.73E-01	4.510+/-0.061 T	1.03±0.08
Uranium-238	14 MeV	2.72759 +/- 3.31E-01	2.73 +/-0.08 V	1.00±0.12
Neptunium-237	Thermal	1.24691 +/- 1.93E-01	1.07 +/-0.10 W	1.16±0.18
Neptunium-237	Fast	1.30329 +/- 1.40E-01	1.22 +/-0.03 B	1.07±0.11
Neptunium-238	Thermal	1.54841 +/- 2.42E-01		
Neptunium-238	Fast	1.64188 +/- 2.83E-01		
Plutonium-238	Thermal	0.32770 +/- 7.03E-02	0.456+/-0.051 T	0.72±0.24
Plutonium-238	Fast	0.50951 +/- 1.34E-01	0.456+/-0.051 T	1.12±0.29
Plutonium-239	Thermal	0.65824 +/- 5.83E-02	0.624+/-0.024 T	1.06±0.10
Plutonium-239	Fast	0.72143 +/- 1.05E-01	0.664+/-0.013 T	1.09±0.15
Plutonium-240	Fast	0.96673 +/- 9.10E-02	0.96 +/-0.11 T	1.01±0.15
Plutonium-241	Thermal	1.36298 +/- 1.48E-01	1.56 +/-0.16 T	0.87±0.15
Plutonium-241	Fast	1.40386 +/- 1.41E-01	1.63 +/-0.16 T	0.86±0.14
Plutonium-242	Fast	1.83733 +/- 1.45E-01	2.28 +/-0.25 T	0.81±0.14
Americium-241	Thermal	0.41096 +/- 5.69E-02	0.44 +/-0.05 W	0.934±0.18
Americium-241	Fast	0.46681 +/- 9.76E-02	0.394+/-0.024 B	1.18±0.22
Americium-242m	Thermal	0.62532 +/- 1.37E-01	0.69 +/-0.05 W	0.906±0.23
Americium-242m	Fast	0.60369 +/- 1.14E-01		
Americium-243	Thermal	0.91154 +/- 1.78E-01		
Americium-243	Fast	0.87035 +/- 1.56E-01		
Curium-242	Spontaneous	0.12504 +/- 3.31E-02		
Curium-243	Thermal	0.22206 +/- 6.57E-02		
Curium-243	Fast	0.22219 +/- 4.53E-02		
Curium-244	Spontaneous	0.33026 +/- 9.82E-02		
Curium-244	Thermal	0.34944 +/- 8.76E-02		
Curium-244	Fast	0.35229 +/- 7.48E-02		
Curium-245	Thermal	0.47013 +/- 1.32E-01	0.59 +/-0.04 W	0.797±0.29
Curium-245	Fast	0.49572 +/- 8.87E-02		
Californium-252	Spontaneous	0.58425 +/- 2.08E-01	0.86 +/-0.10 M	0.679±0.37

a. References denoted by letter; B-Benedetti(1982) M-Manero(1972) T-Tuttle(1975) V-Tuttle(1979) W-Waldo(1981)

Table 9.9 Calculation of \bar{v}_d using JEF2 (1991) decay data and UKFY2

Nuclide	neutron energy	calculated \bar{v}_d	Measured \bar{v}_d ^a	Calculated/Measured
Thorium-232	Fast	5.61039+/-0.390	5.47 +/-0.12 T	1.026±0.07
Thorium-232	14 MeV	2.83841+/-0.245	2.85 +/-0.13 V	0.996±0.10
Uranium-233	Thermal	0.85440+/-0.083	0.664+/-0.018 T	1.287±0.10
Uranium-233	Fast	0.92347+/-0.088	0.729+/-0.019 T	1.267±0.10
Uranium-233	14 MeV	0.33727+/-0.065	0.422+/-0.025 V	0.799±0.20
Uranium-234	Fast	1.15861+/-0.156	1.06 +/-0.12 T	1.093±0.18
Uranium-235	Thermal	1.64484+/-0.114	1.654+/-0.042 T	0.994±0.07
Uranium-235	Fast	1.85414+/-0.129	1.714+/-0.022 T	1.082±0.07
Uranium-235	14 MeV	0.78682+/-0.082	0.927+/-0.029 V	0.849±0.11
Uranium-236	Fast	2.24125+/-0.182	2.31 +/-0.26 T	0.970±0.14
Uranium-238	Fast	4.05641+/-0.195	4.510+/-0.061 T	0.899±0.05
Uranium-238	14 MeV	2.30629+/-0.196	2.73 +/-0.08 V	0.845±0.09
Neptunium-237	Thermal	1.17786+/-0.149	1.07 +/-0.10 W	1.101±0.16
Neptunium-237	Fast	1.18115+/-0.086	1.22 +/-0.03 B	0.968±0.08
Plutonium-238	Thermal	0.33699+/-0.051	0.456+/-0.051 T	0.739±0.19
Plutonium-238	Fast	0.45152+/-0.072	0.456+/-0.051 T	1.001±0.19
Plutonium-239	Thermal	0.58948+/-0.054	0.624+/-0.024 T	0.945±0.10
Plutonium-239	Fast	0.66093+/-0.057	0.664+/-0.013 T	0.995±0.09
Plutonium-240	Fast	0.89203+/-0.107	0.96 +/-0.11 T	0.929±0.17
Plutonium-241	Thermal	1.30026+/-0.129	1.56 +/-0.16 T	0.834±0.14
Plutonium-241	Fast	1.37337+/-0.093	1.63 +/-0.16 T	0.843±0.12
Plutonium-242	Fast	1.81825+/-0.137	2.28 +/-0.25 T	0.797±0.13
Americium-241	Thermal	0.38675+/-0.063	0.44 +/-0.05 W	0.879±0.20
Americium-241	Fast	0.39153+/-0.074	0.394+/-0.024 B	0.994±0.20
Americium-242m	Thermal	0.61209+/-0.084	0.69 +/-0.05 W	0.887±0.16
Curium-245	Thermal	0.47658+/-0.084	0.59 +/-0.04 W	0.808±0.19
Californium-252	Spontaneous	0.68913+/-0.154	0.86 +/-0.10 M	0.801±0.25

a. References denoted by letter; B-Benedetti(1982) M-Manero(1972) T-Tuttle(1975) V-Tuttle(1979) W-Waldo(1981)

Table 9.10 Calculation of $\bar{\nu}_d$ using JEF2.2 decay data and fission yields

Nuclide	neutron energy	calculated $\bar{\nu}_d$	Measured $\bar{\nu}_d^a$	Calculated/Measured
Thorium-232	Fast	6.04559 +/- 4.55E-01	5.47 +/-0.12 T	1.105±0.08
Thorium-232	14 MeV	2.93874 +/- 2.52E-01	2.85 +/-0.13 V	1.031±0.10
Uranium-233	Thermal	0.87778 +/- 8.45E-02	0.664+/-0.018 T	1.322±0.10
Uranium-233	Fast	0.95255 +/- 1.15E-01	0.729+/-0.019 T	1.307±0.12
Uranium-233	14 MeV	0.34425 +/- 6.88E-02	0.422+/-0.025 V	0.816±0.21
Uranium-234	Fast	1.19717 +/- 1.94E-01	1.06 +/-0.12 T	1.124±0.20
Uranium-235	Thermal	1.70768 +/- 1.17E-01	1.654+/-0.042 T	1.032±0.20
Uranium-235	Fast	1.90981 +/- 2.01E-01	1.714+/-0.022 T	1.166±0.11
Uranium-235	14 MeV	0.78986 +/- 8.16E-02	0.927+/-0.029 V	0.852±0.11
Uranium-236	Fast	2.32978 +/- 2.05E-01	2.31 +/-0.26 T	1.009±0.14
Uranium-238	Fast	4.26631 +/- 2.02E-01	4.510+/-0.061 T	0.946±0.09
Uranium-238	14 MeV	2.39520 +/- 2.06E-01	2.73 +/-0.08 V	0.877±0.16
Neptunium-237	Thermal	1.23220 +/- 1.55E-01	1.07 +/-0.10 W	1.152±0.07
Neptunium-237	Fast	1.23409 +/- 8.88E-02	1.22 +/-0.03 B	1.011±0.16
Plutonium-238	Thermal	1.47197 +/- 1.76E-01	0.456+/-0.051 T	3.228±0.20
Plutonium-238	Fast	0.46987 +/- 7.49E-02	0.456+/-0.051 T	1.030±0.19
Plutonium-239	Thermal	0.61740 +/- 5.61E-02	0.624+/-0.024 T	0.989±0.10
Plutonium-239	Fast	0.69008 +/- 7.93E-02	0.664+/-0.013 T	1.039±0.19
Plutonium-240	Fast	0.93974 +/- 1.12E-01	0.96 +/-0.11 T	0.979±0.17
Plutonium-241	Thermal	1.33637 +/- 1.35E-01	1.56 +/-0.16 T	0.857±0.14
Plutonium-241	Fast	1.45238 +/- 9.63E-02	1.63 +/-0.16 T	0.891±0.12
Plutonium-242	Fast	1.92750 +/- 1.39E-01	2.28 +/-0.25 T	0.845±0.13
Americium-241	Thermal	0.40910 +/- 6.62E-02	0.44 +/-0.05 W	0.930±0.20
Americium-241	Fast	0.41147 +/- 7.70E-02	0.394+/-0.024 B	1.044±0.20
Americium-242m	Thermal	0.64864 +/- 8.38E-02	0.69 +/-0.05 W	0.940±0.15
Curium-245	Thermal	0.50695 +/- 8.86E-02	0.59 +/-0.04 W	0.859±0.19
Californium-252	Spontaneous	0.74153 +/- 1.64E-01	0.86 +/-0.10 M	0.862±0.25

a. References denoted by letter; B-Benedetti(1982) M-Manero(1972) T-Tuttle(1975) V-Tuttle(1979) W-Waldo(1981)

Table 9.11: Comparison of the calculated and evaluated $\bar{\nu}_d$ for the three main fissioning systems.

System	Evaluated $\bar{\nu}_d$ Tuttle (1975)	Recommended uncertainty (1990) ^[9.12]	UKFY3 ----- Expt	JEF2.2 ----- Expt	UKFY2 ----- Expt
U233T	0.87778±0.0845 (9.6%)	-	1.20	1.32	1.29
U235T	1.654±0.042 (2.5%)	5.0%	1.00	1.03	0.99
U235F	1.90981±0.201 (10.1%)	-	1.09	1.17	1.08
U235H	0.78986±0.0816 (10.3%)	-	1.09	0.852	0.85
U238F	4.510+/-0.061 (1.4%)	6.4%	1.03	0.94	0.90
Pu239T	0.664+/-0.013 (2.0%)	10.0%	1.06	0.99	0.95

It is interesting to note that the system with the poorest fit to the Z_p model (thermal neutron fission of ^{233}U) also has the worst C/E values. Unfortunately other fissioning systems between masses 235 and 238 do show considerable apparently random variation of C/E. This suggests that the increasing under-estimation of $\bar{\nu}_d$ with increasing compound nucleus mass cannot be explained by a trend in the P_n model calculations.

Although these results show UKFY3 to be an improvement if we consider the overall set of data the situation is more complex. The mean of the C/E values, although not a rigorous statistical comparison, shows that previously the results were slightly under-predicted and now they are slightly over-predicted. However if the χ^2 test is applied using the experimentally determined uncertainties the χ^2 calculations suggest that the results are highly discrepant with some χ^2 components being considerably greater than 3.0. If the calculations are carried out using the uncertainties calculated from Eqn (9.3) then the results do show an improvement.

Table 9.12: χ^2 test of the three sets of calculations

Fission yield file	Decay data file	χ^2 (calc) /dof	χ^2 (expt) /dof	mean C/E
UKFY2	JEF2.1 (pre-release)	2.27	1.90	0.95
JEF2.2	JEF2.2	2.62	16.29	1.08
UKFY3	JEF2.2	2.08	5.22	1.07

These results suggest that using the summation method where it has not been possible to fit the Z_p model produces considerable discrepancies in the calculated $\bar{\nu}_d$ when compared with the evaluated experimental data.

When the components of the χ^2 are examined it was found that most discrepancy came from seven systems with χ^2 components greater than ten. These systems (TH232F, TH232H, U233T, U233F, U233H, U234F and Pu238T) contain little or no fractional independent yield measurements. If these are removed the results become:

Table 9.13: χ^2 test of the three sets of calculations

Fission yield file	Decay data file	χ^2 (calc) /dof	χ^2 (expt) /dof	mean C/E
UKFY2	JEF2.1 (pre-release)	2.18	1.29	0.92
JEF2.2	JEF2.2	1.19	0.87	0.96
UKFY3	JEF2.2	1.13	1.65	1.00

It can thus be concluded that UKFY3 gives good agreement where the systems have been successfully fitted to the Wahl Z_p model. However the extrapolation of the eight Z_p parameters shows considerable deviation from the expected experimental results for the seven system referred to above.

It must be remembered that these calculations are very sensitive to short lived nuclides far from stability and the P_n values used. Thus study of the sensitivity of these calculations to the Z_p parameters and different P_n data sets will give more information on the properties of the $\bar{\nu}_d$ calculations.

9.3.1.2 Sensitivity of $\bar{\nu}_d$ to Z_p Parameters

The sensitivity of the $\bar{\nu}_d$ to the Z_p parameters was studied by considering the fractional change in $\bar{\nu}_d$ following a small change in each Z_p parameter used to generate a set of unadjusted yields. These yield sets were not adjusted to fit physical constraints as this would alter the independent yields used in the calculation. This study was made with the UKFY2 fission yields and its corresponding decay data file. Time constraints have not allowed this work to be repeated with the UKFY3.0 file. Each of the eight parameters \mathbf{x} was varied in turn by + and - 1%, and the sensitivity $S(\mathbf{x})$ of $\bar{\nu}_d$ to \mathbf{x} found from:

$$S(\mathbf{x}) = 100 \frac{\bar{\nu}_d(\mathbf{x} + 1\%) - \bar{\nu}_d(\mathbf{x} - 1\%)}{2\bar{\nu}_d(\mathbf{x})} \quad \text{Eqn (9.4)}$$

The results of this calculation are shown in Table 9.14. This shows the 1% sensitivities to the Z_p parameters for the thermal and fast neutron fission of ^{235}U .

Table 9.14: Sensitivity of $\bar{\nu}_d$ to input Z_p model parameters

System	$\Delta Z(A'=50)$	$\frac{d\Delta Z}{dA'}$	$\bar{\sigma}_z$	$\bar{\sigma}_{50}$	\bar{F}_z	\bar{F}_n	$\Delta A'_z$	ΔZ_{\max}
U235T	-0.44	-0.046	1.2	0.0010	-0.99	0.10	-0.0012	-0.0010
U235F	-0.47	-0.10	1.0	0.00045	-0.95	0.037	-0.000021	0.000023

Variations of + and - 10% were also made, but the calculated sensitivities were not found to change significantly. This suggests the sensitivity to the parameters are not rapidly changing.

These results shows that $\bar{\sigma}_z$, \bar{F}_z and $\Delta Z(A'=50)$ are the most important Z_p parameters for calculation of $\bar{\nu}_d$. The two parameters $\bar{\sigma}_z$ and $\Delta Z(A'=140)$ largely determine the shape and positions of the Gaussian fractional independent fission yield distributions, and hence the yields of the neutron-rich precursors. The dependence on \bar{F}_z reflects the preponderance of odd-Z delayed neutron precursors.

A detailed understanding of how these three Z_p parameters change between different

systems would thus improve the results of summation calculations.

9.3.1.3 Sensitivity of $\bar{\nu}_d$ to different P_n sets

To study the effect of different P_n datasets upon $\bar{\nu}_d$, calculations of Eqn (9.2) were carried out using the UKFY2 cumulative yields with different P_n datasets. It should be noted that if the different P_n values had been used in the production of the UKFY2 they file would alter the predicted cumulative yields. Thus the $\bar{\nu}_d$ would be altered. However, previous work^[1.4] had showed that for most mass chains these differences in chain yields would be small. This effect was, therefore, ignored for the purpose of this study.

The results for the thermal neutron fission of ^{235}U and ^{239}Pu , and the fast neutron fission of ^{235}U and ^{238}U are shown in Table 9.15. The number of delayed neutron emitters in each file are shown in the table with a flag to show whether the set includes experimental (E), model prediction (M) or both (EM). Also the results of the two later calculations with the JEF2.2 decay data are shown for comparison.

Table 9.15: $\bar{\nu}_d$ calculated using different P_n datasets.

Fission yield file	Decay data file	number of P_n 's ^a	$\bar{\nu}_d^{235}\text{U}$ (thermal)	$\bar{\nu}_d^{235}\text{U}$ (fast)	$\bar{\nu}_d^{238}\text{U}$ (fast)	$\bar{\nu}_d^{239}\text{Pu}$ (thermal)
UKFY2(1990)	JEF2 (1991)	94 EM	1.6354	1.8492	3.9039	0.5884
UKFY2(1990)	Lund(1986)	83 E	1.4455	1.5963	3.5420	0.5050
UKFY2(1990)	Mann(1986)	88 E	1.5665	1.7629	3.6896	0.5970
UKFY2(1990)	Brady (1988)	271 EM	1.6995	1.9092	4.0218	0.6131
UKFY2(1990)	Klapdor(1989)	209 M	1.2572	1.4044	3.2950	0.4697
UKFY2(1990)	JEF2 (May 1991) + Klapdor (1989)	251 EM	1.6447	1.8541	4.0491	0.5895
JEF2.2(1993)	JEF2.2 (1993)	165EM	1.7071	1.9092	4.2611	0.6171
UKFY3(1994)	Final JEF2.2 (July 1993)	165 EM	1.65122	1.86154	4.64905	0.65824

a. E is experimental data, M is modelled data and EM is a combination of the two.

This work shows that the majority of the delayed neutron emission comes from precursors whose P_n values have been measured. For the thermal fission of ^{235}U only around 6% of the total $\bar{\nu}_d$ for the thermal ^{235}U case comes from modelled P_n values. Interestingly using all modelled P_n values decreases for the value. This may indicated

that the modelled P_n values are unrealistically small.

9.3.1.4 The Keepin six group model

As described above the neutron emission rate following a neutron irradiation can be calculated from an inventory calculation using Eqn (9.1). However, in practice, reactor kinetics codes consider a small set of “lumped fission products” with a set of a representative decay constants and yields. This approach was pioneered by Keepin^[9.2] who found that a set of six “lumped fission products” gave a good approximation to measurements.

The six group representation of the delayed neutron activity following a single fission pulse of one ‘average’ fission was thus approximated by Keepin^[9.2] as:

$$n_{\text{emit}}(t) = \bar{\nu}_d \sum_{k=1}^6 \alpha_k \lambda_k e^{-\lambda_k t} \quad \text{Eqn (9.5)}$$

and similarly for a long constant irradiation, producing 1 fission per second, as:

$$n_{\text{emit}}(t) = \bar{\nu}_d \sum_{k=1}^6 \alpha_k e^{-\lambda_k t} \quad \text{Eqn (9.6)}$$

where t is the time after the irradiation, α_k are the normalised group strengths and the λ_k are the decay constants for the six delayed neutron emitting groups. For these conditions to be applicable the pulse must be too short for any precursor to decay significantly during the irradiation. Similarly the long irradiation condition only applies if all precursors have reached equilibrium before the end of the irradiation.

It is an interesting result, which also applies to decay heat calculations, that at zero time after the long irradiation the neutron emission is equal to the integral of neutron emission following a single “average” fission pulse over all time after the irradiation.

The fission product yield set used for the following calculations of neutron emission was UKFY2. The calculations were not repeated with UKFY3 due to time constraints. The

UKFY2 fission yield file, unlike JEF2.2 and UKFY3, included nuclides that were not in the corresponding JEF2 (1991) decay data or were stable. Thus the decay data used for this work was based upon a preliminary version of JEF2 (1991), with the P_n values extended with the work of Lund^[9.13] and Klapdor^[9.14]. The half-lives were also extended using the Japanese Chart of the Nuclides^[9.15]. For JEF2.2 and UKFY3 adjustments were made to the fission yields so that the yields not in the decay data were added to the yields that were present in the decay data so that the experimental chain yields were reproduced using the fission yield sets and the JEF2.2 decay data.

To generate the Keepin six group constants using the UKFY2 data it was first necessary to use Eqn (9.1) and the inventory code FISPIN^[2.1] to generate the n_{emit} for all 39 fission systems in UKFY2. Both a single fission pulse (10^6 fission/s for 10^{-6} s) and a 'long' irradiation (1 fission/s for 10^{13} s) were modelled. The cooling time steps after the irradiation ranged from zero to 500 seconds. 204 time steps were chosen to reproduce accurately the rapidly changing curves.

The FISPIN code used was a modified version of 6.0 that read in the UKFY2 and JEF2 (1991) decay data in ENDF/B format. The FISPIN calculations used no actinide content or flux but assumed a constant fission rate that produced fission products. The number density and activities of these were then calculated by numerically solving Eqn (2.1).

The Keepin's six group model was fitted to the pulse and infinite irradiation data simultaneously (i.e. 408 data points) using the Levenberg-Marquardt method^[9.16] as applied by Press et al^[9.17]. The $\bar{\nu}_d$ values used were taken from the zero time long

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irradiation results. The results of these calculations are shown in Table 9.16.

Table 9.16: Keepin six Group parameters fitted using the UKFY2 fission yields for the 39 fissioning systems.

Nuclide	Group	1	2	3	4	5	6
AM241F	alpha	0.0517	0.3316	0.0876	0.2201	0.2742	0.0349
	lambda	0.0125	0.0291	0.0633	0.1821	0.4029	2.1434
AM241T	alpha	0.0277	0.1859	0.2184	0.1706	0.3554	0.0420
	lambda	0.0124	0.0263	0.0322	0.1346	0.3647	2.0514
AM242MF	alpha	0.0214	0.3612	0.1158	0.3055	0.1556	0.0405
	lambda	0.0125	0.0288	0.0882	0.2455	0.5433	2.3395
AM242MT	alpha	0.0235	0.2919	0.0995	0.2062	0.3304	0.0486
	lambda	0.0124	0.0277	0.0385	0.1406	0.3805	2.0568
AM243F	alpha	0.0138	0.3360	0.1433	0.3385	0.1259	0.0424
	lambda	0.0125	0.0288	0.0971	0.2813	0.7276	2.5737
AM243T	alpha	0.0136	0.3659	0.1353	0.3261	0.1189	0.0401
	lambda	0.0125	0.0287	0.0969	0.2847	0.7465	2.6004
CF252S	alpha	0.0060	0.2134	0.2156	0.2166	0.0521	0.2963
	lambda	0.0124	0.0270	0.0306	0.1168	1.5128	0.3892
CM242S	alpha	0.0320	0.1237	0.2618	0.3995	0.0319	0.1511
	lambda	0.0124	0.0253	0.0317	0.3523	1.9673	0.1318
CM243F	alpha	0.0362	0.3419	0.1833	0.3126	0.0305	0.0955
	lambda	0.0124	0.0279	0.1395	0.3619	1.9644	0.0401
CM243T	alpha	0.0258	0.1980	0.2909	0.1710	0.2871	0.0273
	lambda	0.0124	0.0261	0.0314	0.1253	0.3580	1.9313
CM244F	alpha	0.0234	0.3261	0.1266	0.1882	0.2997	0.0360
	lambda	0.0124	0.0275	0.0356	0.1322	0.3687	1.9639
CM244S	alpha	0.0177	0.3566	0.1769	0.2772	0.0285	0.1430
	lambda	0.0124	0.0275	0.1288	0.3703	2.0649	0.0336
CM244T	alpha	0.0222	0.3035	0.1547	0.1866	0.2958	0.0372
	lambda	0.0124	0.0272	0.0341	0.1314	0.3694	1.9630
CM245F	alpha	0.0163	0.2857	0.1616	0.1982	0.2956	0.0427
	lambda	0.0124	0.0272	0.0334	0.1282	0.3785	1.9093
CM245T	alpha	0.0173	0.3169	0.0874	0.2168	0.3182	0.0434
	lambda	0.0124	0.0278	0.0376	0.1291	0.3786	1.9349
NP237F	alpha	0.0308	0.2198	0.1112	0.3863	0.1804	0.0715
	lambda	0.0125	0.0298	0.0863	0.2475	0.5821	2.4425
NP237T	alpha	0.0328	0.2546	0.1169	0.3865	0.1455	0.0638
	lambda	0.0125	0.0295	0.0925	0.2653	0.6557	2.5504
NP238F	alpha	0.0201	0.2308	0.1236	0.4023	0.1548	0.0685
	lambda	0.0125	0.0294	0.0934	0.2698	0.7263	2.6630
NP238T	alpha	0.0201	0.2638	0.1239	0.3857	0.1374	0.0691
	lambda	0.0125	0.0292	0.0962	0.2791	0.8055	2.7287
PU238F	alpha	0.0473	0.2566	0.0816	0.2711	0.2953	0.0481

Table 9.16: Keepin six Group parameters fitted using the UKFY2 fission yields for the 39 fissioning systems.

Nuclide	Group	1	2	3	4	5	6
	lambda	0.0125	0.0294	0.0621	0.1832	0.3984	2.1457
PU238T	alpha	0.0294	0.2517	0.0759	0.2886	0.2933	0.0611
	lambda	0.0125	0.0291	0.0711	0.1980	0.4156	2.2023
PU239F	alpha	0.0289	0.2719	0.0905	0.3055	0.2476	0.0557
	lambda	0.0125	0.0292	0.0737	0.2095	0.4520	2.2679
PU239T	alpha	0.0292	0.2799	0.0982	0.3323	0.2034	0.0569
	lambda	0.0125	0.0292	0.0828	0.2322	0.4973	2.3386
PU240F	alpha	0.0193	0.2911	0.1332	0.3735	0.1341	0.0489
	lambda	0.0125	0.0289	0.0976	0.2740	0.6601	2.5194
PU241F	alpha	0.0122	0.2516	0.1418	0.3878	0.1475	0.0590
	lambda	0.0125	0.0289	0.0998	0.2915	0.8047	2.7593
PU241T	alpha	0.0125	0.2516	0.1344	0.3913	0.1469	0.0634
	lambda	0.0125	0.0290	0.0988	0.2888	0.7827	2.7168
PU242F	alpha	0.0081	0.2134	0.1419	0.3957	0.1784	0.0625
	lambda	0.0126	0.0289	0.1023	0.3047	0.8744	2.8921
TH232F	alpha	0.0291	0.1177	0.1116	0.4632	0.2070	0.0714
	lambda	0.0126	0.0323	0.1058	0.3033	0.9131	2.9891
TH232H	alpha	0.0410	0.1583	0.1148	0.4341	0.1873	0.0645
	lambda	0.0125	0.0315	0.0955	0.2706	0.6942	2.4129
U233F	alpha	0.0722	0.0575	0.1894	0.2697	0.3506	0.0605
	lambda	0.0124	0.0247	0.0391	0.1542	0.3675	2.0712
U233H	alpha	0.0331	0.1123	0.2809	0.3204	0.0327	0.2206
	lambda	0.0112	0.0133	0.0357	0.3369	1.8030	0.1338
U233T	alpha	0.0757	0.1915	0.0947	0.3497	0.2256	0.0629
	lambda	0.0125	0.0315	0.0685	0.2014	0.4620	2.2332
U234F	alpha	0.0559	0.1957	0.0974	0.3554	0.2316	0.0640
	lambda	0.0125	0.0310	0.0726	0.2132	0.4840	2.3218
U235F	alpha	0.0324	0.1605	0.1141	0.4523	0.1533	0.0874
	lambda	0.0125	0.0314	0.0922	0.2607	0.7062	2.6802
U235H	alpha	0.0603	0.2223	0.1046	0.2647	0.3028	0.0452
	lambda	0.0125	0.0296	0.0528	0.1690	0.3949	2.0373
U235T	alpha	0.0343	0.1974	0.1193	0.4002	0.1745	0.0742
	lambda	0.0125	0.0304	0.0903	0.2501	0.6455	2.4599
U236F	alpha	0.0257	0.1681	0.1250	0.4326	0.1703	0.0784
	lambda	0.0126	0.0305	0.0977	0.2810	0.8215	2.7776
U238F	alpha	0.0096	0.1198	0.1109	0.4062	0.2469	0.1067
	lambda	0.0126	0.0298	0.1038	0.3040	0.9322	3.0302
U238H	alpha	0.0193	0.1768	0.1266	0.4288	0.1832	0.0652
	lambda	0.0126	0.0297	0.1010	0.2867	0.8141	2.7951

As well as fitting the twelve α_k and λ_k parameters, an attempt was made to fit the six α_k values with a constant set of λ_k to allow simplification in reactor calculations where more than one of the nuclides are present.

Table 9.17 contains the fitted α_k values if the set of average λ_k values reported by Keepin^[9.2] (Table 4-9, page 91) were used.

Table 9.18 shows the results of using the set of λ_k values from Table 9.16 for the thermal neutron fission of ^{235}U .

The effects of these approximations were then studied. A “maximum percentage deviation” was calculated as the maximum percentage deviation of the fitted curves from the FISPIN calculations. Also a “percentage standard deviation” was calculated as the mean of the percentage deviations of the fitted curves from the FISPIN calculation.

These measures of the goodness of fit are shown in Table 9.19, Table 9.20 and Table 9.20 for the results in Table 9.16, Table 9.17 and Table 9.18 respectively. These tables also include the number of percentage deviations within each of one to five “percentage standard deviations”.

As can be seen from these calculations the 12 parameter fits gives the best results. These seldom vary by more than 1% from the calculation. However the two approximations (using the fixed λ_k sets) show considerably higher variation from the FISPIN calculations. These differences would not allow accurate reactor calculations and thus the full 12 parameters fits must be used.

Table 9.17: Fits to the Keepin 6 Group model using the FISPIN code with UKFY2 fission products yields and preliminary JEF2 decay data for the 39 fissioning systems. The lambda's are kept fixed at the 'average' Keepin values. p91 table 4-9.

Group	1	2	3	4	5	6
lambda	0.0127	0.0320	0.1279	0.3040	1.3485	3.6290
AM241F	0.0574	0.3873	0.1062	0.3882	0.0545	0.0065
AM241T	0.0339	0.4474	0.0172	0.4431	0.0481	0.0102
AM242MF	0.0247	0.4240	0.0576	0.4196	0.0617	0.0124
AM242MT	0.0284	0.4229	0.0583	0.4195	0.0599	0.0109
AM243F	0.0161	0.3996	0.0542	0.4291	0.0861	0.0149
AM243T	0.0160	0.4356	0.0295	0.4226	0.0813	0.0151
CF252S	0.0082	0.5168	0.0089	0.4009	0.0631	0.0022
CM242S	0.0388	0.4206	0.0204	0.4738	0.0404	0.0059
CM243F	0.0427	0.4653	0.0547	0.3944	0.0369	0.0061
CM243T	0.0320	0.5489	0.0115	0.3736	0.0275	0.0064
CM244F	0.0287	0.5019	0.0315	0.3898	0.0402	0.0079
CM244S	0.0223	0.5675	0.0000	0.3715	0.0316	0.0071
CM244T	0.0274	0.5122	0.0224	0.3891	0.0404	0.0085
CM245F	0.0206	0.5077	0.0244	0.3899	0.0490	0.0083
CM245T	0.0214	0.4519	0.0622	0.4020	0.0547	0.0077
NP237F	0.0334	0.2472	0.1415	0.4434	0.1122	0.0222
NP237T	0.0361	0.2865	0.1111	0.4395	0.1040	0.0228
NP238F	0.0222	0.2645	0.1140	0.4497	0.1231	0.0265
NP238T	0.0225	0.3036	0.0886	0.4334	0.1211	0.0309
PU238F	0.0518	0.2996	0.1500	0.4217	0.0665	0.0104
PU238T	0.0328	0.2923	0.1141	0.4677	0.0766	0.0166
PU239F	0.0321	0.3158	0.1177	0.4416	0.0777	0.0151
PU239T	0.0327	0.3217	0.0991	0.4492	0.0801	0.0172
PU240F	0.0220	0.3397	0.0777	0.4583	0.0854	0.0169
PU241F	0.0140	0.2980	0.0772	0.4612	0.1260	0.0235
PU241T	0.0143	0.2973	0.0730	0.4654	0.1245	0.0254
PU242F	0.0093	0.2558	0.0706	0.4728	0.1680	0.0236
TH232F	0.0299	0.1188	0.1345	0.4688	0.2279	0.0201
TH232H	0.0427	0.1654	0.1612	0.4623	0.1597	0.0087
U233F	0.0785	0.2056	0.2375	0.3832	0.0849	0.0103
U233H	0.1405	0.2528	0.2523	0.3011	0.0525	0.0008
U233T	0.0791	0.2072	0.2315	0.3732	0.0954	0.0137
U234F	0.0588	0.2140	0.2029	0.4067	0.1026	0.0150
U235F	0.0337	0.1684	0.1846	0.4416	0.1356	0.0360
U235H	0.0648	0.2792	0.2005	0.3758	0.0747	0.0050
U235T	0.0365	0.2156	0.1712	0.4245	0.1310	0.0213
U236F	0.0272	0.1835	0.1463	0.4464	0.1670	0.0295
U238F	0.0104	0.1369	0.0928	0.4469	0.2675	0.0454
U238H	0.0210	0.1995	0.1152	0.4768	0.1665	0.0210

Table 9.18 Fits to the Keepin six Group model using the FISPIN code with UKFY2 fission products yields and preliminary JEF2 decay data for the 39 fissioning systems. The Lambdas being fixed at the U235T values from this work.

Group	1	2	3	4	5	6
lambda	0.0125	0.0304	0.0903	0.2502	0.6454	2.4580
AM241F	0.0536	0.3633	0.0868	0.3593	0.1134	0.0237
AM241T	0.0311	0.4248	0.0121	0.3969	0.1068	0.0283
AM242MF	0.0226	0.3975	0.0449	0.3873	0.1101	0.0376
AM242MT	0.0261	0.3970	0.0468	0.3835	0.1126	0.0340
AM243F	0.0146	0.3723	0.0453	0.3828	0.1348	0.0502
AM243T	0.0145	0.4071	0.0296	0.3705	0.1292	0.0489
CF252S	0.0073	0.4813	0.0202	0.3502	0.1172	0.0238
CM242S	0.0358	0.3996	0.0144	0.4182	0.1148	0.0172
CM243F	0.0394	0.4400	0.0436	0.3695	0.0889	0.0187
CM243T	0.0293	0.5203	0.0126	0.3497	0.0708	0.0174
CM244F	0.0262	0.4733	0.0282	0.3620	0.0865	0.0237
CM244S	0.0203	0.5384	0.0000	0.3503	0.0704	0.0206
CM244T	0.0250	0.4836	0.0209	0.3604	0.0850	0.0249
CM245F	0.0187	0.4769	0.0256	0.3565	0.0944	0.0279
CM245T	0.0195	0.4225	0.0512	0.3746	0.1038	0.0283
NP237F	0.0312	0.2284	0.0991	0.4119	0.1615	0.0679
NP237T	0.0336	0.2675	0.0786	0.4021	0.1519	0.0663
NP238F	0.0205	0.2445	0.0811	0.4067	0.1682	0.0790
NP238T	0.0207	0.2824	0.0648	0.3893	0.1566	0.0862
PU238F	0.0486	0.2791	0.1061	0.4108	0.1211	0.0343
PU238T	0.0304	0.2731	0.0748	0.4429	0.1314	0.0474
PU239F	0.0298	0.2939	0.0842	0.4150	0.1317	0.0454
PU239T	0.0303	0.3010	0.0688	0.4174	0.1328	0.0497
PU240F	0.0202	0.3175	0.0538	0.4186	0.1381	0.0518
PU241F	0.0128	0.2759	0.0579	0.4016	0.1756	0.0762
PU241T	0.0130	0.2755	0.0545	0.4047	0.1740	0.0783
PU242F	0.0084	0.2350	0.0561	0.3873	0.2217	0.0915
TH232F	0.0284	0.1061	0.0972	0.3697	0.2951	0.1035
TH232H	0.0405	0.1498	0.1155	0.3976	0.2344	0.0623
U233F	0.0751	0.1854	0.1700	0.3954	0.1342	0.0399
U233H	0.1351	0.2286	0.1973	0.3235	0.1011	0.0144
U233T	0.0756	0.1875	0.1655	0.3844	0.1373	0.0497
U234F	0.0559	0.1946	0.1458	0.3962	0.1547	0.0528
U235F	0.0319	0.1525	0.1233	0.4248	0.1718	0.0958
U235H	0.0614	0.2553	0.1546	0.3669	0.1340	0.0278
U235T	0.0343	0.1973	0.1196	0.4002	0.1743	0.0743
U236F	0.0255	0.1673	0.1028	0.3941	0.2121	0.0983
U238F	0.0096	0.1241	0.0671	0.3467	0.2907	0.1618
U238H	0.0195	0.1832	0.0808	0.4054	0.2257	0.0854

Table 9.19: Differences between FISPIN calculation and six group model using the 12 parameter fits of Table 9.16.

System	Maximum % diff	%SD	number of points within standard deviations				
			1	2	3	4	5
AM241F	0.634	0.1327	296	377	406	407	408
AM241T	0.874	0.1952	295	380	406	407	408
AM242MF	0.598	0.1577	266	395	406	407	408
AM242MT	1.05	0.2275	303	382	406	407	408
AM243F	0.522	0.1715	262	394	407	408	408
AM243T	0.497	0.1651	259	393	407	408	408
CF252S	0.989	0.2018	322	377	405	406	408
CM242S	0.617	0.1524	281	384	406	407	408
CM243F	0.616	0.1365	302	382	406	407	408
CM243T	0.623	0.1461	285	382	406	407	408
CM244F	0.816	0.1797	304	379	406	407	408
CM244S	0.778	0.1704	306	377	406	407	408
CM244T	0.843	0.1870	300	379	406	407	408
CM245F	1.02	0.2196	302	379	406	407	408
CM245T	1.02	0.2192	304	379	406	407	408
NP237F	0.916	0.2378	272	395	406	407	408
NP237T	0.756	0.2158	273	398	406	407	408
NP238F	0.759	0.2494	265	392	407	408	408
NP238T	0.682	0.2318	264	392	408	408	408
PU238F	0.755	0.1550	300	376	406	407	408
PU238T	0.835	0.1779	291	383	406	407	408
PU239F	0.856	0.1930	286	388	406	407	408
PU239T	0.779	0.1867	281	391	406	407	408
PU240F	0.586	0.1756	261	395	407	408	408
PU241F	0.599	0.2067	260	394	408	408	408
PU241T	0.667	0.2142	261	394	407	408	408
PU242F	0.645	0.2310	262	393	408	408	408
TH232F	0.918	0.3220	268	390	408	408	408
TH232H	0.880	0.2631	271	391	407	408	408
U233F	1.13	0.2397	306	382	406	407	408
U233H	0.602	0.1822	272	390	407	408	408
U233T	0.984	0.2023	296	380	406	407	408
U234F	1.01	0.2250	290	386	406	407	408
U235F	0.910	0.3023	271	391	407	408	408
U235H	0.844	0.1641	306	374	405	406	408
U235T	0.907	0.2648	272	394	407	408	408
U236F	0.800	0.2936	270	390	408	408	408
U238F	0.976	0.3470	262	394	408	408	408
U238H	0.730	0.2674	263	389	408	408	408

Table 9.20: Differences between FISPIN calculation and six group model using the 6 parameter fits of Table 9.17.

System	Maximum % diff	%SD	number of points within standard deviations				
			1	2	3	4	5
AM241F	5.277	1.76997	284	384	408	408	408
AM241T	12.41	4.46131	277	379	408	408	408
AM242MF	13.37	4.70202	282	377	408	408	408
AM242MT	12.15	4.27126	280	377	408	408	408
AM243F	16.25	5.68500	286	374	408	408	408
AM243T	17.26	6.07802	288	375	408	408	408
CF252S	25.32	8.87814	298	373	408	408	408
CM242S	10.413	3.71415	278	381	408	408	408
CM243F	10.087	3.56741	278	380	408	408	408
CM243T	14.45	5.19135	282	377	408	408	408
CM244F	14.12	5.02283	282	377	408	408	408
CM244S	18.07	6.45693	286	374	408	408	408
CM244T	14.86	5.30635	283	378	408	408	408
CM245F	16.99	6.01770	289	374	408	408	408
CM245T	15.33	5.38727	288	376	408	408	408
NP237F	4.569	1.50362	282	383	404	405	408
NP237T	6.313	2.14711	281	381	408	408	408
NP238F	8.396	2.82976	285	379	408	408	408
NP238T	10.202	3.51224	280	378	408	408	408
PU238F	3.424	1.10436	290	381	403	404	408
PU238T	7.043	2.38741	282	381	408	408	408
PU239F	7.266	2.43468	283	379	408	408	408
PU239T	8.150	2.80030	280	381	408	408	408
PU240F	12.38	4.33948	280	377	408	408	408
PU241F	14.27	4.93830	287	376	408	408	408
PU241T	13.99	4.84020	286	376	408	408	408
PU242F	15.93	5.50193	289	374	408	408	408
TH232F	-5.790	2.18133	286	388	408	408	408
TH232H	-3.996	1.48478	298	384	408	408	408
U233F	5.535	1.90107	279	384	408	408	408
U233H	6.293	2.20002	274	386	408	408	408
U233T	5.270	1.70830	278	387	407	408	408
U234F	4.161	1.30596	276	387	406	407	408
U235F	3.424	1.06953	284	382	406	407	408
U235H	3.385	1.02755	291	378	406	407	408
U235T	2.201	0.873311	279	388	408	408	408
U236F	-2.949	1.15692	281	383	408	408	408
U238F	7.688	2.81241	266	387	408	408	408
U238H	6.469	2.27519	269	385	408	408	408

Table 9.21: Differences between FISPIN calculation and six group model using the 6 parameter fits of Table 9.18.

System	Maximum % diff	%SD	number of points within standard deviations				
			1	2	3	4	5
AM241F	2.214	0.75101	282	387	408	408	408
AM241T	6.570	2.3247	283	379	408	408	408
AM242MF	7.023	2.4645	285	378	408	408	408
AM242MT	6.302	2.2019	284	380	408	408	408
AM243F	8.813	3.0941	289	378	408	408	408
AM243T	9.395	3.2845	291	378	408	408	408
CF252S	14.60	5.1432	294	377	408	408	408
CM242S	5.261	1.8496	283	381	408	408	408
CM243F	5.085	1.7735	282	381	408	408	408
CM243T	7.742	2.7373	284	378	408	408	408
CM244F	7.502	2.6415	286	378	408	408	408
CM244S	9.910	3.4796	289	377	408	408	408
CM244T	7.968	2.8137	284	378	408	408	408
CM245F	9.262	3.2679	287	377	408	408	408
CM245T	8.375	2.9641	288	378	408	408	408
NP237F	1.761	0.58613	290	384	407	408	408
NP237T	2.854	0.99391	278	385	408	408	408
NP238F	3.936	1.3428	285	382	408	408	408
NP238T	5.033	1.7493	284	380	408	408	408
PU238F	-1.145	0.39214	304	383	408	408	408
PU238T	3.190	1.0934	284	384	408	408	408
PU239F	3.253	1.0866	282	381	408	408	408
PU239T	3.888	1.3463	281	383	408	408	408
PU240F	6.560	2.3255	283	380	408	408	408
PU241F	7.637	2.6771	288	378	408	408	408
PU241T	7.396	2.5772	288	378	408	408	408
PU242F	8.639	3.0112	291	378	408	408	408
TH232F	-3.171	1.2232	281	390	408	408	408
TH232H	-2.119	0.81461	285	387	408	408	408
U233F	-3.552	1.3251	286	382	408	408	408
U233H	-3.740	1.4532	279	383	408	408	408
U233T	-3.151	1.1599	289	378	408	408	408
U234F	-2.511	0.94849	284	384	408	408	408
U235F	2.561	0.91626	286	382	408	408	408
U235H	-2.024	0.77499	283	382	408	408	408
U235T	0.9155	0.26491	273	395	406	407	408
U236F	1.840	0.34728	301	390	403	404	408
U238F	3.547	1.2526	283	384	408	408	408
U238H	2.938	1.0309	282	385	408	408	408

The following figures are an example of the results obtained from the calculations. They show the delayed neutron emission rates for the thermal neutron fission of ^{235}U and ^{239}Pu , and the fast neutron fission of ^{238}U . Both the pulse and long irradiation results are shown. To show this work in context the figures plot the results of the FISPIN calculation, the six group parameter fits to this and the six group parameters published by other workers.

The other workers who have published complete six group parameters include Keepin^[9.2], Brady and England^[9.6] and Waldo^[9.10]. The work of Keepin and Waldo are based upon experimental measurements. The Brady and England work is based upon summation calculations. Brady and England based their work on the update of the Meek and Rider fission yields and the ENDF/B-V decay data. They augmented the decay data with model calculations of P_n values and individual nuclides' delayed neutron spectra. They were thus able to also produce estimates of the delayed neutron spectra after fission.

The differences from the "long" irradiation case FISPIN results are shown for each of the six group parameter sets in a second figure.

When comparing the results it should be born in mind that experiments have difficulty in measuring the neutron emission at very long times after irradiation due to the fall off of the delayed neutron emission to below the experimental noise. Also, the short lived groups cannot be measured directly as moderated neutrons from the irradiation will still be present. One common technique to measure the short lived groups is to use a pulsed irradiation. The long-lived groups and the moderated neutrons then become a background that can be subtracted. However, at very short times, this background will swamp the neutron emission being measured. Thus the short and long measurements will not be as accurate as those at the middle of the range. Also the accuracy of the six group model will be less than that for $\bar{\nu}_d$.

The six group half-lives vary from ~0.2 to 60 seconds. Thus if any neutron emission occurs outside of this time window it cannot be accurately represented by the model.

Figure 9.1: The delayed neutron emission rate following a pulse and long irradiation for the thermal neutron fission of ^{235}U .

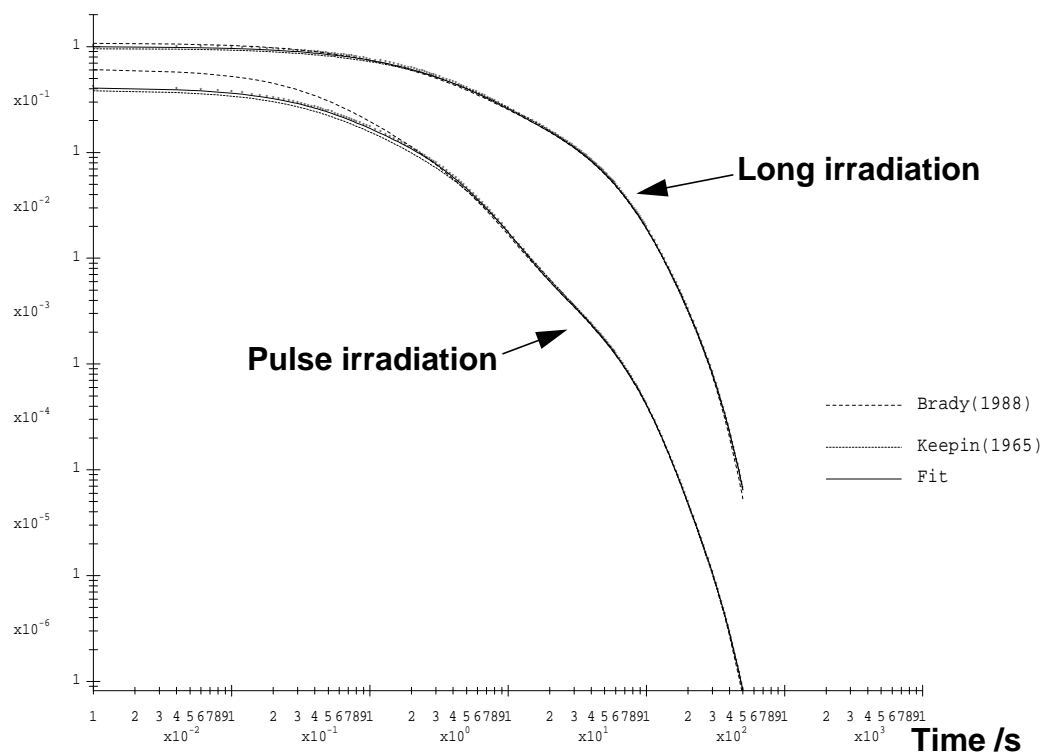


Figure 9.2: Percentage difference between the long irradiation FISPIN calculations and 6 group parameters for the thermal neutron fission of ^{235}U

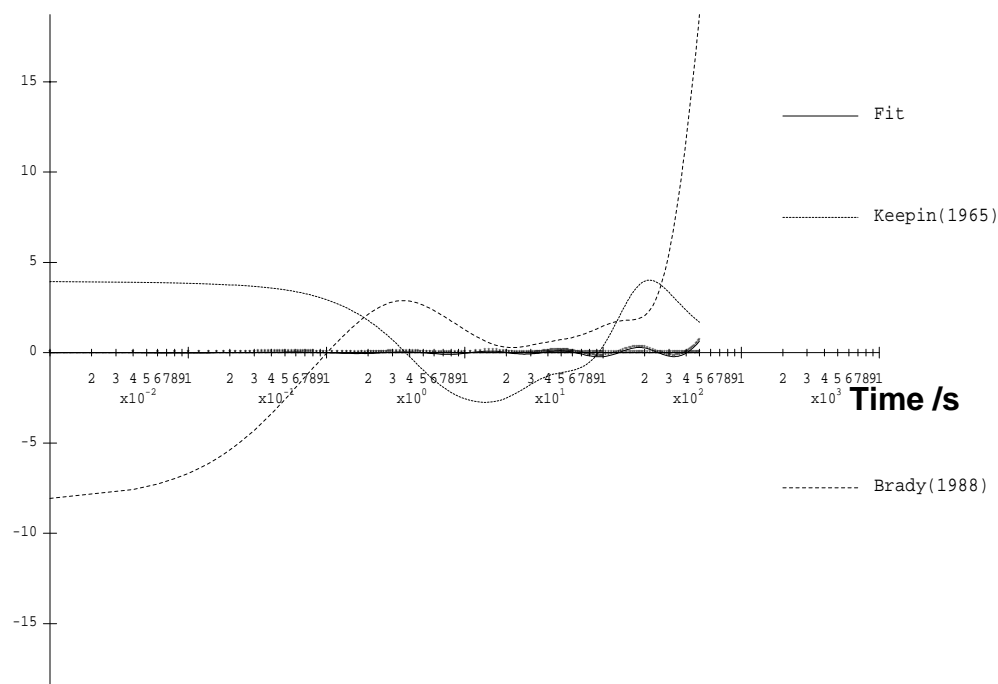


Figure 9.3: The delayed neutron emission rate following a pulse and long irradiation for the thermal neutron fission of ^{239}Pu .

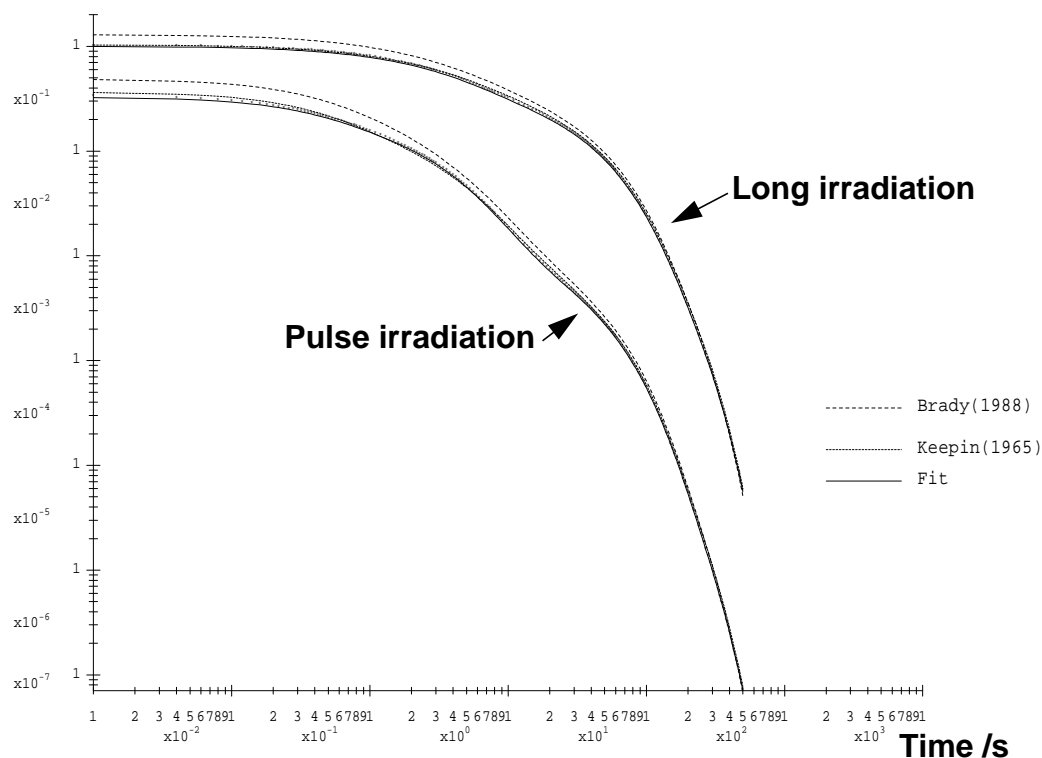


Figure 9.4: Percentage difference between the long irradiation FISPIN calculations and 6 group parameters for the thermal neutron fission of ^{239}Pu

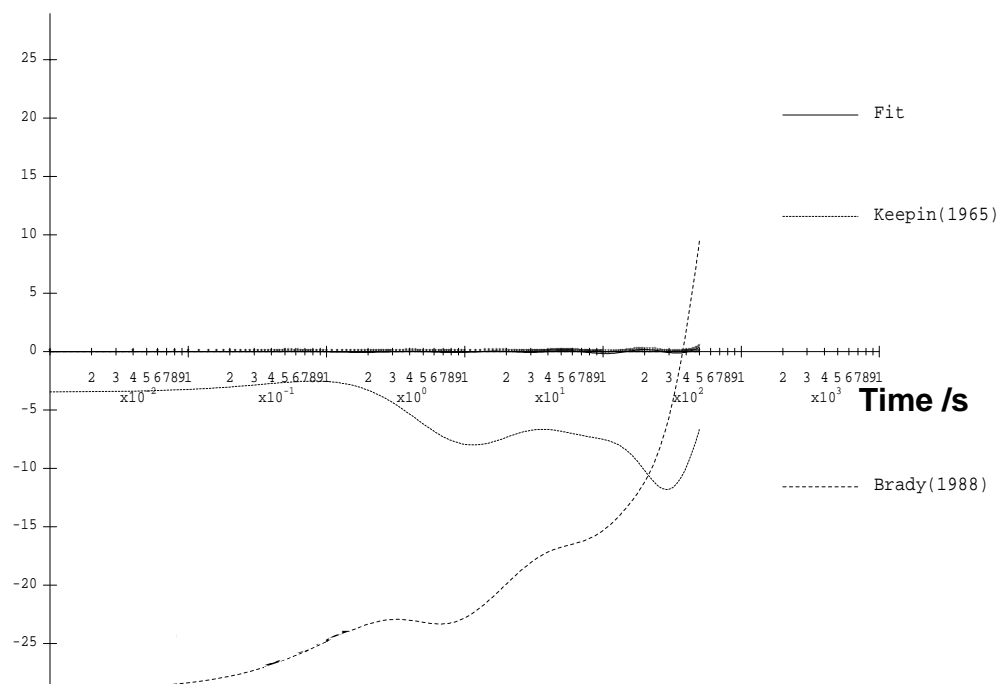


Figure 9.5: The delayed neutron emission rate following a pulse and long irradiation for the fast neutron fission of ^{238}U .

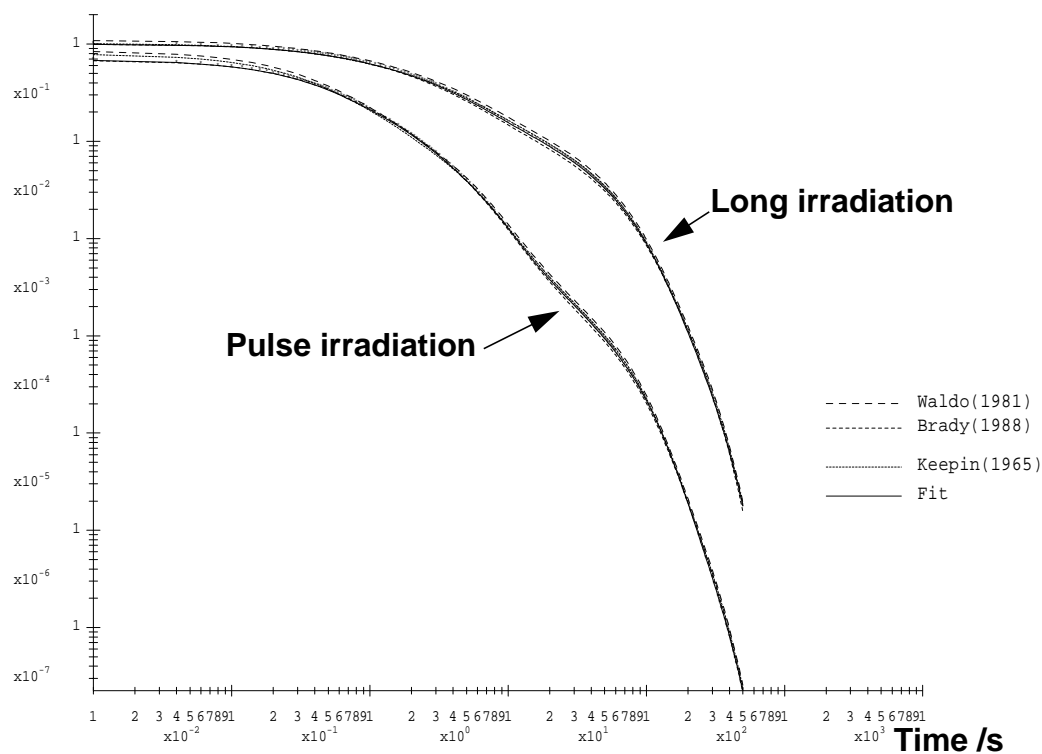
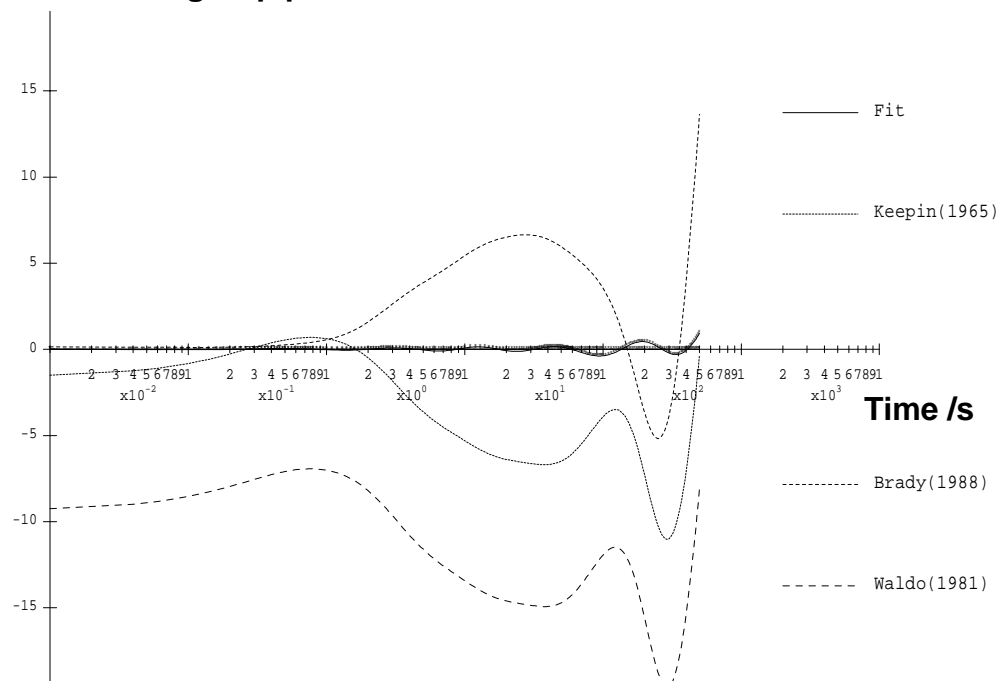


Figure 9.6: Percentage difference between the long irradiation FISPIN calculations and 6 group parameters for the fast neutron fission of ^{238}U .



The majority of the differences in these figures can be attributed to the different values of $\bar{\nu}_d$ used in the calculations. This can be seen on the figures showing the differences, because at zero time after the “long” irradiation the neutron emission rate will equal the $\bar{\nu}_d$ value. Thus the differences at zero time are directly related to the $\bar{\nu}_d$ values used.

In the region up to 200 seconds the remaining differences are of the same order as the uncertainty on $\bar{\nu}_d$. For times greater than 200 seconds the neutron emission has dropped to such a level that the differences have no practical significance.

9.3.2 Decay heat calculations

Another method of testing the fission yield dataset is in calculation of decay heat using decay data and fission yields in an inventory code. The FISPIN code used for the delayed neutron calculations above also generates the power produced by decay of fission products. Thus the energy released per fission can be extracted from the “long” irradiation FISPIN models. This requires the approximation described above that the rate of emission at zero time after a “long” irradiation is equal to the total emission following a single ‘average’ fission.

The decay power in FISPIN is generated by calculating the activity of each fission product. The average baryon, lepton and photon release per decay (often loosely referred to as the alpha, beta and gamma energy release per decay) in the decay data file is then used to calculate the components of the energy release. These components can then be summed over all fission products to produce totals. It should be noted that the ENDF/B decay data format includes the delayed neutron energy release in the alpha energy release values as this covers all baryons.

The version of FISPIN used in these calculations also used the total energy release for each decay branch in the decay data. This is calculated from the binding energies and is given in the decay data file. Hence a total decay power including neutrinos was also generated. The neutrino energy release was thus calculated by subtraction. The results of these calculations are shown in Table 9.22 for each of the 39 fissioning systems.

Table 9.22: Calculated delayed energy release per fission.

Nuclide	Average delayed energy release per fission in MeV				
	Total	beta	gamma	alpha	neutrino
AM241F	15.7390	4.79557	4.42494	1.94255E-04	6.5183
AM241T	16.0106	4.90415	4.44575	1.26687E-04	6.6606
AM242MF	17.5343	5.34123	4.96844	1.58028E-04	7.2245
AM242MT	18.0544	5.52760	4.97669	1.94630E-04	7.5499
AM243F	19.5907	5.99902	5.54356	2.16633E-04	8.0479
AM243T	19.8362	6.07784	5.58494	2.44248E-04	8.1732
CF252S	19.8770	6.21047	5.20475	1.30202E-04	8.4617
CM242S	12.5941	3.84906	3.58749	3.63303E-05	5.1575
CM243F	14.0780	4.26621	3.99532	7.87618E-05	5.8164
CM243T	14.3828	4.39328	4.03421	6.90842E-05	5.9552
CM244F	15.7202	4.77613	4.43039	1.01247E-04	6.5136
CM244S	15.9284	4.88581	4.47624	7.71950E-05	6.5663
CM244T	15.7734	4.79532	4.44029	1.00561E-04	6.5377
CM245F	17.0605	5.19413	4.79192	1.30464E-04	7.0743
CM245T	17.4481	5.32354	4.86709	1.32539E-04	7.2573
NP237F	19.7303	6.00895	5.48515	3.76642E-04	8.2358
NP237T	19.9430	6.08048	5.46396	4.17397E-04	8.3981
NP238F	21.3995	6.54241	5.92135	4.02045E-04	8.9353
NP238T	21.3399	6.53268	5.89469	4.48627E-04	8.9121
PU238F	15.7993	4.79294	4.47115	1.98432E-04	6.5350
PU238T	15.5911	4.71935	4.49008	1.06685E-04	6.3816
PU239F	17.6549	5.36554	5.00604	2.07672E-04	7.2831
PU239T	17.7189	5.40062	4.95770	1.99531E-04	7.3604
PU240F	19.2116	5.86983	5.37211	2.21704E-04	7.9694
PU241F	21.8447	6.71432	6.03755	3.11226E-04	9.0925
PU241T	21.9267	6.73069	6.05606	3.46218E-04	9.1396
PU242F	23.6137	7.27032	6.46576	3.96404E-04	9.8772
TH232F	27.3841	8.22437	7.79775	1.56241E-03	11.360
TH232H	22.8252	6.81977	6.83133	1.11457E-03	9.1730
U233H	13.6818	4.04465	4.24601	3.85983E-04	5.3908
U233T	17.0150	5.06582	4.94797	5.75037E-04	7.0006
U234F	18.6637	5.60385	5.32437	5.89650E-04	7.7349
U235F	21.7001	6.58928	6.05029	5.54042E-04	9.0600
U235H	17.2386	5.14087	5.16158	4.30630E-04	6.9357
U235T	21.5246	6.53190	5.95720	6.30297E-04	9.0349
U236F	23.2179	7.05850	6.41035	6.70750E-04	9.7484
U238F	27.8521	8.54696	7.53807	7.12207E-04	11.766
U238H	23.5930	7.18285	6.70420	6.00352E-04	9.7054

There exist several published evaluations for the energy release per fission. The values published by James^{[9.18][9.19]} are shown in Table 9.22, along with comparison with the calculations above.

Table 9.23: Comparison of calculations and the James evaluation of beta and gamma energy release from fission.

Fissioning system	Average delayed energy release per fission in MeV					
	beta			gamma		
	Evaluated	Calculated	Difference/standard deviation	Evaluated	Calculated	Difference/standard deviation
TH232F	8.3 ± 0.6	8.2	-0.2	8.6 ± 2.0	7.8	-0.5
U233T	5.7 ± 0.4	5.1	-1.5	5.9 ± 1.3	4.9	-0.8
U234F	6.2 ± 0.5	5.6	-1.2	6.4 ± 1.3	5.3	-0.7
U235T	7.0 ± 0.3	6.5	-1.7	7.2 ± 1.1	6.0	-1.1
U236F	7.5 ± 0.5	7.1	-0.8	7.7 ± 1.7	6.4	-0.8
U238F	8.9 ± 0.6	8.5	-0.7	8.4 ± 1.6	7.5	-0.6
Np237T	6.4 ± 0.5	6.0	-0.8	6.6 ± 1.4	5.5	-0.8
Pu238T	5.5 ± 0.4	4.7	-2.0	5.7 ± 1.2	4.5	-1.0
Pu239T	6.1 ± 0.6	5.4	-1.2	6.1 ± 1.3	5.0	-0.8
Pu240F	6.5 ± 0.5	5.9	-1.2	6.8 ± 1.4	5.4	-1.0
Pu241T	7.4 ± 0.6	6.7	-1.2	7.8 ± 1.6	6.1	-1.1
Pu242F	8.0 ± 0.6	7.3	-1.2	8.2 ± 1.6	6.5	-1.0

It is interesting that the beta energy release is under-estimated by around 0.5 MeV and the gamma energy release is under-estimated by 1.5 MeV. These differences are either due to an under-estimation by summation or an over-estimation in the evaluation.

A second evaluation by Beck^[9.20] was similarly compared. These results are shown in Table 9.22. The results show a similar beta energy under-estimate of around 0.5 MeV and a gamma under-estimate around 0.8 MeV.

The experimental delayed energy release data available is minimal. These evaluations of delayed energy release depend upon extrapolation from the thermal neutron fission of

[9.18] Journal of Nuclear Energy, Vol. 23, p517-536. M.F.James (1969).

[9.19] Journal of Nuclear Energy, Vol. 25, p513-523. M.F.James (1971).

[9.20] "The components of fission energy release for 17 actinides", Stanford University (U.S.A.), Thesis by C.A.Beck (1978).

Table 9.24: Comparison of calculations and the Beck evaluation of beta and gamma energy release from fission.

Fissioning system	Average delayed energy release per fission in MeV					
	beta			gamma		
	Evaluated	Calculated	Difference/standard deviation	Evaluated	Calculated	Difference/standard deviation
TH232F	8.2 ± 0.5	8.2	0.0	8.0 ± 0.75	7.8	-0.3
U233T	5.6 ± 0.5	5.1	-1.0	5.5 ± 0.75	4.9	-0.8
U234F	6.1 ± 0.5	5.6	-1.0	5.9 ± 0.75	5.3	-0.8
U235T	6.9 ± 0.3	6.5	-1.3	6.7 ± 0.5	6.0	-1.4
U236F	7.4 ± 0.5	7.1	-0.6	7.2 ± 0.75	6.4	-1.1
U238F	8.7 ± 0.5	8.5	-0.4	8.5 ± 0.75	7.5	-1.3
Np237T	6.2 ± 0.5	6.0	-0.4	6.1 ± 0.75	5.5	-0.8
Pu238T	5.4 ± 0.5	4.7	-1.4	5.3 ± 0.75	4.5	-1.1
Pu239T	6.0 ± 0.5	5.4	-1.2	5.9 ± 0.75	5.0	-1.2
Pu240F	6.4 ± 0.5	5.9	-1.0	6.3 ± 0.75	5.4	-1.2
Pu241T	7.3 ± 0.5	6.7	-1.2	7.1 ± 0.75	6.1	-1.3
Pu242F	7.7 ± 0.5	7.3	-0.8	7.6 ± 0.75	6.5	-1.5

^{235}U to fill many of the gaps in the data.

The data used by James(1969) for the beta energy release from thermal neutron fission of ^{235}U are based upon the work of Carter et al^[9.21], McNair et al^[9.22], McMahon^[9.23] and Armbruster^[9.24]. Some of these values were modified after private communication between James, his colleagues and the authors. These results are shown in Table 9.25.

Table 9.25: Experimental measurements of the beta energy release from fission for thermal neutron fission of ^{235}U .

Reference	Energy per fission
Carter et al (1959)	7.1 ± 0.6
Armbruster (1962)	7.75 ± 0.28
McNair et al (1965)	6.73 ± 0.35
McMahon (1968)	6.3 ± 0.5

[9.21] Phys. Rev. 113, 280. R.E. Carter, F.Reines, J.J. Wagner and M.E. Wyman (1959).

[9.22] Report AWRE 0-95/65. A.McNair, F.J. Bannister, R.L.G. Keith and H.W. Wilson (1965)

[9.23] Thesis, University of Strathclyde. T.D.McMahon (1968)

[9.24] Z.f. Phys., 170, 274. P.Armbruster and H. Meister (1962)

From these results it is immediately obvious that the Armbruster result is significantly higher than the other measurements, although this result has the smallest quoted uncertainty.

James in his work used an unweighted mean because of this obvious discrepancy. This gave a value of 7.0 ± 0.4 . Applying a weighted mean gives a value of 7.2 ± 0.3 . The normalized residual technique, described in chapter 3, gives 7.1 ± 0.3 . If, however, the Armbruster result is removed the weighted mean becomes 6.7 ± 0.2 .

It is interesting to speculate that if the James beta energy release evaluations were scaled down by 0.3 MeV, about half of the discrepancy between the evaluation and calculation would be resolved. However, considering the uncertainties of the summation calculation, and of the experimental measurements no valid conclusions can be drawn from the differences between the calculations and the previous evaluations.

10 Summary of results and areas of future work

10.1 Experimental data and analysis

The UKFY3 experimental database considerably extends the UKFY2 database and has allowed an improved study of fission yield systematics to be carried out. There are now a reduced number of discrepancies within the file, however many still remain which need to be resolved.

New experimental work currently being carried out will allow much greater understanding of the mass, charge and isomeric fission product yield distributions and these should be incorporated in future evaluations. Two experimental programmes are especially important. The first is the work of Mutter at Darmstadt, Germany, using the Heidelberg-Darmstadt Crystal-Ball-Spectrometer. This allows the mass and nuclear charge of fission fragments, mass and nuclear charge of ternary fragments, angular distribution in coincidence with gamma-rays and neutrons emitted and their angular distribution to be measured for a single fission event. These data will allow a greater understanding of the production of fission products and may lead to new predictive theories. The second is the program of Rudstam at Studsvik, Sweden, who will soon publish new the fractional independent and isomeric yield measurements for the fast neutron fission of ^{238}U and ^{232}Th .

10.2 Chain yields

The chain yield data can be fitted effectively by the five Gaussian model, and the parameters can be extrapolated for unmeasured systems. However, the fine structure on the mass distributions, believed to be the result of an odd-even effect and prompt neutron emission, has yet to be satisfactorily modelled. Modelling of this fine structure may allow the five Gaussian model to be significantly improved.

There is still a need for some yields to be better known, especially those used for determining the burn-up of spent nuclear fuel, which would allow higher accuracy in these analyses. The work of Mutter and Rudstam soon to be published will allow greater understanding of the chain yield distributions.

10.3 Ternary yields

This work has shown that the alpha yields are dependent upon the initial, and not compound, nucleus parameters. Also, the alpha and tritium yields cannot be shown to have any strong energy dependency. New work by Wagemans at Geel, Belgium, will allow greater testing of this energy independence approximation. These empirical results suggest either that the extra mass and energy added to the compound nucleus by a neutron does not significantly alter the nuclear parameters effecting light charged particle emission or that some form of compensation is occurring between the neutron energy and the resultant yields.

The hydrogen yields have been shown to be a constant fraction of the alpha yield over a wide range of nuclides suggesting that the triton and alpha particle production processes are linked.

10.4 Fractional independent yields

The fractional independent Z_p model was used to fit the UKFY3 experimental data. It was found that more fissioning systems could be fitted in this work than for UKFY2. However, the data needs to be examined in more detail to remove the remaining discrepancies in UKFY3. This is especially true for yields of isomeric states where many discrepancies still exist. New data, primarily from Rudstam, may allow some of these discrepancies to be resolved and a greater understanding of the charge distribution may be obtained.

If the fitting of the Z_p model can be improved, by removing discrepancies and adding new experimental data, it would then be worthwhile to try to implement Wahl's more detailed A_p ' model.

10.5 Independent yield isomeric splitting

The Rudstam extension of the Madland and England model allows a considerable improvement to be made to the modelling of isomeric splitting. However, this model requires more experimental data before the parameters can be extrapolated to other fissioning systems. Until such time as these parameters can be modelled the Madland and England model, or experimental data must be used. The UKFY3 experimental data

still contains many discrepancies for this data type and further work is suggested in order to remove these.

10.6 The production of the UKFY3.0 evaluated file

A new library of independent and cumulative yields have been produced for a selected set of nuclides considered important for applications. Improved understanding of fission product yield systematics from the study of UKFY3 has considerably improved the file.

10.7 Testing of the UKFY2 and UKFY3.0 data libraries

The UKFY2 evaluated file has been used to generate decay heat and delayed neutron emission for the fissioning systems evaluated. So far the UKFY3.0 evaluation has only been used to generate the average number of delayed neutrons per fission. The UKFY3.0 testing should be extended to the same level as employed for UKFY2. Also, the UKFY3.0 evaluated file should now be used in spent fuel inventory calculations and the results compared with post irradiation experimental analyses.

Some yields important for applications should be studied in depth to remove discrepancies, e.g. where the UKFY3 and latest US evaluations differ significantly. Especially important in this regard are the yields of ^{148}Nd , ^{137}Cs and ^{140}Ba which are used for many applications.

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Appendices

- A.1 Chain and cumulative yield tables
- A.2 Discrepancy tables for chain yield data
- A.3 Fractional independent yield tables
- A.4 Discrepancy tables for fractional Independent yields
- A.5 Experimental reference list
- A.6 Computer codes used in the UKFY3 evaluation

A.1 Chain and cumulative yield tables

These tables contain experimental values for chain yields and cumulative yields for isobars near the stable ends of mass chains. In averaging the data, a cumulative yield was only included if the sum of fractional independent yields for subsequent isobars is so small that the cumulative yield should be a good estimate of the chain yield.

These Tables give in successive columns:

- i The mass number
- ii An asterisk * after the mass shows that the automatic down-weighting procedure has been used for at least one measurement.
- iii The element and any isomeric state identifier.
- iv The source of the value is given as a number corresponding to its reference in Appendix A.5.
- v If the measurement was relative, or ratio of ratio, the reference number is followed by 'r'.
- vi The measured data. The yield is given as a percentage per fission, and the standard deviation as a percentage of the yield. For a relative measurement, the yield was calculated using standard yields from a preliminary evaluation involving absolute measurements only. For absolute measurements the standard deviation is the value stored in the UKFY3 database. For relative measurements, the percentage uncertainties of the experiment and of the evaluated standard yields are combined in quadrature.
- vii A 'W' after the percentage standard deviation indicates that the measurement was down-weighted using the method of reduced residuals. This technique was applied if a measurement was discrepant and no resolution of the discrepancy could be found by further study of the relevant reference.
- viii If a chain having an isobar, near enough to the stable end for its cumulative yield to be a good measure of the chain yield, which has an isomer, then the calculated cumulative yields of ground and excited state, and direct measurements of the chain yield, are averaged separately and shown.

- ix The normalised residual of the measured value.
- x If a chain having an isobar, near enough to the stable end for its cumulative yield to be a good measure of the chain yield, which has an isomer, then the values of χ^2 per degree of freedom are given separately for data for each isomer and for direct data for the chain yield. Cases for which $\chi^2 > 2$ are flagged, to indicate discrepancies.
- xi The separate weighted means of the cumulative yields of each isomer and of the chain yield are adjusted to give consistency. The contribution to χ^2 from this is then given.
- xii In the results section of the table the first parameters are the total χ^2 and χ^2 per degrees of freedom .
- xiii The weighted mean chain yield and its percentage standard deviation is then given. Both internal 'I' and external 'E' standard deviations are quoted.
- xiv The larger of the internal and external standard deviations is flagged by an 'A' and is taken as the recommended standard deviation.
- xv Discrepant sets of data are flagged, if χ^2 per degrees of freedom are >1 or > 2 .

Index of Cumulative and Chain yield Tables

[illegible]

A.2 Discrepancy tables for chain yield data

These Tables refer to the experimental data tables in appendix A.1. They summarize the deficiencies in these chain yields measurements.

A table is included for each fissioning reaction (i.e. for each fissile nucleus and incident neutron energy). Successive columns give the mass number of the fission product chain, the number of measurements (if any), the reference number and the contribution to χ^2 of the most discrepant measurement, the value of the total χ^2 , and the probability of such a value arising by chance. An entry is made if the probability is less than 10%, and the line has a flag for additional emphasis if it is less than 1.5% or 0.01%. A “w” at the head of the line shows that automatic down-weighting has been applied to at least one measurement (probably the one specified), but that the discrepancy remained: the χ^2 and the probability are those subsequent to the down-weighting. Of course, the listing of the most discrepant measurement should not be taken as indicating that it is inevitably the most suspect: all data should be re-investigated in any detailed evaluation of the chain.

If there is only one measurement, this is stated and the reference number given. An entry is made in this case because it is felt very strongly that any single experiment needs confirmation by others.

There are also clearly labelled entries for chains with no measurements.

An entry reading ‘DATA BUT NOT “INCLUDED”’ indicates that measurements have been made but only on fission products too far along the chain for them to be good estimates of the chain yield.

A.3 Fractional Independent yield tables

These Tables of fractional independent yields give in successive columns:

- i The mass number.
- ii The chemical symbol, and whether the measurement was for the ground state (G), the first or second excited state (M or N), or for all states combined (T).
- iii The reference number.
- iv The value for the fractional independent yield derived from this measurement.
- v The percentage standard deviation.
- vi The reduced residual (defined in chapter 3).
- vii The type of measurement:

FractInd	Direct measurement of the fractional independent yield.
Ind/Y(A)	A measurement of the independent yield converted to a fractional yield by dividing by the chain yield obtained by evaluation of measurements given in the Tables of Appendix A.1.
Ind/I(A)	A measurement of the independent yield converted to a fractional yield by dividing by the chain yield obtained by interpolation between yields of neighbouring chains, no measurements of this chain yield being available.
Ind/C(A)	A measurement of the independent yield converted to a fractional yield by dividing by the chain yield obtained from a 5-Gaussian fit, no measurements of this or of neighbouring chain yields being available.
- viii The weighted mean of the measurements.
- ix The value of χ^2 / degrees of freedom.
- x The internal percentage standard deviation (I).
- xi The external percentage standard deviation (E).
- xii The recommended percentage standard deviation (A), which is the larger of the two previous columns.

Index of fractional independent yield tables

TABLE	1	ENERGY:THERMAL	NUCLIDE:TH-229
TABLE	2	ENERGY:THERMAL	NUCLIDE:U -233
TABLE	3	ENERGY:THERMAL	NUCLIDE:U -235
TABLE	4	ENERGY:THERMAL	NUCLIDE:NP-237
TABLE	5	ENERGY:THERMAL	NUCLIDE:NP-238
TABLE	6	ENERGY:THERMAL	NUCLIDE:PU-238
TABLE	7	ENERGY:THERMAL	NUCLIDE:PU-239
TABLE	8	ENERGY:THERMAL	NUCLIDE:PU-241
TABLE	9	ENERGY:THERMAL	NUCLIDE:AM-241
TABLE	10	ENERGY:THERMAL	NUCLIDE:AM-242
TABLE	11	ENERGY:THERMAL	NUCLIDE:CM-245
TABLE	12	ENERGY:THERMAL	NUCLIDE:CF-249
TABLE	13	ENERGY:FAST	NUCLIDE:TH-232
TABLE	14	ENERGY:FAST	NUCLIDE:U -235
TABLE	15	ENERGY:FAST	NUCLIDE:U -236
TABLE	16	ENERGY:FAST	NUCLIDE:U -238
TABLE	17	ENERGY:FAST	NUCLIDE:NP-237
TABLE	18	ENERGY:FAST	NUCLIDE:PU-239
TABLE	19	ENERGY:FAST	NUCLIDE:PU-240
TABLE	20	ENERGY:HIGH	NUCLIDE:TH-232
TABLE	21	ENERGY:HIGH	NUCLIDE:U -233
TABLE	22	ENERGY:HIGH	NUCLIDE:U -235
TABLE	23	ENERGY:HIGH	NUCLIDE:U -238
TABLE	24	ENERGY:HIGH	NUCLIDE:PU-239
TABLE	25	ENERGY:HIGH	NUCLIDE:AM-241
TABLE	26	ENERGY:SPONT.	NUCLIDE:CM-244
TABLE	27	ENERGY:SPONT.	NUCLIDE:CF-252
TABLE	28	ENERGY:SPONT.	NUCLIDE:FM-254

A.4 Discrepancy Tables for Fractional Independent yields

These tables refer to the experimental data tables in appendix A.3. They summarize the deficiencies in these fractional independent yields measurements.

A table is given for each fissioning system. Fractional independent yields with discrepant measurements are shown. Each entry lists the mass number, the chemical symbol of the nuclide, the value of χ^2 per degrees of freedom, the probability of this value arising by chance, and the number of measurements. A “w” at the start of a line shows that automatic down-weighting has been applied to at least one of the measurements. A flag at the end of the line shows if the probability falls below 1.5% or 0.01%.

A.5 Experimental reference list

This appendix lists the references for the UKFY3 database. These reference numbers are detailed in this appendix. The reference numbers are divided into five section each with a range of values.

These are:

- The Crouch database (1981) 1 to 1190
- The Banai reference list (1986) 1191 to 1206
- The James and Mills list (upto 1993). 2000 to 2115
- Data extracted from the EXFOR database
(Last update August 1993) 10433-77500 (not continuous)
- Data that requires special note are prefixed
by a nine 90000-92043 (not continuous)

Where possible the references are abbreviated using the standard CINDA and EXFOR journal and report codes, as given in the “CINDA93” book^[2.6]

A.6 Computer codes used in the UKFY3 evaluation

The following are the computer codes used to produce the UKFY3.0 evaluated file. For each code the purpose and UNIX run commands are given.

- **ANALYSE**

Purpose: To analyse the experimental data

To run: `cd ~/fy/Analysis/shell`
`csH runx`

To test for convergence of iteration 5 the following commands are executed.

```
cd ~/fy/Analysis/datafiles
diff -rs 5 6
```

- **FOUTPUT**

Purpose: To format the tables output from ANALYSE.

To run: `cd ~/fy/Analysis`
`echo 0 | fortran/foutput/foutput.out`

The FOUTPUT code reads yield masses for which to prepare tables from the standard input until "0" is entered. If no masses are selected then all masses are printed. This allows listings tailored to individual requirements. The output is left in the directory ~/fy/Analysis/output_short.

- **MKCHAIN**

Purpose: To combine the experiment data with model estimates to generate complete fission product chain yield distributions for UKFY3.

To run: `cd ~/fy/Analysis/fortran/mkchain_ukfy3`
`mkchain.out > mkchain.log.301094`

Output files are stored in ~/fy/Library/data/chain_ukfy3.

- **MKFIND**

Purpose: To generate complete sets of fractional independent yields.

To run: `cd ~/fy/Analysis/fortran/mkfind_ukfy3`

`mkfind.exe`

The output files were placed in the directory `~/fy/Analysis/data/find_ukfy3`.

- **FITFYS_SCAN**

Purpose: To adjust the fission product yield data sets with different numbers of constraints to determine how many constraints should be applied.

To run: `cd ~/fy/Library/fitfys_jef2`

`OBJ/run_scan.out`

- **FITFYS**

Purpose: To adjust the fission product yield data sets and produce adjusted independent yield files.

It is first necessary to edit `setdat.f` to include the number of constraints to apply.

To run: `cd ~/fy/Library/fitfys_jef2`

`OBJ/run_scan.out`

- **DECAY_PROG**

Purpose: To produce adjusted independent and cumulative yields in ENDF-6 format.

To run: `cd ~/fy/Library/decay_prog`

`OBJ/run.out`

- **MAKEQ**

Purpose: To generate the Q matrix required by the DECAY_PROG code.

To run: `cd ~/fy/Library/decay_data/makeq`
`makeq.exe`

- **MKUKFY3**

Purpose: To generate the complete ENDF-6 formatted file, UKFY3.0, from the outputs of DECAY_PROG.

To run: `cd ~/fy/Library/decay_prog/mkukfy3`
`mkukfy3.exe`

TABLE 1 CHAIN AND CUMULATIVE YIELDS FROM THERMAL FISSION OF 227TH.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXT./DF	INT.	EXT./DF	MEAN	DEVIATION
77 AS	21496	1.400E+00	20.0				1.400E+00	20.0
83 BR	21496	1.100E+00	31.8					
89 SR	21496	8.000E+00	5.4				8.000E+00	5.4
90 SR	21496	8.720E+00	10.0				8.720E+00	10.0
91 SR	21496	6.210E+00	15.6				6.210E+00	15.6
95 ZR	21496	3.400E+00	8.5				3.400E+00	8.5
97 ZR	21496	2.410E+00	23.7				2.410E+00	23.7
99 MO	21496	1.440E+00	9.7				1.440E+00	9.7
103 RU	21496	5.800E-01	15.5				5.800E-01	15.5
105 RU	21496	2.800E-01	14.3				2.800E-01	14.3
106 RU	21496	1.900E-01	31.6				1.900E-01	31.6
109 PD	21496	3.300E-02	33.3				3.300E-02	33.3
111 AG	21496	5.100E-02	19.6				5.100E-02	19.6
112 PD	21496	2.900E-02	20.7				2.900E-02	20.7
113 AG	21496	3.400E-02	20.6				3.400E-02	20.6
115 CD	21496	1.770E-01	20.0				1.770E-01	20.0
121 SN	21496	1.100E-01	36.4					
125 SN	21496	4.300E-01	23.3					
127 SB	21496	6.800E-01	23.5				6.800E-01	23.5
TE	21496	5.300E-01	47.2					
129 TE(M)	21496	1.360E+00	20.6				1.360E+00	20.6
131 I	21496	2.610E+00	17.6				2.610E+00	17.6
132 TE	21496	3.300E+00	11.8				3.300E+00	11.8
133 I	21496	4.800E+00	21.0				4.800E+00	21.0
137 CS	21496	6.930E+00	17.9				6.930E+00	17.9
140 BA	21496	7.710E+00	15.0				7.710E+00	15.0
141 CE	21496	7.620E+00	6.7				7.620E+00	6.7
143 CE	21496	6.970E+00	6.9				6.970E+00	6.9
144 CE	21496	5.950E+00	7.4				5.950E+00	7.4
147 ND	21496	1.800E-01	27.8					

TABLE 2 CHAIN AND CUMULATIVE YIELDS FROM THERMAL FISSION OF 229TH.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXT./DF	INT.	EXT./DF	MEAN	DEVIATION
77 GE	640	1.100E-02	15.0				3.33	9.215E-03 (1) 19.7 >2
AS	300	1.050E-01	50.0	1.83				(E) 36.0A
CHAIN	2102	9.100E-03	20.0	-1.83				
78 GE	640	5.200E-02	15.0					2.030E-01 14.8
AS	2024	2.030E-01	14.8					
79 GE	12734	4.300E-01	18.6					4.300E-01 18.6
80 AS	12734	2.780E+00	28.1					2.780E+00 28.1
83*SE(G)	2024	3.150E+00	2.5					
12734	3.290E+00	4.6						
12807	3.420E+00	2.6						
SE(M)	2024	1.990E+00	7.0					
BR	640	6.400E+00	5.0W	0.49				
300	8.000E+00	30.0	1.23					
CHAIN	2102	4.510E+00	5.0W	-2.45				
84 SE	12734	1.380E+00	3.2					2.45 1.22 1.052E+01 (1) 2.4
2024	8.390E+00	3.6						(E) 2.6A
BR(G)	2024	1.012E+01	3.2	1.020E+01 -0.64	1.22			
640	1.090E+01	5.0	1.61					
12807	9.720E+00	5.8	-1.07					
BR(M)	2024	3.180E-01	3	3.180E-01				
85 SE	12734	7.500E+00	16.0					9.830E+00 15.0
KR(M)	2024	8.790E+00	3.4					
12807	9.200E+00	7.3						
CHAIN	2102	9.830E+00	15.0					
86 BR	12734	5.320E+00	10.2	-2.43				5.91 5.91 6.327E+00 (1) 5.5 >2
2024	7.050E+00	6.5	2.43					(E) 13.5A
87 KR	12807	6.380E+00	4.2	-0.08				
12734	6.460E+00	5.4	0.32					0.18 0.09 6.363E+00 (1) 0.8
88*BR	12734	3.130E+00	15.7					
KR	2024	5.80E+00	8.8W	-1.75				
12807	7.240E+00	8.8	0.24					(E) 4.2A
RB	640	7.660E+00	6.0	1.41				
12807	7.690E+00	6.1	1.44					
SR	224	3.012E+00	20.1					
CHAIN	2102	9.230E+00	10.0	2.38				
89 KR	12734	8.470E+00	7.7	-0.66				
2024	8.910E+00	2.2	0.13					7.16 1.19 8.889E+00 (1) 1.4
RB	12734	7.660E+00	7.2	-2.29				(E) 1.5A
2024	8.990E+00	2.0	0.76					
SR	300	7.200E+00	30.0	-0.78				
640	9.300E+00	5.0	0.92					
CHAIN	2102	8.600E+00	20.0	-0.17				
90 KR	12734	5.960E+00	10.4					0.72 0.72 8.367E+00 (1) 4.9A
RB(M)	12734	2.070E+00	6.8					(E) 4.2
SR	300	5.700E+00	30.0	-0.85				
640	8.400E+00	5.0	0.85					
91 RB	12734	4.350E+00	8.3					8.90 2.22 6.520E+00 (1) 2.1 >2
SR	300	5.700E+00	30.0	-0.40				(E) 3.1A
12807	6.250E+00	3.9	-1.27					
2024	6.590E+00	3.9	0.94					
Y (G)	640	7.400E+00	5.0	7.400E+00 0.00	5.65			
Y (M)	12807	3.790E+00	2.1	3.790E+00 0.00	0.00			

TABLE 2 CHAIN AND CUMULATIVE YIELDS FROM THERMAL FISSION OF 239TH.

(CONT.)

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXT.	INT.	EXT./DF	MEAN	DEVIATION		
=====										
CHAIN 2102 7.110E+00 10.0 6.386E+00 0.00 0.86										
92 SR	12807	5.430E+00 11.2	-0.86		2.86	0.71	5.927E+00 (I)	3.0A		
	2024	5.780E+00 4.2	-0.93					(E)	2.6	
Y 12807 6.685E+00 7.7										
	640	6.400E+00 8.0	0.35							
	640	6.400E+00 8.0	0.99							
CHAIN 2102 6.530E+00 10.0 0.96										
93*SR	12734	3.650E+00 11.8			7.00	3.50	4.938E+00 (I)	3.2 >2		
	12807	3.560E+00 11.5						(E)	6.0A	
	2024	4.400E+00 3.4								
	12807	4.500E+00 15.6								
Y 640 4.400E+00 6.0W										
	12807	5.020E+00 6.4	-2.46							
	2024	5.780E+00 4.2	0.30							
	640	6.400E+00 8.0	2.24							
94 SR	12734	3.180E+00 5.7			2.63	2.63	3.384E+00 (I)	6.4 >2		
Y 2024 3.150E+00 8.3										
	12807	3.910E+00 10.0	-1.62					(E)	10.4A	
	2024	3.910E+00 10.0	1.62							
95 Y	12734	2.350E+00 15.3			0.78	0.26	2.673E+00 (I)	2.4A		
ZR 2024 2.550E+00 6.3										
	640	2.600E+00 15.0	-0.84					(E)	1.2	
	300	2.600E+00 30.0	-0.19							
	300	2.600E+00 30.0	-0.09							
	12807	2.700E+00 2.6	0.88							
97 ZR	640	6.100E-01 15.0	-0.97		4.66	1.17	6.978E-01 (I)	1.6		
	12807	6.850E-01 4.5	-0.44					(E)	1.7A	
	12807	6.970E-01 2.1	-0.08							
	2024	7.000E-01 2.9	0.13							
CHAIN 2102 8.600E-01 10.0 1.90										
99*MO	2024	1.050E-01 9.5W	-1.52		10.17	3.39	1.225E-01 (I)	6.7 >2		
	640	1.500E-01 10.0W	2.24					(E)	12.3A	
	300	1.600E-01 50.0	0.47							
CHAIN 2102 3.300E-01 20.0W										
103 RU	300	4.300E-02 50.0	1.72		2.98	2.98	5.928E-03 (I)	9.9 >2		
	640	5.900E-03 10.0	-1.72					(E)	17.2A	
105 RU	300	2.500E-02 50.0	1.36		1.85	1.85	8.017E-03 (I)	5.0		
	640	8.000E-03 5.0	-1.36					(E)	6.8A	
106 RU	640	1.170E-02 9.0	-0.83		0.68	0.68	1.179E-02 (I)	8.9A		
	300	2.000E-02 50.0	0.83					(E)	7.3	
109 PD	300	1.300E-02 50.0	0.90		0.81	0.81	7.170E-03 (I)	9.8A		
	640	7.100E-03 10.0	-0.90					(E)	8.9	
111 AG	300	2.000E-02 50.0	-0.11		1.00	0.50	2.111E-02 (I)	4.9A		
	640	2.100E-02 5.0	-0.67					(E)	3.5	
CHAIN 2102 3.000E-02 30.0 0.99										
112 PD	300	800E-02 50.0	1.36		1.57	0.79	2.109E-02 (I)	4.9A		
	640	2.100E-02 5.0	-0.56					(E)	4.4	
CHAIN 2102 3.300E-02 30.0 1.21										
113 AG	640	1.440E-02 10.0	-1.32		3.95	1.98	1.482E-02 (I)	9.5		
	300	1.600E-02 50.0	0.15					(E)	13.5A	
CHAIN 2102 3.600E-02 30.0 1.98										
115 CD(G)	640	1.840E-02 5.0	-0.83		0.70	0.35	1.857E-02 (I)	4.8A		
	300	2.100E-02 50.0	0.23					(E)	2.8	
CHAIN 2102 2.200E-02 20.0 0.80										
117 CD	640	1.630E-02 12.0	-0.13		0.02	0.02	1.652E-02 (I)	6.0A		
IN 640 1.660E-02 7.0 0.13										
118 CD	640	1.740E-02 5.0	0.13					(E)	0.8	
	640	1.740E-02 5.0								
	640	1.740E-02 5.0								
121 SN	640	7.400E-03 5.0								
CHAIN 2102 1.200E-02 20.0 1.200E-02 20.0										

TABLE 2 CHAIN AND CUMULATIVE YIELDS FROM THERMAL FISSION OF 229TH.

(CONT.)

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXT.	INT.	EXT./DF	MEAN	DEVIATION		
=====										
CHAIN 2102 2.900E-02 50.0 1.77										
125 SN	300	2.900E-02 50.0			3.13	3.13	3.419E-03 (I)	28.9 >2		
SN(M) 640 2.200E-03 14.0										
CHAIN 2102 3.300E-03 30.0 -1.77										
126 CHAIN	2102	5.500E-03 20.0						5.500E-03	20.0	
127 SB	300	3.900E-02 50.0	1.75							
	640	8.400E-03 5.0	-1.75							
TE 300 4.000E-02 50.0										
CHAIN 2102 5.000E-03 20.0 -1.75										
129 SB	640	1.220E-01 7.0	-2.09		4.89	2.44	1.293E-01 (I)	6.0 >2		
	2024	1.700E-01 11.8	2.21					(E)	9.4A	
TE 300 1.210E-01 50.0 -0.10										
130 SB(G)	12734	1.500E-01 40.0	0.15		0.15	0.15	5.920E-01 (I)	10.6A		
	12807	1.740E-01 10.3	1.34					(E)	4.0	
SB(M) 12734 4.200E-01 14.3 4.200E-01										
131*SB	12734	5.800E-01 24.1	0.00		14.38	2.05	5.797E-01 (I)	1.9 >2		
	2024	7.220E-01 5.5W	2.15					(E)	2.8A	
TE 12807 4.400E-01 6.8W -2.33										
I 2024 6.90E-01 1.9W -0.19										
	12807	6.90E-01 2.3W	0.67							
	300	8.700E-01 50.0	-2.14							
CHAIN 640 4.300E-01 10.0W -2.14										
132*SB(G)	2024	5.760E-01 10.0	-0.07							
	12734	1.260E+00 11.9			9.96	1.99	1.201E+00 (I)	1.9		
SB(M) 12734 7.400E-01 6.8										
TE	12807	1.180E+00 2.5	-1.08					(E)	2.7A	
	300	1.230E+00 30.0	0.08							
	2024	1.400E+00 15.0	-2.50							
	640	8.700E-01 15.0W								
I 12807 1.250E+00 3.2 1.51										
CHAIN 2102 1.290E+00 10.0 0.70										
133*SB	2024	7.640E-01 6.5			8.16	2.04	3.075E+00 (I)	1.6 >2		
TE(G) 12807 1.420E+00 9.9										
	12734	1.490E+00 8.1						(E)	2.3A	
TE(M) 12807 8.600E-01 12.8										
I	12807	3.080E+00 1.9	0.14							
	2024	3.170E+00 3.2	1.09							
CS 223E2.382E+00 11.2W -2.49										
CHAIN 2102 2.910E+00 10.0 -0.58										
	640	4.000E+00 24.0	0.96							
134 TE	12807	4.760E+00 7.6			0.52	0.52	5.678E+00 (I)	7.9A		
	2024	5.120E+00 9.2						(E)	5.8	
	12734	5.720E+00 8.0								
I (G) 12807 5.950E+00 3.0										
	2024	6.340E+00 2.4								
I (M) 2024 2.150E-01 4.7										
	12734	9.700E-01 19.6								
CHAIN 640 5.300E+00 13.0 -0.72										
135 I	12807	4.980E+00 2.8	-0.44		0.00	0.00	2.8>2	1.39	5.092E+00 (I)	1.5
	12807	5.030E+00 5.1	0.00					(E)	1.7A	
	2024	5.030E+00 5.1	0.16							
XE(G) 2024 5.350E+00 3.2 5.350E+00 0.00 2.30										
XE(M) 2024 1.300E-01 46.1 1.300E-01 0.00 0.00										

TABLE 4 CHAIN AND CUMULATIVE YIELDS FROM THERMAL FISSION OF 233U . (CONT.)

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	YIELDS & SD	COMPONENT	VALUE	EXT.	DF	MEAN	DEVIATION	INT.	EXT./DF	MEAN	DEVIATION
105 RH	10918 9.690E-01	1.8	-0.58								
	1119 9.700E-01	3.0	-0.18								
106 RU	13054 1.500E-01	50.0	-1.35					9.06	1.29	2.508E-01	(I) 2.7
	42 1.570E-01	40.0	0.16								(E) 3.0A
	343 2.570E-01	15.0	0.27								
	305 2.590E-01	12.0	1.07								
	13361 2.800E-01	10.0	-0.98								
CHAIN	1119 2.410E-01	5.0	-0.87								
	247 2.420E-01	5.0	1.86								
107 RU	2023 1.110E-01	10.8	-0.40					0.16	0.08	1.156E-01	(I) 3.0A
	10918 1.160E-01	4.0	0.14								(E) 0.9
	10918 1.60E-01	5.2	0.09								
108 RU	2023 7.700E-02	6.5	-0.63					2.12	1.06	7.974E-02	(I) 3.1
	10918 8.600E-02	5.8	1.45								(E) 3.2A
109 PD(G)	13361 4.000E-02	10.0	-1.22					1.48	1.48	4.227E-02	(I) 8.4
	343 5.040E-02	15.0	1.22								(E) 10.2A
110 CHAIN	1119 3.990E-02	10.0	2.09								3.990E-02
	13054 1.444E-02	50.0	-1.47					7.75	1.94	2.483E-02	(I) 5.7
	305 1.870E-02	20.0	-1.77								(E) 7.9A
	343 2.360E-02	15.0	-0.38								
	13361 2.500E-02	10.0	0.08								
	2025r2.488E-02	8.3	2.09								
111 AG	305 1.250E-02	10.0	-1.83					3.64	1.82	1.438E-02	(I) 5.0
	343 1.500E-02	7.0	0.82								(E) 6.7A
	13361 1.600E-02	10.0	1.14								
115 CD(G)	343 1.710E-02	15.0	0.60					0.89	0.30	1.942E-02	(I) 7.8A
	13361 1.600E-02	10.0	0.60								(E) 4.3
CD(M)	13361 1.000E-03	10.0	0.37								
	343 1.070E-03	15.0	0.37								
CHAIN	21736r3.133E-02	60.1	0.40								
117 SN(G)	243 1.500E-02	7.0	-0.98								1.500E-02
	243 1.550E-02	7.0	0.08								1.550E-02
118 SN	243 1.550E-02	7.0	0.08								1.550E-02
119 SN(G)	243 1.580E-02	8.0	0.08								1.580E-02
120 SN	243 1.750E-02	7.0	0.08								1.750E-02
121 SN	13361 1.800E-02	10.0	-0.34					0.16	0.08	1.846E-02	(I) 6.3A
	2025r1.860E-02	9.6	0.10								(E) 1.8
	343 1.930E-02	15.0	0.32								
122 SN	243 1.950E-02	6.0	0.08								1.950E-02
123 SN(G)	13054 2.406E-03	50.0	0.08								
124 SN	243 3.220E-02	7.0	0.08								3.220E-02
125 SN	13361 5.000E-02	10.0	0.08								1.160E-01
SN(G)	13054 1.925E-02	50.0	0.08								
	2025r3.788E-02	8.4	0.08								
	343 5.790E-02	15.0	0.08								
CHAIN	247 1.160E-01	12.0	2.05					4.19	4.19	4.564E-01	(I) 11.1 >2
127 SB	305 5.900E-01	14.0	2.05								
TE(M)	13054 6.449E-02	50.0	-2.05								(E) 22.7A
CHAIN	21736r3.760E-01	17.0	0.08								
128 SB	13054 1.636E-02	50.0	0.08								
	13393 1.300E-04	10.0	0.08								

TABLE 4 CHAIN AND CUMULATIVE YIELDS FROM THERMAL FISSION OF 233U . (CONT.)

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	YIELDS & SD	COMPONENT	VALUE	EXT.	DF	MEAN	DEVIATION	INT.	EXT./DF	MEAN	DEVIATION
129 TE(M)	13054 2.118E-01	50.0	-0.15								
	343 2.360E-01	15.0	-0.03								
130 XE	13393 3.900E-03	10.0	0.23					0.20	0.05	3.554E+00	(I) 2.5A
131 I	13361 2.700E-00	50.0	-0.76								0.6
	305 2.840E+00	20.0	-0.35								
	343 2.890E+00	20.0	-0.13								
	2025r3.333E+00	6.6	0.58								
	601r3.627E+00	5.1	0.45								
XE	72 3.520E+00	7.0	-0.70								
	13377 3.550E+00	5.0	0.70								
CHAIN	21736r3.634E+00	7.7	-0.29								
	247 3.510E+00	5.0	-0.29								
132 TE	305 4.320E+00	7.0	-1.61					5.51	0.69	4.767E+00	(I) 2.5A
	13054 4.716E+00	50.0	-0.02								2.1
	2025r4.769E+00	6.5	0.01								
	343 5.250E+00	15.0	0.62								
I	601r5.055E+00	4.9	1.33								
XE	711 4.270E+00	10.0	-1.21								
	72 4.820E+00	10.0	0.11								
CHAIN	21736r4.762E+00	8.6	-0.01								
	247 4.860E+00	5.0	0.53								
133 I (G)	305 3.370E+00	9.0	0.51					1.96	0.24	5.941E+00	(I) 2.2A
XE	601r6.116E+00	6.0	-0.72								(E) 1.1
CS	15 5.200E+00	20.0	-0.63								
	70 5.600E+00	10.0	-0.30								
	72 5.770E+00	10.0	-0.35								
13322 5.850E+00	5.0	-0.23									
CHAIN	376 5.880E+00	5.0	0.61								
	376 6.110E+00	5.0	0.31								
134 XE	711 5.980E+00	10.0	-0.40					0.33	0.08	6.208E+00	(I) 2.7A
	13377 6.180E+00	10.0	-0.05								(E) 0.8
	13377 6.280E+00	5.0	0.31								
CHAIN	247 6.130E+00	5.0	-0.30								
135 I	269 4.850E+00	7.0	-1.84					5.34	1.07	5.341E+00	(I) 3.9
	13361 5.100E+00	10.0	-0.52								(E) 4.1A
XE	2025r5.545E+00	11.5	0.34								
	601r5.789E+00	11.7	0.70								
	70 6.000E+00	10.0	1.17								
	72 6.020E+00	10.0	1.20								
136 I (M)	343 1.820E+00	15.0	-0.70					0.49	0.49	7.039E+00	(I) 9.3A
XE	72 6.890E+00	10.0	0.70								(E) 6.5
CS	13054 1.925E-02	50.0	-0.76								
137 CS	13015 5.160E+00	20.0	-0.2					20.34	1.45	6.206E+00	(I) 2.2A
	305 5.390E+00	20.0	-0.35								
	15 5.800E+00	20.0	-0.13								
	378 6.130E+00	10.0	0.34								
	217 6.420E+00	10.0	0.4								
	2025r6.580E+00	4.0	0.58								
	72 6.580E+00	10.0	1.37								
13322 6.630E+00	5.0	0.45									
42 6.820E+00	20.0	-1.28									
CHAIN	21736r5.828E+00	5.5	1.32								
	376 6.580E+00	5.0	1.37								
	376 6.630E+00	5.0	2.22								
	247 6.930E+00	5.0	-0.56								
138 CHAIN	376 5.740E+00	5.0	0.31					0.31	0.31	5.850E+00	(I) 3.5A

TABLE 4 CHAIN AND CUMULATIVE YIELDS FROM THERMAL FISSION OF 233U . (CONT)

A EL. NO.	REF. NO.	EXPERIMENTAL YIELDS & SD	MEAN	R	CHI2/DF	CHI2 COMPONENT	EXTERNAL	TOTAL CHI2	INT. EXT./DF	WEIGHTED MEAN	STANDARD DEVIATION
=====											
-----	15	5.400E-01	20.0	1.91							
=====											
CHAIN 21736r2.381E-01 20.3											
	247	3.650E-01	5.0	2.09							
=====											
152 SM	13384r2.079E-01	11.4	0.46						3.89	0.97	1.975E-01 (I) 3.6A
	259	2.140E-01	10.0	0.83							(E) 3.5
	72	2.220E-01	10.0	1.17							
=====											
CHAIN 247 1.860E-01 5.0											
	343	8.450E-02	20.0	-1.91							
153 SM	13563r4.563E-02	20.0									1.300E-01 15.0
	74r9.602E-02	11.7									
=====											
EU 18 1.300E-01 15.0											
=====											
154 SM	13384r4.563E-02	11.4	-0.11								
	259	2.140E-01	10.0	0.83					0.20	0.07	4.619E-02 (I) 4.0A
	72	4.800E-02	10.0	0.41							(E) 1.0
=====											
CHAIN 247 4.580E-02 5.0											
	247	4.580E-02	5.0	-0.29							
=====											
156 EU	74r1.134E-02	11.9									1.134E-02 11.9
157 EU	74r7.085E-03	12.6									7.085E-03 12.6
159 GD	74r9.589E-04	12.4									9.589E-04 12.4
161 TB	74r1.194E-04	13.6									1.194E-04 13.6
=====											

TABLE 5 CHAIN AND CUMULATIVE YIELDS FROM THERMAL FISSION OF 235U .

A EL. NO.	REF. NO.	EXPERIMENTAL YIELDS & SD	MEAN	R	CHI2/DF	CHI2 COMPONENT	EXTERNAL	TOTAL CHI2	INT. EXT./DF	WEIGHTED MEAN	STANDARD DEVIATION
=====											
1 H FI	1186	1.600E-03	10.0	-1.28					3.79	1.89	1.711E-03 (E) 7.9
	2065r4.757E-03	40.2	1.60								10.8A
=====											
2 H FI	840	8.400E-04	20.0	0.00					0.00	0.00	8.400E-04 (I) 17.9A
	1195	8.400E-04	40.0	0.00							(E) 0.0
=====											
3 H	839r5.267E-03	30.2W	-2.49						21.07	1.50	9.314E-03 (E) 3.1
	839	7.500E-03	33.0	-0.74							3.8A
	824	8.000E-03	12.0	-1.44							
	821	8.500E-03	20.0	-0.49							
	862	9.520E-03	10.0	0.23							
=====											
H FI	840	1.040E-02	10.0	1.09							
	1196	1.060E-02	10.0	1.26							
	2043	1.060E-02	12.0	1.04							
	859	1.060E-02	15.0	0.82							
	1201	1.080E-02	10.0	1.43							
	831r1.121E-02	20.3	0.84								
	2055r1.359E-02	20.3	1.56								
	3052r6.8495E-03	6.2	-1.88								
	861	9.900E-03	10.0	0.62							
=====											
HE	830r3.398E-07	300.0									
=====											
4 HE	1191	1.570E-01	30.0	-0.28					9.89	0.90	1.699E-01 (I) 3.6A
	828	2.180E-01	30.0	0.74							(E) 3.4
=====											
HE FI	1195	1.300E-01	40.0	-0.77							
	2050	1.302E-01	40.0	-0.77							
	932	1.50E-01	10.0	-1.0							
	2043	1.693E-01	10.0	-0.53							
	1196	1.700E-01	10.0	-0.04							
	1196	1.700E-01	10.0	0.00							
	1201	1.700E-01	10.0	0.00							
	1194	1.930E-01	15.0	0.82							
	2056	2.560E-01	10.0	1.49							
	2058	2.60E-01	10.0	1							
=====											
6*HE FI	840	1.850E-03	18.2W	-2.46					7.94	1.99	2.668E-03 (I) 4.9
	831r2.260E-03	20.3	-0.93								6.9A
	1196	2.860E-03	10.0	0.76							
	2047r2.871E-03	6.2	1.72								
	1195	2.86E-03	40.0	0.42							
=====											
7 LI FI	1195	6.890E-05	40.0								6.890E-05 40.0
=====											
BE	21884	2.000E-10	20.0								
=====											
8*HE FI	1195	1.360E-04	40.0						2.77	1.38	7.292E-05 (I) 13.8
=====											
LI FI	1202	1.520E-04	15.0W	1.42							(E) 16.2A
	1203	2.020E-04	15.0W	0.93							
	1195	3.020E-05	40.0W	-1.25							
=====											
BE FI	1202	8.060E-05	15.0								
=====											
9*LI FI	2047r3.721E-05	7.0W	-0.34						5.76	1.44	4.071E-05 (I) 5.9
	1195	5.040E-05	40.0	0.51							(E) 7.0A
=====											
BE FI	2047r2.837E-05	50.1	-0.99								
	1195	4.870E-05	40.0	0.44							
=====											
B FI	2062r7.136E-05	10.6W	2.41								
=====											
10*BE	21884	3.000E-04	20.0W	-2.32					7.65	1.53	5.201E-04 (I) 4.0
=====											
BE FI	1195	5.380E-04	40.0	0.08							(E) 4.9A
	2062r5.419E-04	2	0.82								
	1202	5.710E-04	15.0	0.81							
	1203	6.220E-04	15.0	1.12							
=====											
B FI	2062r5.437E-04	6.2	0.92								
=====											
11 BE FI	1195	3.360E-05	40.0								
=====											
B FI	1195	4.200E-06	40.0								
	2062r5.029E-05	12.5									
=====											
12 BE FI	2047r1.189E-05	20.3	-1.28						1.65	1.65	1.261E-05 (I) 18.6
	1195	2.520E-05	40.0	1.28							(E) 23.9A
=====											
B FI	2062r2.464E-05	14.5									
	1195	2.860E-06	40.0								
	2047r3.738E-06	10.6									
=====											

TABLE 5
CHAIN AND CUMULATIVE YIELDS FROM THERMAL FISSION OF ^{235}U

[illegible]

TABLE 5 CHAIN AND CUMULATIVE YIELDS FROM THERMAL FISSION OF ^{235}U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE		INT. EXT./DF	MEAN	DEVIATION	DEVIATION	
SB	221	1.110E+00 15.0							
	905	4.090E-01 25.0							
	1361	6.000E-01 3.3							
	1319	6.000E-01 3.3							
	172	6.310E-01 5.0							
SB(G)	13461	4.000E-01 10.0							
TE(M)	13054	4.07E-01 5.0							
	341	1.950E-01 15.0							
	13461	3.370E-01 38.6							
	905	3.450E-01 10.0							
I	21917	6.900E-01 7.2	-0.40						
	21593	9.000E-01 25.0	0.87						
CHAIN	13319	6.100E-01 4.9W	-1.72						
	1098	8.040E-01 5.0W	2.17						
	21531	8.170E-01 5.8W	2.29						
130 IN(G)	22003	4.100E-02 15.0				4.08	4.08	1.778E+00 (I) 2.9A	2.9A
SN(G)	22003	9.400E-01 9.0							
SN(M)	22003	1.310E-01 13.0							
SB	13319	1.380E+00 11.6							
	13461	2.100E+00 19.1							
SB(G)	22003	1.120E+00 11.0							
	279	2.060E+00 25.0							
SB(M)	22003	3.000E-01 24.0							
XE	13393	5.000E-04 10.0							
CHAIN	13319	1.430E+00 12.6	-2.02						
	1098	1.810E+00 3.0	2.02						
131*IN	2028	1.600E-02 31.3				28.71	1.37	2.881E+00 (I) 1.0	1.1A
IN(G)	22003	3.100E-03 29.0							
IN(M)	22003	1.600E-02 44.0							
IN(N)	22003	7.600E-05 24.0							
SN	307	1.290E+00 16.0							
	22003	8.600E-01 10.0							
SB	905	1.750E+00 15.0							
	13461	1.750E+00 22.9							
	279	2.570E+00 8.0							
	22003	2.650E+00 14.0							
TE(M)	13955	4.150E-01 5.0	-1.96						
	905	4.260E-01 5.0	-2.48						
	341	4.510E-01 15.0	-1.70						
	2007	5.000E-01 10.0	-1.70						
	21662	5.000E-01 10.0	-1.70						
I	13955	1.700E+00 15.0W	-1.96						
	793	2.660E+00 5.0	-1.70						
	774	2.670E+00 7.0	-1.14						
	628	2.680E+00 5.0	-1.54						
	1151	2.710E+00 15.0	-0.42						
	13955	2.800E+00 10.0	-0.42						
	175	2.860E+00 15.0	-0.05						
	13478	2.860E+00 5.0	-0.15						
	341	2.870E+00 15.0	-0.03						
	757	2.930E+00 5.0	0.34						
	13465	3.020E+00 5.0	0.64						
	4573	3.15E+00 5.2	2.03						
XE	1116	2.910E+00 2.0	0.56						
	13386	2.920E+00 10.0	0.13						
	277	2.990E+00 5.0	0.74						
CHAIN	248	2.790E+00 3.0	-1.16						
	21531	2.900E+00 5.2	0.13						
	1098	2.920E+00 3.0	0.47						
	2173613	0.37E+00 2.5	2.24						

TABLE 5
CHAIN AND CUMULATIVE YIELDS FROM THERMAL FISSION OF ^{235}U

TABLE 5 CHAIN AND CUMULATIVE YIELDS FROM THERMAL FISSION OF ^{235}U .

A. EL. NO.	REP. NO.	EXPERIMENTAL YIELDS & SD	MEAN COMPONENT VALUE	R	CHI2/DF	CHI2 EXTERNAL	CHI2 INTERNAL	TOTAL CHI2	WEIGHTED MEAN	STANDARD DEVIATION

I (G) 22003 7.100E+00 11.0										

XE 340 7.460E+00 15.0 -0.25										
806 7.710E+00 3.0 -0.15										
1116 7.920E+00 2.0 1.39										
1386 8.030E+00 10.0 0.36										
1656 8.140E+00 15.0 1.19										
2077 8.220E+00 5.0 1.19										

CS 13457E7.893E+00 20.0 0.10										

CHAIN 21531 7.290E+00 5.0 -1.29										
1098 7.650E+00 3.0 -0.44										

I35 SB 22003 5.900E-01 31.0 1.77 0.22 6.563E+00 (I) 2.6A										

TE 22003 4.200E+00 22.0 (E) 1.2										

I (G) 13395 4.300E+00 15.0										
774 5.620E+00 3.0										
341 5.740E+00 16.0										
13461 6.310E+00 3.2										
628 6.310E+00 9.0										
13395 6.480E+00 10.0										
22003 6.860E+00 5.2										
1178 6.860E+00 7.0										

I (M) 2018 9.300E-01 10.8										

XE 341 6.040E+00 15.0 -0.59										
68 6.410E+00 10.0 -0.25										
628 6.710E+00 5.0 0.51										

CS 13385 6.410E+00 10.0 -0.25										
1275 6.570E+00 10.0 0.01										
13395 6.180E+00 10.0 0.89										

CHAIN 21531 6.180E+00 10.0 -0.65										
398 6.520E+00 10.0 -0.07										
1098 6.560E+00 5.0 -0.01										

I36 SB 22003 1.800E-02 27.0 1.91 0.32 6.279E+00 (I) 1.8A										

TE 21743 1.440E+00 6.9 (E) 1.0										
22003 1.930E+00 13.0										

I (G) 22003 1.710E+00 15.0										
687E3.904E+00 20.0										

I (M) 2092 1.500E+00 15.0										

XE 906 6.160E+00 15.0 -0.81										
13386 6.440E+00 10.0 -0.25										
28E6.440E+00 15.1 0.17										
277 6.600E+00 5.0 1.03										

CS 13054 2.239E-02 50.0										
13457E7.668E+00 *										

CHAIN 1098 6.220E+00 3.0 -0.40										
356 6.470E+00 5.0 0.63										

I37*TE 22003 4.600E-01 18.0 12.31 0.68 6.211E+00 (I) 0.9A										

I 22003 2.450E+00 9.0 (E) 0.8										

XE 2018 6.940E+00 12.8 0.82										
22003 7.700E+00 16.0 1.21										

CS 13054 2.127E+00 50.0W -0.30										
2025E6.091E+00 6.6 -0.50										
13385 6.110E+00 10.0 -0.18										
13478 6.120E+00 2.4 -0.67										
757 6.150E+00 4.0 -0.25										
356 6.110E+00 10.0 -0.13										
2025E6.091E+00 6.6 -0.50										

TABLE 5 CHAIN AND CUMULATIVE YIELDS FROM THERMAL FISSION OF 235U .

(cont)

A EL. NO.	REF.	EXPERIMENTAL YIELDS & SD	MEAN COMPONENT VALUE	CHI2/DF EXTERNAL	CHI2 TOTAL	CHI2/DF INTERNAL	EXT./DF MEAN	WEIGHTED STANDARD DEVIATION
150 ND	13386	6.400E-01	10.0	-0.16	4.53	0.27	6.505E-01	(I) 0.9A
	20251	6.494E-01	10.4	-0.02				(E) 0.5
	13384	6.533E-01	2.3	0.20				
	148	6.550E-01	3.0	0.24				
	55	6.550E-01	5.0	0.17				
	277	6.560E-01	5.0	0.17				
	1116	6.580E-01	2.5	0.49				
	19	7.000E-01	15.0	0.47				
	13428	7.080E-01	10.0	0.82				
	339	7.250E-01	15.0	0.69				
CHAIN	374	6.330E-01	3.0	-0.97				
	248	6.380E-01	3.0	-0.68				
	356	6.380E-01	4.0	-0.50				
	374	6.400E-01	3.0	-0.57				
	374	6.500E-01	3.0	-0.02				
	13352	6.580E-01	10.0	0.11				
	1212	7.080E-01	15.0	0.54				
151 PM	774	3.690E-01	9.0		11.36	1.26	4.181E-01	(I) 1.5
SM	13384	3.980E-01	10.0	-0.51				(E) 1.7A
	13386	4.500E-01	10.0	0.72				
	68	4.500E-01	5.0	1.48				
	277	4.610E-01	5.0	1.94				
CHAIN	21736	3.163E-01	16.1	-2.02				
	253	3.160E-01	10.0	-0.44				
	248	4.080E-01	3.0	-0.97				
	1098	4.170E-01	3.6	-0.08				
152 SM	13384	2.510E-01	1.0	-1.77				
	148	2.600E-01	15.0	0.59				
	13352	2.790E-01	10.0	0.95				
	13386	2.800E-01	10.0	0.99				
	277	2.870E-01	8.0	1.51				
CHAIN	248	2.120E-01	10.0	-1.92				
	1098	2.750E-01	4.7	1.76				
153 SM	278	1.290E-01	10.0	-1.81				
	361	1.440E-01	10.0	-0.51				
	13396	1.500E-01	10.0	-0.07				
	148	1.580E-01	15.0	0.30				
	73	1.610E-01	10.0	0.64				
EU	148	1.640E-01	4.0M	2.42				
CHAIN	1098	1.950E-01	15.0M	-2.27				
	21736	1.992E-01	16.2M	2.49				
	21531	1.430E-01	11.2	-0.52				
	356	1.480E-01	10.0	-0.22				
154 SM	13384	6.800E-02	10.0	-0.72				
	148	7.440E-02	3.0	1.04				
	13386	7.700E-02	10.0	0.56				
	338	8.570E-02	15.0	1.02				
CHAIN	1098	5.600E-02	16.1	-1.89				
	248	5.630E-02	10.0M	-2.44				
	356	2.400E-02	3.0M	0.31				
155 SM	13422	3.022E-02	20.5	-0.14				
	341	3.180E-02	15.0	0.20				
EU	13395	1.900E-02	15.0M	-2.41				
	148	3.240E-02	3.0M	0.31				
156 SM	341	1.230E-02	15.0	-0.60				
	13424	1.348E-02	1.7	0.97				
	13396	1.400E-02	10.0	0.43				
EU	277	1.150E-02	18.0	-1.28				
	167	1.250E-02	10.0	-0.92				
	175	1.380E-02	15.0	0.20				
	73	1.390E-02	10.0	0.37				
157 EU	167	6.000E-03	12.0	-1.03				

TABLE 5 CHAIN AND CUMULATIVE YIELDS FROM THERMAL FISSION OF 235U .

(cont)

A EL. NO.	REF.	EXPERIMENTAL YIELDS & SD	MEAN COMPONENT VALUE	CHI2/DF EXTERNAL	CHI2 TOTAL	CHI2/DF INTERNAL	EXT./DF MEAN	WEIGHTED STANDARD DEVIATION
158 EU	13423	1.639E-03	10.1W	-0.27				
	341	2.050E-03	50.0	0.09				
	167	3.100E-03	20.0W	1.75				
GD	13352	8.400E-03	10.0W	2.48				
159 EU	167	1.100E-03	28.0	0.13				
GD	278	1.040E-03	10.0	-0.27				
	180	1.130E-03	12.0	0.57				
161 TB	786	1.310E-04	20.0	1.94				
	278	7.170E-05	10.0	-1.72				
	180	8.210E-05	11.0	0.14				
	73	8.600E-05	10.0	1.00				
166 DY	263	6.560E-08	50.0					
172 ER	755	8.700E-07	40.0					
175 TB	755	6.000E-07	40.0					
177 LU	755	3.600E-07	40.0					

TABLE 6 CHAIN AND CUMULATIVE YIELDS FROM THERMAL FISSION OF 237NP.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
85	CHAIN	21651 1.040E+00	7.7				1.040E+00	7.7
87	CHAIN	21651 1.880E+00	8.5				1.880E+00	8.5
88	CHAIN	21651 2.240E+00	7.6				2.240E+00	7.6
91	CHAIN	21651 3.670E+00	7.1				3.670E+00	7.1
92	CHAIN	21651 4.180E+00	5.7				4.180E+00	5.7
93	CHAIN	21651 4.800E+00	9.4				4.800E+00	9.4
94	CHAIN	21651 5.020E+00	11.0				5.020E+00	11.0
95	CHAIN	21651 5.720E+00	7.7				5.720E+00	7.7
97	CHAIN	21651 5.880E+00	4.9				5.880E+00	4.9
99	CHAIN	21651 6.650E+00	5.6				6.650E+00	5.6
101	CHAIN	21651 6.800E+00	9.1				6.800E+00	9.1
103	CHAIN	21651 5.870E+00	7.3				5.870E+00	7.3
104	CHAIN	21651 3.490E+00	7.5				3.490E+00	7.5
105	CHAIN	21651 2.600E+00	9.6				2.600E+00	9.6
115	CHAIN	21651 1.310E-02	9.2				1.310E-02	9.2
127	CHAIN	21651 1.700E-01	23.5				1.700E-01	23.5
129	CHAIN	21651 9.900E-01	13.1				9.900E-01	13.1
131	TE	2027t6.209E+00	20.6	2.07		4.26	2.07 4.26 3.634E+00 (I)	7.5 >2
	CHAIN	21651 3.510E+00	8.0	-2.07				(E) 15.5A
132	TE	2027t4.471E+00	20.6	0.17		0.03	0.03 4.321E+00 (I)	7.4A
	CHAIN	21651 4.300E+00	7.9	-0.17				(E) 1.3
133	TE	2027t3.987E+00	20.6					5.5
	CHAIN	21651 6.550E+00	5.5					6.550E+00
134	TE	2027t4.386E+00	20.6					8.3
	CHAIN	21651 6.620E+00	8.3					6.620E+00
135	CHAIN	21651 7.770E+00	4.5					7.770E+00
138	CHAIN	21651 6.230E+00	6.1					6.230E+00
140	CHAIN	21651 6.110E+00	6.5					6.110E+00
141	CHAIN	21651 6.140E+00	7.7					6.140E+00
142	CHAIN	21651 5.030E+00	8.0					5.030E+00
143	CHAIN	21651 5.100E+00	7.2					5.100E+00
146	CHAIN	21651 2.870E+00	12.5					2.870E+00
147	CHAIN	21651 2.570E+00	8.2					2.570E+00
149	CHAIN	21651 1.700E+00	14.7					1.700E+00
151	CHAIN	21651 8.100E-01	14.8					8.100E-01
156	CHAIN	21651 1.200E-01	33.3					1.200E-01

TABLE 7 CHAIN AND CUMULATIVE YIELDS FROM THERMAL FISSION OF 238NP.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
85	CHAIN	2110 9.110E-01	5.0				9.110E-01	5.0
86	CHAIN	2110 1.120E+00	5.0				1.120E+00	5.0
87	CHAIN	2110 1.380E+00	5.0				1.380E+00	5.0
88	CHAIN	2110 1.890E+00	5.0				1.890E+00	5.0
89	CHAIN	2110 2.270E+00	5.0				2.270E+00	5.0
90	CHAIN	2110 3.030E+00	5.0				3.030E+00	5.0
91	CHAIN	2110 3.460E+00	5.0				3.460E+00	5.0
92	CHAIN	2110 4.090E+00	5.0				4.090E+00	5.0
93	CHAIN	2110 4.640E+00	5.0				4.640E+00	5.0
94	CHAIN	2110 5.090E+00	5.0				5.090E+00	5.0
95	CHAIN	2110 5.300E+00	5.0				5.300E+00	5.0
96	CHAIN	2110 5.450E+00	5.0				5.450E+00	5.0
97	CHAIN	2110 5.800E+00	5.0				5.800E+00	5.0
98	CHAIN	2110 5.760E+00	5.0				5.760E+00	5.0
99	CHAIN	2110 6.350E+00	5.0				6.350E+00	5.0
100	CHAIN	2110 6.520E+00	5.0				6.520E+00	5.0
101	CHAIN	2110 6.530E+00	5.0				6.530E+00	5.0
102	CHAIN	2110 6.540E+00	5.0				6.540E+00	5.0
103	CHAIN	2110 6.400E+00	5.0				6.400E+00	5.0
104	CHAIN	2110 5.60E+00	5.0					
105	CHAIN	2110 4.450E+00	5.0				4.450E+00	5.0
106	CHAIN	2110 3.260E+00	5.0				3.260E+00	5.0
108	CHAIN	2110 1.160E+00	10.0				1.160E+00	10.0
109	CHAIN	2110 6.200E-01	10.0				6.200E-01	10.0
110	CHAIN	2110 3.100E-01	10.0				3.100E-01	10.0

TABLE 8 CHAIN AND CUMULATIVE YIELDS FROM THERMAL FISSION OF 238PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION	
87 KR	22087 6.00E+00	16.7				6.00E+00	16.7	
89 KR	22087 1.230E+00	6.5				1.480E+00	6.8	
RB	22087 1.480E+00	6.8						
91 SR	22087 2.550E+00	5.0				2.550E+00	5.0	
92 SR	22087 3.220E+00	5.0				3.220E+00	5.0	
93 SR	22087 3.170E+00	7.9				3.600E+00	8.3	
CHAIN 22087	3.600E+00	8.3						
94 SR	22087 3.870E+00	5.0				4.750E+00	5.0	
Y	22087 4.750E+00	5.0						
95 Y	22087 5.570E+00	5.0	0.18			0.03	0.03	5.535E+00 (I) 3.5A
ZR	22087 5.500E+00	5.0	-0.18					(E) 0.6
97 ZR	22087 5.730E+00	5.0				5.730E+00	5.0	
99 MO	22087 6.110E+00	5.0				6.110E+00	5.0	
101 MO	22087 6.840E+00	5.0				6.840E+00	5.0	
103 RU	22087 7.910E+00	5.0				7.910E+00	5.0	
104 TC	22087 6.870E+00	5.0				6.870E+00	5.0	
105 RU	22087 5.800E+00	5.0				5.800E+00	5.0	
109 RH(G)	22087 1.280E+00	7.8				1.400E+00	7.9	
CHAIN 22087	1.400E+00	7.9						
127 SR	22087 6.300E+00	12.7				6.300E+00	12.7	
128 SN	22087 6.100E-01	16.4				6.100E-01	16.4	
129 SB	22087 1.920E+00	7.8				1.920E+00	7.8	
130 SN(G)	22087 5.000E+00	14.0				5.000E+00	14.0	
131 SB	22087 2.660E+00	5.0				5.200E+00	5.0	
I	22087 5.200E+00	5.0						
132 TE	22087 7.470E+00	5.0				7.470E+00	5.0	
133 SB	22087 1.350E-01	37.0				7.620E+00	5.0	
TE(G)	22087 2.900E+00	6.9						
I	22087 7.620E+00	5.0						
134 TE	22087 3.080E+00	5.0				7.780E+00	5.0	
CHAIN 22087	7.780E+00	5.0						
135 I	22087 5.530E+00	5.0				7.560E+00	5.0	
CHAIN 22087	7.560E+00	5.0						
137 XE	22087 5.480E+00	5.5				5.480E+00	5.5	
138 XE	22087 4.080E+00	5.0				5.460E+00	5.5	
CS(G)	22087 5.460E+00	5.5						
139 XE	22087 1.890E+00	10.6				5.870E+00	5.1	
CS	22087 5.360E+00	5.6						
BA	22087 5.870E+00	5.1						
140 BA	22087 5.290E+00	5.0				5.290E+00	5.0	
141 BA	22087 5.590E+00	7.2				5.550E+00	5.0	
CS	22087 5.550E+00	5.0						
142 BA	22087 4.790E+00	5.0				5.270E+00	5.0	
LA	22087 5.270E+00	5.0						

TABLE 8 CHAIN AND CUMULATIVE YIELDS FROM THERMAL FISSION OF 238PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION	
143 CE	22087 3.940E+00	5.0				3.940E+00	5.0	
144 LA	22087 2.390E+00	12.6						
145 CE	22087 2.730E+00	5.0				2.730E+00	5.0	
147 ND	22087 1.610E+00	9.3				1.610E+00	9.3	
149 ND	22087 1.090E+00	18.3				1.090E+00	18.3	

TABLE 9 CHAIN AND CUMULATIVE YIELDS FROM THERMAL FISSION OF 239PU. (CONT)

A EL. NO.	REF. NO.	EXPERIMENTAL YIELDS & SD	MEAN R	CHI2/DF	CHI2	TOTAL CHI2	INT. EXT./DF	WEIGHTED STANDARD DEVIATION
111 AG	201*2	758E-01	6.1	-2.08	6.63	0.95	3.077E-01	(I) 2.3A (E) 2.2
	261	2.790E-01	14.0	-0.75				
	342	2.810E-01	15.0	-0.64				
	2021	3.100E-01	5.0	0.17				
	2025	3.107E-01	6.2	0.17				
	2021	3.200E-01	5.0	0.86				
CHAIN	1021*3	172E-01	6.1	0.53				
	1028*3	298E-01	6.1	1.18				
112 PD	342	1.040E-01	15.0		8.81	2.94	1.286E-01	(I) 3.3 >2 (E) 5.7A
	2018	4.53E-02	13.1					
	261	9.300E-02	10.0					
AG	2021	1.200E-01	5.0	-2.05				
	2021	9.600E-01	5.2M	2.48				
CD	1045	1.260E-01	5.0	-0.56				
CHAIN	1021*3	134E-01	20.9	-0.65				
113 AG	2021	1.000E-01	4.0M	1.95	6.43	3.21	8.119E-02	(I) 2.7 >2 (E) 4.9A
	2021	7.300E-02	5.5M	-1.38				
CD	1045	7.250E-02	5.0M	-1.99				
114 CD	1045	5.400E-02	5.0					
115 CD(G)	2021	3.300E-02	12.1	3.383E-02	-0.25	1.82		
	261	3.300E-02	6.0	-1.70	6.20	1.24	3.646E-02	(I) 4.7 (E) 5.3A
	342	4.680E-02	15.0	1.97				
CD(M)	2021	2.200E-01	5.0M	0.25	6.34E-03	-1.35	0.85	
	201*2	6.08E-03	9.1	-0.25				
	261	3.000E-03	20.0	0.67				
	342	3.100E-03	15.0	1.17				
116 CD	1045	4.580E-02	5.0					
	1045	4.580E-02	5.0					
117 CD(G)	891	7.180E-02	20.0					
SN	1045	4.580E-02	5.0					
118 SN	1045	4.580E-02	7.0					
119 SN	1045	4.860E-02	7.0					
120 SN	1045	4.290E-02	14.0					
121 SN(G)	2021	3.400E-02	11.8					
	342	4.260E-02	15.0					
SN(M)	1045	1.050E-02	14.0					
122 SN	1045	6.960E-02	5.0					
124 SN	1045	1.280E-01	5.0					
125 SN(G)	342	7.000E-02	15.0					
	2021	7.700E-02	19.5					
CHAIN	249	1.160E-01	12.0					
126 SN	1045	3.030E-01	15.0					
127 SN	1141	4.090E-01	20.5	-0.62	5.59	1.12	4.587E-01	(I) 4.9 (E) 5.2A
SB	342	3.840E-01	20.0	-1.02				
	2021	4.200E-01	19.1	-0.50				
	1261	5.500E-01	10.0	1.82				
	2025	5.928E-01	21.1	1.09				
128 SN	1141	5.400E-01	12.9					
SB(M)	1141	6.200E-01	6.1					
XE	13393	2.000E-04	10.0					
129 SB	1141	1.380E+00	5.0	-0.51	0.26	0.26	1.388E+00	(I) 4.9A (E) 2.5
	891	1.540E+00	20.0	0.51				
130 SB(M)	1141	8.560E-01	5.1					
XE	13393	5.200E-03	10.0					
131 SB	20878	1.060E+00	36.8		19.86	1.24	3.710E+00	(I) 1.6 (E) 3.7A

TABLE 9 CHAIN AND CUMULATIVE YIELDS FROM THERMAL FISSION OF 239PU. (CONT)

A EL. NO.	REF. NO.	EXPERIMENTAL YIELDS & SD	MEAN R	CHI2/DF	CHI2	TOTAL CHI2	INT. EXT./DF	WEIGHTED STANDARD DEVIATION
111 AG	201*2	758E-01	6.1	-2.08	6.63	0.95	3.077E-01	(I) 2.3A (E) 2.2
	261	2.790E-01	14.0	-0.75				
	342	2.810E-01	15.0	-0.64				
	2021	3.100E-01	5.0	0.17				
	2025	3.107E-01	6.2	0.17				
	2021	3.200E-01	5.0	0.86				
CHAIN	1021*3	172E-01	6.1	0.53				
	1028*3	298E-01	6.1	1.18				
112 PD	342	1.040E-01	15.0		8.81	2.94	1.286E-01	(I) 3.3 >2 (E) 5.7A
	2018	4.53E-02	13.1					
	261	9.300E-02	10.0					
AG	2021	1.200E-01	5.0	-2.05				
	2021	9.600E-01	5.2M	2.48				
CD	1045	1.260E-01	5.0	-0.56				
CHAIN	1021*3	134E-01	20.9	-0.65				
113 AG	2021	1.000E-01	4.0M	1.95	6.43	3.21	8.119E-02	(I) 2.7 >2 (E) 4.9A
	2021	7.300E-02	5.5M	-1.38				
CD	1045	7.250E-02	5.0M	-1.99				
114 CD	1045	5.400E-02	5.0					
115 CD(G)	2021	3.300E-02	12.1	3.383E-02	-0.25	1.82		
	261	3.300E-02	6.0	-1.70	6.20	1.24	3.646E-02	(I) 4.7 (E) 5.3A
	342	4.680E-02	15.0	1.97				
CD(M)	2021	2.200E-01	5.0M	0.25	6.34E-03	-1.35	0.85	
	201*2	6.08E-03	9.1	-0.25				
	261	3.000E-03	20.0	0.67				
	342	3.100E-03	15.0	1.17				
116 CD	1045	4.580E-02	5.0					
	1045	4.580E-02	5.0					
117 CD(G)	891	7.180E-02	20.0					
SN	1045	4.580E-02	5.0					
118 SN	1045	4.580E-02	7.0					
119 SN	1045	4.860E-02	7.0					
120 SN	1045	4.290E-02	14.0					
121 SN(G)	2021	3.400E-02	11.8					
	342	4.260E-02	15.0					
SN(M)	1045	1.050E-02	14.0					
122 SN	1045	6.960E-02	5.0					
124 SN	1045	1.280E-01	5.0					
125 SN(G)	342	7.000E-02	15.0					
	2021	7.700E-02	19.5					
CHAIN	249	1.160E-01	12.0					
126 SN	1045	3.030E-01	15.0					
127 SN	1141	4.090E-01	20.5	-0.62	5.59	1.12	4.587E-01	(I) 4.9 (E) 5.2A
SB	342	3.840E-01	20.0	-1.02				
	2021	4.200E-01	19.1	-0.50				
	1261	5.500E-01	10.0	1.82				
	2025	5.928E-01	21.1	1.09				
128 SN	1141	5.400E-01	12.9					
SB(M)	1141	6.200E-01	6.1					
XE	13393	2.000E-04	10.0					
129 SB	1141	1.380E+00	5.0	-0.51	0.26	0.26	1.388E+00	(I) 4.9A (E) 2.5
	891	1.540E+00	20.0	0.51				
130 SB(M)	1141	8.560E-01	5.1					
XE	13393	5.200E-03	10.0					
131 SB	20878	1.060E+00	36.8		19.86	1.24	3.710E+00	(I) 1.6 (E) 3.7A

TABLE 9 CHAIN AND CUMULATIVE YIELDS FROM THERMAL FISSION OF 239PU.

(CONT.)

A EL. NO.	REF. NO.	EXPERIMENTAL YIELDS & SD	MEAN	R	CHI2/DF	CHI2	EXTERNAL COMPONENT	INTERNAL COMPONENT	TOTAL CHI2	WEIGHTED MEAN	STANDARD DEVIATION
135 SB	20878	7.000E-02	42.9		1.16	0.15	7.320E+00	(I)	2.5A		
I	13395	1.300E+00	15.0							(E)	1.0
	270	5.270E+00	10.0								
	342	5.720E+00	15.0								
	1141	6.430E+00	5.0								
XE	2021	7.100E+00	10.0	-0.32							
	69	7.270E+00	10.0	-0.07							
	2025	7.390E+00	6.9	0.15							
	67	7.450E+00	10.0	0.18							
	1141	7.600E+00	5.0	0.84							
CS	20	6.950E+00	10.0	-0.55							
	233	7.050E+00	10.0	-0.40							
	13429	7.251E+00	14.6	-0.07							
CHAIN	177	7.250E+00	5.0	-0.23							
136 I (G)	342	1.970E+00	15.0		8.23	1.65	6.770E+00	(I)	2.3		
I (M)	2015	1.300E+00	15.4							(E)	2.9A
XE	13392	4.700E+00	10.6W	-2.36							
	107	6.580E+00	10.0	-0.24							
	710	6.620E+00	10.0	-0.23							
	179	6.680E+00	11.0	-0.13							
	1153	7.360E+00	3.0W	1.56							
CHAIN	177	6.620E+00	5.0	-0.57							
137 XE	946	5.970E+00	10.0		8.43	0.84	6.700E+00	(I)	1.1A		
	1061	6.150E+00	5.0							(E)	1.0
CS	261	5.400E+00	10.0	-2.43							
	20	6.500E+00	10.0	-0.31							
	2025	6.505E+00	5.7	-0.53							
	13256	6.720E+00	2.1	0.17							
	13256	6.819E+00	2.1	0.99							
	13429	6.864E+00	2.9	0.87							
CHAIN	177	6.480E+00	5.0	-0.69							
	13256	6.720E+00	5.0	-0.06							
	249	6.740E+00	5.0	0.12							
138 I	2015	1.100E+00	18.2		3.75	0.94	6.094E+00	(I)	2.4A		
XE	21855	5.320E+00	10.0							(E)	2.3
	946	5.000E+00	10.0								
	1141	5.260E+00	8.9								
	1061	5.420E+00	7.0								
CS	181	5.720E+00	20.0								
	1141	5.720E+00	20.0								
BA	13258	5.150E+00	15.0	-1.24							
	1153	6.140E+00	3.0	0.41							
	20	6.260E+00	10.0	0.27							
CHAIN	249	5.400E+00	10.0	-1.33							
	177	6.310E+00	5.0	0.77							
139 XE	1061	3.070E+00	5.0		6.91	1.15	5.976E+00	(I)	1.3		
CS	1141	5.500E+00	22.7							(E)	1.4A
BA	2021	5.550E+00	16.2	-0.48							
	602	5.607E+00	3.2	-2.28							
	342	5.610E+00	15.0	-0.44							
	32	5.960E+00	10.0	-0.03							
	13474	6.070E+00	1.5	2.15							
	1143	7.500E+00	18.7	1.09							
140 BA	760	3.090E+00	40.0	-1.81							
	2021	4.980E+00	20.1	-0.34							
	2021	5.040E+00	19.8	-0.28							
	793	5.240E+00	1.0	-0.23							
	1141	5.250E+00	5.0	-0.27							
	13433	5.310E+00	2.8	-0.08							
	2021	5.360E+00	2.6	0.31							
	1152	5.430E+00	15.0	0.13							

TABLE 9 CHAIN AND CUMULATIVE YIELDS FROM THERMAL FISSION OF 239PU.

(CONT.)

A EL. NO.	REF. NO.	EXPERIMENTAL YIELDS & SD	MEAN	R	CHI2/DF	CHI2	EXTERNAL COMPONENT	INTERNAL COMPONENT	TOTAL CHI2	WEIGHTED MEAN	STANDARD DEVIATION
141 XE	1061	4.880E-01	6.0		2.44	0.22	5.203E+00	(I)	1.4A		
LA	1141	5.350E+00	5.0	0.11							
CE	1153	5.080E+00	3.0	-1.70							
	20	5.520E+00	5.0	0.74							
CHAIN	1021	5.240E+00	2.3	-0.74							
	249	5.610E+00	5.0	1.05							
	177	5.880E+00	5.0	1.94							
142 XE	1061	1.380E-01	7.0		9.87	0.90	4.967E+00	(I)	1.1A		
LA	1141	4.670E+00	5.9	-1.12							
	602	5.018E+00	5.8	0.17							
	2021	5.390E+00	3.5	2.31							
CE	13429	4.665E+00	10.6	-0.61							
	2025	4.789E+00	6.2	-0.61							
	13256	4.894E+00	2.0	-0.88							
	13256	4.930E+00	2.0	-0.44							
	1153	5.080E+00	3.0	0.79							
	20	6.660E+00	20.0	1.27							
CHAIN	375	4.930E+00	5.0	-0.15							
	177	4.970E+00	5.0	0.01							
	249	5.040E+00	5.0	0.30							
143 BA	2015	3.400E+00	23.5		5.35	0.49	4.485E+00	(I)	1.1A		
CE	760	2.960E+00	12.0							(E)	0.8
	595	4.000E+00	10.0								
	602	4.097E+00	8.4								
	2021	4.190E+00	7.2								
	2021	4.200E+00	3.6								
	1141	4.300E+00	15.0								
	2025	4.339E+00	6.1								
	1152	4.710E+00	15.0								
	342	5.300E+00	15.0								
	13395	5.400E+00	15.0								
PR	593	4.240E+00	10.0	-0.58							
	13395	5.400E+00	15.0	1.13							
ND	1153	4.430E+00	3.0	-0.45							
	2025	4.445E+00	5.1	-0.18							
	13256	4.453E+00	2.1	-0.41							
	13256	4.453E+00	2.0	0.32							
	13256	4.510E+00	2.0	0.33							
	392	5.480E+00	15.0	1.21							
	20	6.100E+00	20.0	1.32							
CHAIN	249	4.480E+00	5.0	-0.02							
	1153	4.610E+00	5.0	0.11							
	177	4.560E+00	5.0	0.34							
144 LA	2015	4.000E+00	15.0		10.57	0.50	3.756E+00	(I)	0.8A		
CE	337	3.176E+00	20.3	-0.90							
	2021	3.180E+00	6.2	-1.52							
	2025	3.545E+00	4.0	-1.52							
	13429	3.576E+00	4.2	-1.25							
	602	3.740E+00	4.0	-0.11							
	1153	3.770E+00	3.0	0.13							
	2021	3.800E+00	1.8	0.69							

TABLE 9 CHAIN AND CUMULATIVE YIELDS FROM THERMAL FISSION OF 239PU.

(CONT.)

A EL.	REF.	EXPERIMENTAL	NO.	YIELDS & SD	MEAN	R	CH12/DF	CH12	CH12	TOTAL	CH12	INT.	EXT./DF	MEAN	STANDARD	DEVIATION
NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.
145	PR	595	3.540E+00	10.0	1.42		4.69	0.52	3.040E+00	(I)	1.0A					
ND		13256	3.000E+00	2.1	-0.73											
ND		1153	3.020E+00	3.0	-0.23											
ND		2025+3.030E+00	5.1	-0.07												
ND		13256	3.040E+00	2.6	0.00											
ND		13429+3.051E+00	1.6	0.29												
ND		20	4.200E+00	20.0	1.38											
CHAIN		249	3.030E+00	5.0	-0.07											
CHAIN		375	3.040E+00	5.0	0.00											
CHAIN		177	3.120E+00	5.0	0.52											
146	CE	1141	2.260E+00	15.5			2.86	0.36	2.498E+00	(I)	0.9A					
PR		891	1.670E+00	30.0												
ND		1153	2.470E+00	3.0	-0.40											
ND		13256	2.483E+00	2.1	-0.34											
ND		13256	2.490E+00	2.0	-0.19											
ND		2025+2.432E+00	5.1	-0.05												
ND		13429+2.448E+00	1.6	0.48												
ND		20	3.530E+00	20.0	1.46											
CHAIN		249	2.490E+00	5.0	-0.07											
CHAIN		375	2.490E+00	5.0	0.00											
CHAIN		177	2.570E+00	5.0	0.57											
147	ND	2025+1.810E+00	10.6	-1.26			9.12	0.61	2.047E+00	(I)	1.7A					
ND		261	1.920E+00	10.0	-0.68											
ND		337+1.982E+00	20.3	-0.16												
ND		1141	2.050E+00	5.0	0.03											
ND		2021	2.050E+00	5.0	0.03											
ND		593	2.130E+00	10.0	0.39											
ND		1152	2.180E+00	15.0	0.41											
PM		69	2.070E+00	10.0	0.11											
PM		593	2.140E+00	10.0	0.44											
PM		20	2.580E+00	10.0	2.08											
SM		232	1.920E+00	27.0	-0.25											
SM		13429	1.975E+00	5.0	-0.79											
SM		1153	1.990E+00	6.0	-0.50											
CHAIN		249	1.930E+00	5.0	-0.62											
CHAIN		375	1.930E+00	5.0	0.00											
148	ND	1153	1.650E+00	3.0	-0.73		3.48	0.44	1.684E+00	(I)	0.9A					
ND		13256	1.670E+00	1.8	-0.55											
ND		13256	1.671E+00	2.0	-0.43											
ND		13429+1.698E+00	1.6	0.60												
ND		228	1.710E+00	10.0	0.63											
ND		20	2.300E+00	20.0	1.34											
CHAIN		375	1.670E+00	5.0	-0.17											
CHAIN		249	1.700E+00	5.0	0.19											
CHAIN		177	1.710E+00	5.0	0.30											
149	ND	595	1.140E+00	10.0	-1.15		4.48	0.64	1.267E+00	(I)	2.2A					
PM		337+1.253E+00	22.3	-0.05												
PM		595	1.300E+00	5.0	0.56											
SM		1153	1.310E+00	5.0	-0.86											
SM		20	1.680E+00	20.0	1.23											
CHAIN		249	1.240E+00	5.0	-0.48											
CHAIN		177	1.300E+00	5.0	0.56											

TABLE 9 CHAIN AND CUMULATIVE YIELDS FROM THERMAL FISSION OF 239PU.

(CONT.)

A EL.	REF.	EXPERIMENTAL	NO.	YIELDS & SD	MEAN	R	CH12/DF	CH12	CH12	TOTAL	CH12	INT.	EXT./DF	MEAN	STANDARD	DEVIATION
NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.
150	ND	20	1.350E+00	20.0	1.38		3.61	0.45	9.778E-01	(E)	1.2A					
ND		13256	9.450E-01	5.0	-0.72											
ND		13256	9.600E-01	5.0	-0.38											
ND		1153	9.660E-01	5.0	-0.25											
ND		13429+9.810E-01	1.6	0.32												
ND		2025+9.933E-01	5.1	0.32												
CHAIN		177	1.020E+00	5.0	0.85											
CHAIN		375	9.600E-01	5.0	-0.38											
CHAIN		249	9.650E-01	5.0	-0.27											
151	PM	1141	7.90E-01	63.0	-0.18		9.16	1.15	7.794E-01	(I)	2.1					
PM		595	7.90E-01	63.0	-0.18											
PM		13429	7.715E-01	5.0	-0.23											
SM		20	1.510E+00	20.0	2.42											
SM		1153	7.290E-01	5.0	-1.55											
SM		232	7.960E-01	10.0	0.30											
SM		232	7.960E-01	10.0	0.21											
CHAIN		177	8.020E-01	5.0	0.62											
CHAIN		249	8.110E-01	5.0	0.85											
152	ND	13429	6.236E-01	5.0	0.00		0.00	0.4	3.64	0.91	6.093E-01	(I)	2.7A			
PM(G)		232	5.220E-01	10.0	5.466E-01	-1.44	2.06+2	0.34								
PM(M)		20	7.500E-01	20.0	1.44											
PM(M)		1153	9.400E-02	15.0	9.400E-02	0.00	0.03									
CHAIN		177	6.60E-01	5.0	6.057E-01	-1.07	0.58	0.04								
153	SM	595	1.700E-01	40.0												
SM		337+3.484E-01	20.6													
SM		342	4.050E-01	20.0												
154	ND	13429	2.782E-01	2.0			1.33	1.33	2.806E-01	(I)	3.5					
SM		232	2.020E-01	20.0												
SM		1153	2.500E-01	5.0												
SM		20	3.600E-01	20.0												
CHAIN		249	2.700E-01	5.0	-1.15											
CHAIN		177	2.930E-01	5.0	1.15											
155	SM	13422+1.633E-01	31.4	0.01			4.03	2.01	1.628E-01	(I)	10.3	>2				
SM		342	2.180E-01	15.0	1.96											
EU		13395	1.400E-01	15.0	-1.79											
156	SM	595	9.600E-02	10.0	-2.10		12.52	2.50	1.147E-01	(I)	2.5	>2				
EU		593	1.240E-01	7.0	1.18											
EU		342	1.250E-01	15.0	0.56											
EU		337+9.600E-02	20.7	-2.42												
EU		337+9.600E-02	20.7	-0.75												
CHAIN		1021+1.194E-01	2.8W	1.58												
157	EU	595	7.600E-02	10.0												
159	GD	337+2.058E-02	21.0	0.21			0.04	0.04	2.140E-02	(E)	1.9					
GD		595	2.160E-02	10.0	-0.21											
161	TB	337+4.108E-03	21.7	-1.02			1.05	1.05	4.895E-03	(I)	9.1					
TB		595	5.160E-03	10.0	1.02											
66	DI	337+7.137E-05	53.9													
DI		337+7.137E-05	53.9													

TABLE 10 CHAIN AND CUMULATIVE YIELDS FROM THERMAL FISSION OF 241PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	INT.	EXT./DF	MEAN	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	EXTERNAL	INT.	EXT./DF	MEAN	EXT./DF	MEAN	DEVIATION	DEVIATION
3 H PI	1201	1.410E-02	10.0										1.410E-02	0.0
4 HE PI	1201	1.860E-01	10.0	-1.37				1.87	1.87	2.015E-01	(I)	7.3		
	2055	2.277E-01	10.6	1.37							(E)	10.0A		
77 AS	1014	9.65E-04	13.5										4.965E-04	13.5
83 BR	1014	9.44E-01	7.6	-0.31				0.10	0.10	1.982E-01	(I)	4.2A		
CHAIN	250	2.000E-01	5.0	0.31							(E)	1.3		
84 CHAIN	250	3.530E-01	5.0							3.530E-01		5.0		
85 KR (G)	582	9.505E-02	6.8					0.02	0.02	3.890E-01	(I)	3.5A		
RB	585	3.910E-01	5.0	0.15							(E)	0.5		
CHAIN	250	3.870E-01	5.0	-0.15										
86 CHAIN	250	6.010E-01	5.0							6.010E-01		5.0		
87 KR	1060	7.140E-01	5.0	-0.52				0.28	0.28	7.270E-01	(I)	3.5A		
CHAIN	250	7.410E-01	5.0	0.52							(E)	1.9		
88 KR	1060	1.000E+00	8.0	0.39				0.31	0.16	9.716E-01	(I)	3.6A		
SR	2025	9.864E-01	6.8	0.26							(E)	1.4		
CHAIN	250	9.540E-01	5.0	-0.54										
89 KR	1060	1.110E+00	6.0	-1.40				2.07	1.03	1.186E+00	(I)	3.2		
SR	770	1.210E+00	5.0	0.51							(E)	3.3A		
	2025	1.243E+00	5.9	0.91										
90 KR	1060	1.190E+00	5.0					0.65	0.16	1.498E+00	(I)	2.5A		
SR	770	1.460E+00	5.0	-0.60							(E)	1.0		
	2103	1.480E+00	5.0	-0.28										
	2025	1.528E+00	6.8	0.32										
	2025	1.529E+00	8.4	0.26										
CHAIN	250	1.530E+00	5.0	0.49										
91*KR (G)	594	1.690E+00	10.0	-0.02				13.55	2.71	1.694E+00	(I)	2.5 >2		
SR	2025	1.798E+00	5.8	1.10							(E)	4.1A		
	10894	1.900E+00	5.3	2.32										
Y	10694	1.040E+00	10.0W	-2.13										
ZR	2103	1.820E+00	5.0	1.61							(E)	1.7		
CHAIN	250	1.820E+00	5.0	1.61										
92 KR	1060	5.750E-01	12.0					0.52	0.26	2.224E+00	(I)	3.4A		
Y	10894	2.040E+00	13.2	-0.71										
ZR	2103	2.250E+00	5.0	0.31							(E)			
CHAIN	250	2.230E+00	5.0	0.07										
93 KR	1060	1.940E-01	7.0					0.17	0.17	2.872E+00	(I)	4.5A		
Y	10894	2.770E+00	10.1	-0.41							(E)	1.8		
CHAIN	250	2.900E+00	5.0	0.41										
94 ZR	2103	3.280E+00	5.0	-0.21				0.05	0.05	3.305E+00	(I)	3.5A		
CHAIN	250	3.330E+00	5.0	0.21							(E)	0.8		
95 ZR	762	3.000E+00	20.0	-1.59										
	2025	3.876E+00	5.0	-0.33				5.11	0.85	3.941E+00	(I)	2.2A		
	770	4.080E+00	5.0	0.75							(E)	2.0		
	1014	1.94E+00	5.3	1.24										
CHAIN	250	3.920E+00	5.0	-0.12										
	30514	4.370E+00	20.0	0.49										
96 ZR	2103	4.280E+00	5.0	-0.16				0.03	0.03	4.305E+00	(I)	3.5A		
CHAIN	250	4.330E+00	5.0	0.16							(E)	0.6		

TABLE 10 CHAIN AND CUMULATIVE YIELDS FROM THERMAL FISSION OF 241PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	INT.	EXT./DF	MEAN	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	EXTERNAL	INT.	EXT./DF	MEAN	EXT./DF	MEAN	DEVIATION	DEVIATION
97 ZR	762	3.220E+00	30.0	-1.54										
	771	4.347E+00	5.4	-0.66										
	1014	4.567E+00	5.4	-0.60										
	10894	4.750E+00	4.2	0.28										
	2025	4.846E+00	5.9	0.54										
MO	2103	5.110E+00	5.0	1.73										
CHAIN	250	4.760E+00	5.0	0.27										
98 MO	2103	5.240E+00	5.0											
99 MO	2025	5.45E+00	5.6	-1.46										
	2025	5.753E+00	4.7	-0.26										
	10894	5.760E+00	4.7	-0.29										
	770	6.150E+00	5.0	1.17										
CHAIN	250	6.170E+00	5.0	1.23										
100 MO	2103	6.150E+00	5.0											
101 CHAIN	250	5.940E+00	5.0											
102 RU	2103	6.530E+00	5.0	0.46										
CHAIN	250	6.320E+00	5.0	-0.46										
103 RU	762	5.530E+00	30.0	-0.91										
	771	6.950E+00	4.3	-0.33										
	10894	7.100E+00	4.9	0.26										
	2025	7.100E+00	5.7	0.22										
CHAIN	30514	7.660E+00	20.0	0.42										
104 RU	2103	7.150E+00	5.0	0.71										
CHAIN	250	6.800E+00	5.0	-0.71										
105 RU	10894	5.950E+00	4.9											
106 CHAIN	250	6.080E+00	5.0											
107 RU	2016	4.880E+00	8.4											
108 RU	2016	4.890E+00	8.0											
109 RU	2016	2.730E+00	1.0	-0.53										
PD	771	2.897E+00	10.9	0.53										
111 AG	771	5.90E+00	10.0											
	1016	6.119E-01	8.6											
	2025	6.892E-01	10.7											
112*PD	771	1.661E-01	9.1W	-1.81										
	770	2.230E-01	10.0	1.75										
AG	10894	2.800E-01	14.3	2.33										
113 AG	1014	1.843E-01	16.8											
115 CD (G)	771	1.820E-02	8.7											
121 SB	2025	1.205E-02	18.4											
CHAIN	40194	9.200E-02	20.0											
122 CHAIN	40194	1.060E-01	20.0											
123 CHAIN	40194	1.360E-01	20.0											
124 CHAIN	40194	1.860E-01	20.0											
125 CHAIN	40194	2.620E-01	20.0											
126 CHAIN	40194	3.820E-01	20.0											
127 SB	770	2.270E-01	5.0	1.75										
	771	2.718E-01	8.4											
	2025	2.730E-01	7.7											
CHAIN	40194	5.830E-01	20.0											
128 CHAIN	40194	8.600E-01	20.0											
129 CHAIN	40194	1.380E+00	20.0											

TABLE 14 CHAIN AND CUMULATIVE YIELDS FROM THERMAL FISSION OF 245CM.

(CONT.)

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	YIELDS & SD.	COMPONENT	VALUE	EXT./DF	MEAN	DEVIATION	EXT./DF	MEAN	DEVIATION	EXT./DF	MEAN
111 AG	620x3.357E+00	20.9	-0.30	0.09	0.09	3.487E+00	(I)	15.9A			
112 PD	1173 3.700E+00	24.3	0.30				(E)	4.8			
112 PD	620x1.275E+00	28.7				3.420E+00		12.6			
114 CD	1173 1.800E+00	38.9				1.800E+00		38.9			
115 CD(G)	1173 5.700E-01	5.3	5.700E-01					5.1A			
121 SN(M)	620x6.336E-03	39.8				6.336E-03		39.8			
125 SN(M)	620x7.390E-02	26.7	-0.02			0.00 0.00 7.414E-02	(I)	17.6A			
127 SN	1173 4.400E-01	15.9	0.16			0.04 0.02 4.296E-01	(I)	6.7A			
128 SN	1173 4.400E-01	11.4				0.00 0.00 6.588E-01	(I)	6.0A			
129 SB	1173 1.060E+00	11.3	0.50			0.25 0.25 1.031E+00	(I)	10.1A			
130 SB(G)	1173 7.990E-01	5.3	7.990E-01			0.00 0.00 1.739E+00	(I)	6.2A			
131*SB	1173 2.240E+00	10.7				4.66 2.33 2.915E+00	(I)	2.5 >2			
132 SB	1173 1.830E+00	8.2				9.84 9.84 4.465E+00	(I)	4.1 >2			
133 TE(G)	1173 2.000E+00	8.0				5.390E+00		5.0			
134 TE	1173 5.390E+00	5.0									
135 I	1173 5.480E+00	5.0				11.07 11.07 6.509E+00	(I)	4.2 >2			
136 I (G)	1173 1.800E+00	27.8									
137 I (M)	1173 1.200E+00	58.3				4.42 2.21 5.340E+00	(I)	8.7 >2			
138 XE	1173 4.900E+00	10.4	-2.07					12.9A			

TABLE 14 CHAIN AND CUMULATIVE YIELDS FROM THERMAL FISSION OF 245CM.

(CONT.)

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	YIELDS & SD.	COMPONENT	VALUE	EXT./DF	MEAN	DEVIATION	EXT./DF	MEAN	DEVIATION	EXT./DF	MEAN
138 XE	1173 4.780E+00	7.1				9.20 9.20 6.355E+00	(I)	4.9 >2			
139 XE	1173 4.800E+00	14.6				0.31 0.15 7.166E+00	(I)	7.3A			
140*BA	620x5.063E+00	14.4	-0.79			7.32 1.83 5.632E+00	(I)	2.2			
141 BA	1173 4.010E+00	11.2				5.75 2.87 5.334E+00	(I)	4.4 >2			
142 BA	1173 4.240E+00	10.8				4.33 4.33 4.963E+00	(I)	4.9 >2			
143 CE	620x3.412E+00	17.5	-1.79			6.49 3.25 4.409E+00	(I)	4.8 >2			
144 LA	1173 4.310E+00	7.2				6.11 6.11 3.958E+00	(I)	7.0 >2			
145 CE	1173 3.040E+00	8.9									
146 CE	1173 2.880E+00	12.5				3.84 1.28 2.554E+00	(I)	6.5			
147 ND	1173 2.330E+00	7.3				4.56 1.14 2.515E+00	(I)	3.9			
148 PM	620x1.945E+00	26.3	-1.13								
149 ND	1173 1.940E+00	7.7				0.00 0.00 1.940E+00	(I)	7.3A			
150 PM	620x1.935E+00	23.7	-0.01								
151 ND	1173 1.500E+00	4.3				5.05 1.68 1.120E+00	(I)	3.5			
152 PM	1173 1.400E+00	50.0									
153 PM	1173 6.700E-01	80.6				9.825E-01		26.5			
154 SM	620x9.825E-01	26.5									
155 EU	620x2.074E-01	25.6	-2.91			8.45 8.45 3.099E-01	(I)	12.8 >2			
156 EU	1173 4.400E-01	13.6									

TABLE 15 CHAIN AND CUMULATIVE YIELDS FROM THERMAL FISSION OF 249CF.

(CONT.)

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	EXTERNAL	INT. EXT./DF	MEAN	STANDARD	DEVIATION
NO.	EL.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	EXTERNAL	INT. EXT./DF	MEAN	STANDARD	DEVIATION
144 LA	12705	3.360E+00	7.7					1.19	1.19	4.412E+00	(I) 4.6
CE	695	4.180E+00	7.0	-1.09							(E) 5.0A
	205	4.620E+00	6.0	1.09							
145 CE	12705	3.560E+00	15.2							3.560E+00	15.2
146 CE	12705	3.160E+00	15.7	-0.70				0.11	0.05	3.222E+00	(I) 6.3A
	12705	3.160E+00	15.3	-0.19							(E) 1.5
PR	12705	3.280E+00	8.2	0.33							
147 ND	12705	2.600E+00	6.9	-0.98				2.08	0.69	2.747E+00	(I) 3.6A
	205	2.620E+00	15.0	0.98							(E) 3.0
	12710	2.800E+00	4.6	0.64							
	695	3.270E+00	15.0	1.09							
149 ND	12710	1.940E+00	5.2M	-2.07				14.35	2.87	2.154E+00	(I) 3.1
	12705	2.040E+00	7.8	-0.90							(E) 5.3A
	1051	2.310E+00	10.0	1.02							
	1051	2.620E+00	10.0	1.86							
	1051	2.850E+00	10.0M	2.50							
PM	695	2.360E+00	7.0	1.40							
151 ND	12705	1.140E+00	10.5					8.85	1.77	1.683E+00	(I) 3.5
PM	1051	1.540E+00	10.0	-1.00							(E) 4.6A
	12705	1.610E+00	10.6	-0.45							
	12710	1.610E+00	5.0	-1.32							
	1051	1.980E+00	10.0	1.57							
	1051	2.120E+00	10.0	2.15							
153 SM	1052	1.120E+00	15.0	-0.49				12.99	2.17	1.201E+00	(I) 2.9
	12710	1.130E+00	5.0	-1.59							(E) 4.2A
	1052	1.190E+00	15.0	1.02							
	695	1.260E+00	5.0	1.12							
	12705	1.270E+00	7.1	0.83							
	1051	1.630E+00	10.0M	2.48							
	1052	1.300E+00	15.0	-2.01							
154 PM(M)	12705	5.100E-01	39.2								
155 SM	12710	6.200E-01	6.5							6.200E-01	6.5
156 SM	1052	5.900E-01	15.0	-1.24				15.44	2.21	6.949E-01	(I) 3.8
	1052	6.100E-01	15.0	0.97							(E) 5.7A
	1052	8.100E-01	15.0	1.52							
	1052	9.700E-01	15.0	1.92							
	1051	9.900E-01	10.0M	2.43							
EU	1051	6.000E-01	10.0	-1.77							
	12705	6.400E-01	9.4	-0.92							
	12705	6.400E-01	9.4	-0.92							
157 EU	12710	3.600E-01	8.3	-1.76				5.93	1.19	3.999E-01	(I) 4.9
	1052	3.800E-01	15.0	-0.37							(E) 5.3A
	1051	4.100E-01	10.0	0.28							
	1052	4.800E-01	15.0	1.56							
	695	5.200E-01	15.0	1.59							
159 GD	1052	3.300E-01	15.0	-0.62				1.64	0.41	3.576E-01	(I) 6.0A
	1052	3.400E-01	15.0	-0.38							(E) 3.9
	1051	3.700E-01	10.0	0.41							
	1052	4.200E-01	15.0	1.05							
161 TB	1052	1.900E-01	15.0	-0.47				0.22	0.22	1.990E-01	(I) 10.6A
	695	2.100E-01	15.0	0.47							(E) 5.0

TABLE 16 CHAIN AND CUMULATIVE YIELDS FROM THERMAL FISSION OF 251CF.

A EL.	REF.	EXPERIMENTAL	NO.	YIELDS & SD	MEAN	R	CHI2/DF	CHI2	EXTERNAL	INT. EXT./DF	MEAN	STANDARD	DEVIATION
91 SR	903	5.100E-01	8.0								5.100E-01	8.0	
93 Y	903	7.200E-01	10.0								7.200E-01	10.0	
95 ZR	903	9.900E-01	10.0								9.900E-01	10.0	
97 ZR	903	1.610E+00	7.0								1.610E+00	7.0	
99 MO	903	3.220E+00	6.0								3.220E+00	6.0	
105 RU	903	4.790E+00	9.0								4.790E+00	9.0	
109 PD	903	5.160E+00	8.0								5.160E+00	8.0	
111 AG	903	4.930E+00	5.0								4.930E+00	5.0	
112 PD	903	5.240E+00	8.0								5.240E+00	8.0	
113 AG(G)	903	3.650E+00	10.0								3.650E+00	10.0	
115 CD	903	4.080E+00	5.0			-1.82				3.31	3.31	4.345E+00 (I)	3.3 -2.82
CHAIN	2014	4.600E+00	4.3			1.82						(E)	6.0A
121 SN(G)	903	4.600E-01	8.0			-1.45				2.10	2.10	4.916E-01 (I)	6.0 -2.82
CHAIN	2014	5.500E-01	9.1			1.45						(E)	8.7A
125 SN(G)	903	1.900E-01	10.0								1.900E-01	10.0	
127 SB	903	5.900E-01	10.0								5.900E-01	10.0	
129 SB	903	9.000E-01	10.0								9.000E-01	10.0	
131 I	903	1.770E+00	8.0								1.770E+00	8.0	
132 TE	903	4.180E+00	10.0			-0.38				0.14	0.14	4.295E+00 (I)	6.7A
2014	4.400E+00	9.1				0.38						(E)	2.6
133 I	903	3.780E+00	10.0			-0.40				0.16	0.16	3.884E+00 (I)	7.1A
2014	4.000E+00	10.0				0.40						(E)	2.8
135 I	2014	4.060E+00	9.3								4.060E+00	9.3	
140 BA	903	3.60E+00	5.0								3.60E+00	5.0	
141 CE	903	4.790E+00	10.0								4.790E+00	10.0	
143 CE	903	4.910E+00	6.0								4.910E+00	6.0	
147 ND	903	3.490E+00	10.0								3.490E+00	10.0	
149 PM	903	3.000E+00	10.0								3.000E+00	10.0	
151 PM	903	1.240E+00	15.0								1.240E+00	15.0	
156 SM	903	5.600E-01	10.0								5.600E-01	10.0	

TABLE 17 CHAIN AND CUMULATIVE YIELDS FROM THERMAL FISSION OF 254ES.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL	CHI2	EXT.	DF	WEIGHTED	STANDARD
NO.	YIELDS & SD.	NO.	YIELDS & SD.	COMPONENT	VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION		
=====												
89 SR	927 5.300E-02	15.0							5.300E-02		15.0	
91 SR	927 2.800E-01	11.0							2.800E-01		11.0	
95 ZR	927 7.200E-01	10.0							7.200E-01		10.0	
97 ZR	927 9.900E-01	10.0							9.900E-01		10.0	
99 MO	927 2.340E+00	8.0							2.340E+00		8.0	
103 RU	927 3.150E+00	10.0							3.150E+00		10.0	
105 RU	927 4.290E+00	10.0							4.290E+00		10.0	
106 RU	927 4.070E+00	10.0							4.070E+00		10.0	
109 PD	927 3.760E+00	15.0							3.760E+00		15.0	
111 AG	927 4.230E+00	5.0							4.230E+00		5.0	
112 PD	927 4.400E+00	10.0							4.400E+00		10.0	
113 AG(G)	927 3.490E+00	10.0							4.720E+00		10.0	
=====												
CHAIN	927 4.720E+00	10.0										
115 CD(G)	927 5.340E+00	10.0	5.340E+00	0.00	0.00	0.0	0.00	0.00	5.640E+00	(I)	6.9A	
CD(M)	927 3.000E-01	10.0	3.000E-01	0.00	0.00					(E)	0.0	
=====												
CHAIN	927 5.640E+00	10.0	5.640E+00	0.00	0.00							
121 SN	927 2.540E+00	6.0	-1.15				1.33	1.33	2.621E+00	(I)	5.2	
=====												
CHAIN	927 2.920E+00	10.0	1.15							(E)	5.9A	
125 SN	927 4.470E-01	11.0										
CHAIN	927 9.400E-01	10.0							9.400E-01		10.0	
127 SB	927 9.500E-01	11.0							9.500E-01		11.0	
129 SB	927 1.940E+00	10.0							1.940E+00		10.0	
131 I	927 3.640E+00	10.0							3.640E+00		10.0	
132 TE	927 4.760E+00	10.0							4.760E+00		10.0	
133 I	927 5.090E+00	15.0							5.090E+00		15.0	
135 I	927 5.310E+00	15.0							5.310E+00		15.0	
140 BA	927 4.010E+00	5.0							4.010E+00		5.0	
141 CE	2014 4.600E+00	6.5	-0.06				0.00	0.00	4.612E+00	(I)	5.1A	
	927 4.630E+00	8.0	0.06							(E)	0.3	
143 CE	927 4.890E+00	8.0							4.890E+00		8.0	
144 CE	927 3.920E+00	10.0							3.920E+00		10.0	
151 PM	927 1.730E+00	20.0							1.730E+00		20.0	
153 PM	927 6.20E+00	20.0							6.20E+00		20.0	
156 SM	927 8.000E-01	20.0							8.000E-01		20.0	
157 EU	927 7.600E-01	15.0							7.600E-01		15.0	

TABLE 18 CHAIN AND CUMULATIVE YIELDS FROM THERMAL FISSION OF 255PM.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL	CHI2	EXT.	DF	WEIGHTED	STANDARD
NO.	YIELDS & SD.	NO.	YIELDS & SD.	COMPONENT	VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION		
=====												
91 SR	2014 5.000E-01	20.0							5.000E-01		20.0	
93 Y	902 2.000E-01	20.0							2.000E-01		20.0	
97 ZR	902 7.000E-01	10.0							7.000E-01		10.0	
99 MO	902 1.560E+00	10.0							1.560E+00		10.0	
105 RU	902 2.430E+00	10.0							2.430E+00		10.0	
109 PD	902 2.600E+00	20.0							2.600E+00		20.0	
111 AG	902 2.850E+00	20.0							2.850E+00		20.0	
112 PD	902 3.740E+00	20.0							3.740E+00		20.0	
113 AG	902 3.240E+00	20.0							3.240E+00		20.0	
115 CD	902 5.130E+00	10.0	-0.60						5.329E+00	(I)	7.3A	
CHAIN	2014 5.600E+00	10.7	0.60							(E)	4.4	
121 SN(G)	902 3.270E+00	10.0	-0.83						3.442E+00	(I)	7.4A	
CHAIN	2014 3.700E+00	10.8	0.83							(E)	6.1	
125 SN(G)	2014 1.600E+00	12.5							1.600E+00		12.5	
127 SB	902 2.390E+00	10.0							2.390E+00		10.0	
129 SB	902 2.330E+00	10.0							2.330E+00		10.0	
131 I	902 3.350E+00	10.0	0.10						3.373E+00	(I)	7.3A	
	2014 3.400E+00	10.5	0.10							(E)	0.7	
132 TE	902 4.900E+00	10.0							4.900E+00		10.0	
133 I	902 5.580E+00	10.0	-0.15						5.636E+00	(I)	7.3A	
	2014 5.580E+00	10.0	0.15							(E)	0.7	
135 I	902 6.150E+00	10.0							6.150E+00		10.0	
140 BA	902 5.030E+00	10.0							5.030E+00		10.0	
143 CE	2014 3.00E+00	10.8							3.700E+00		10.8	
149 PM	902 1.530E+00	10.0							1.530E+00		10.0	
151 PM	902 1.340E+00	10.0							1.340E+00		10.0	
153 SM	902 1.040E+00	10.0							1.040E+00		10.0	
157 EU	902 3.800E-01	10.0							3.800E-01		10.0	

TABLE 19 CHAIN AND CUMULATIVE YIELDS FROM THERMAL FISSION OF 257PM.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT. EXT./DF	MEAN	DEVIATION	
112 PD	13458	3.020E+00	19.9			3.020E+00	19.9	
127 SB	13458	6.300E+00	15.1			6.300E+00	15.1	
132 TE	13458	5.570E+00	15.1			5.570E+00	15.1	
140 BA	13458	3.950E+00	15.2			3.950E+00	15.2	

TABLE 20 CHAIN AND CUMULATIVE YIELDS FROM EPI-TH FISSION OF 239PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT. EXT./DF	MEAN	DEVIATION	
72 ZN	13219	1.013E-04	18.0			1.013E-04	18.0	
87 CHAIN	21560	8.534E-01	5.1			8.534E-01	5.1	
88 CHAIN	21560	1.256E+00	4.6			1.256E+00	4.6	
97 CHAIN	21560	5.230E+00	1.8			5.230E+00	1.8	
105 CHAIN	21560	5.778E+00	3.0			5.778E+00	3.0	
107 CHAIN	21560	3.023E+00	5.7			3.023E+00	5.7	
111 CHAIN	21560	2.372E-01	4.0			2.372E-01	4.0	
115 CD(G)	13219	2.434E-02	16.5	0.07	0.00	2.410E-02 (1)	7.7A	
CHAIN	21560	2.403E-02	8.6	-0.07			(E)	0.5
127 CHAIN	21560	3.757E-01	8.6			3.757E-01	8.6	
128 CHAIN	21560	7.708E-01	7.0			7.708E-01	7.0	
129 CHAIN	21560	1.385E+00	5.5			1.385E+00	5.5	
140 CHAIN	21560	5.373E+00	2.7			5.373E+00	2.7	
149 CHAIN	21560	1.242E+00	4.3			1.242E+00	4.3	

TABLE 21 CHAIN AND CUMULATIVE YIELDS FROM FAST FISSION OF 232TH. (CONT.)

A EL. NO.	REF. NO.	EXPERIMENTAL YIELDS & SD	MEAN	R	CHI2/DF	COMPONENT VALUE	EXTERNAL	TOTAL CHI2	INT. EXT./DF	WEIGHTED MEAN	STANDARD DEVIATION
CHAIN 2002 6.030E+00 7.0											
144 LA 2010 3.580E+00 10.6											
CE 13667 7.100E+00 17.0											
145 CE 2010 4.200E+00 6.2											
CHAIN 2002 3.010E+00 10.3											
146 CE 2010 6.220E+00 20.0											
CHAIN 2002 3.530E+00 12.2											
147 ND 994 2.590E+00 15.0											
148 CE 2010 1.910E+00 8.9											
CHAIN 364 2.080E+00 7.0											
149 ND 2010 1.150E+00 13.0											
PM 225f9 485E-01 22.6											
CHAIN 2002 1.160E+00 14.7											
150 CHAIN 364 1.040E+00 15.0											
151 PM 994 3.400E-01 25.0											
153 SM 362 2.080E-01 10.0											
156 EU 225f2 521E-03 12.7											

TABLE 22 CHAIN AND CUMULATIVE YIELDS FROM FAST FISSION OF 231PA.

A EL. NO.	REF. NO.	EXPERIMENTAL YIELDS & SD	MEAN	R	CHI2/DF	COMPONENT VALUE	EXTERNAL	TOTAL CHI2	INT. EXT./DF	WEIGHTED MEAN	STANDARD DEVIATION
83 BR 651 2.270E+00 15.0											
85 KR(G) 580r1.015E+00 15.4											
89 SR 227r7.217E+00 25.1											
91 SR 227r7.081E+00 25.1											
97 ZR 651 4.500E+00 15.0											
99 MO 651 2.500E+00 15.0											
103 RU 651 3.280E-01 15.0											
105 RU 651 1.540E-01 15.0											
106 RU 651 1.080E-01 15.0											
109 PD 227r8.138E-02 26.5											
PD(G) 651 8.300E-02 15.0											
111 AG 227r1.019E-01 25.2											
112 PD 651 1.30E-02 15.6											
113 AG(G) 651 7.700E-02 15.0											
115 CD(M) 227f6.485E-03 26.5											
CHAIN 651 8.000E-02 15.0											
121 SN(G) 651 7.600E-02 15.0											
SN(M) 227r1.420E-02 38.8											
129 CHAIN 651 1.180E+00 15.0											
131 I 580r2.696E+00 15.3											
132 TE 651 3.420E+00 15.0											
133 XE 580r5.288E+00 15.6											
135 XE 580r7.120E+00 15.7											
137 CS 580r7.332E+00 15.3											
140 BA 227f6.763E+00 25.1											
LA 580r7.432E+00 18.1											
141 CE 580r7.177E+00 15.4											
143 CE 580r5.439E+00 15.4											
144 CE 580r4.990E+00 15.7											
147 ND 580r2.036E+00 15.4											
149 PM 580r1.082E+00 18.2											
153 SM 651 7.900E-02 15.0											

TABLE 23 CHAIN AND CUMULATIVE YIELDS FROM FAST FISSION OF 232U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION	
87 BR	12926 2.810E+00	6.4						
137 I	12926 4.800E-01	70.8						

TABLE 24 CHAIN AND CUMULATIVE YIELDS FROM FAST FISSION OF 233U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION	
3 M	91204 1.500E-01	50.0						
4 HE PI	2057+2.003E-01	10.8						
83 SE	40554 5.500E-01	12.7						
KR	868 9.950E-01	5.0						
84 KR	868 1.640E+00	5.0						
85 KR (M)	40554 3.050E+00	9.2						
CHAIN	21736 2.120E+00	20.9						
86 KR	868 2.780E+00	5.0						
87 BR	12926 2.310E+00	8.2						
KR	40554 4.850E+00	10.5						
RB	868 3.840E+00	10.0						
88 SR	868 5.120E+00	5.0						
89 SR	868 6.300E+00	7.0						
90 CHAIN	868 6.450E+00	5.0						
91 Y (G)	29+6.169E+00	15.9						
Y (M)	40554 4.200E+00	9.1						
ZR	868 6.440E+00	5.0						
CHAIN	21736 5.139E+00	15.4						
92 SR	40554 5.900E+00	8.0						
ZR	868 6.540E+00	5.0						
CHAIN	21736 5.139E+00	20.3						
93 R	868 6.240E+00	5.0						
94 ZR	868 6.740E+00	5.0						
95 ZR	21707 6.400E+00	4.6						
MO	868 6.290E+00	5.0						
CHAIN	21736 6.240E+00	3.9						
96 ZR	868 5.700E+00	5.0						
97 ZR	21707 5.510E+00	3.6						
MO	868 5.440E+00	5.0						
CHAIN	21736 5.078E+00	9.1						
98 MO	868 5.140E+00	5.0						
99 MO	61 4.750E+00	8.0						
21707 4.910E+00	3.5							
CHAIN	21736 3.977E+00	20.3						
100 MO	868 4.360E+00	5.0						
103*RU	21707 1.680E+00	4.9W						
61 4.130E-01	50.0W							
CHAIN	21736 1.652E+00	8.1						
104 TC	40554 1.680E+00	10.1						
106 RU	61 1.600E-01	13.0						
CHAIN	21736 2.876E-01	9.1						
111 AG	29+1.373E-01	20.5						
61 8.370E-02	10.0							
115 CD(G)	61 5.200E-02	11.0						

TABLE 25 CHAIN AND CUMULATIVE YIELDS FROM FAST FISSION OF 235U . (CONT)

A EL. NO.	REF.	EXPERIMENTAL YIELDS & SD	MEAN COMPONENT VALUE	R CH2/DF	CHI2	CHI2 EXTERNAL	TOTAL INT. EXT./DF	WEIGHTED STANDARD DEVIATION
135 TE	21743	2.080E+00	3.9				9.91	1.42 6.304E+00 (I) 2.0
I	40554	6.780E+00	5.0					(E) 2.4A
XE	40554	7.350E+00	5.0					
CS	414	5.750E+00	5.0					-2.15
	413	6.010E+00	5.0					-1.08
	869	6.520E+00	5.0					0.72
CHAIN	21736	5.109E+00	20.0					-1.30
	245	5.930E+00	10.0					0.82
	1109	6.670E+00	5.0					1.19
	924	6.680E+00	5.0					1.22
	21155	6.720E+00	20.0					0.31
136 TE	21743	8.500E-01	5.0					0.12 0.06 6.115E+00 (I) 4.4A
XE	245	5.930E+00	10.0					(E) 1.1
	869	6.160E+00	5.0					0.29
CHAIN	21155	6.200E+00	20.0					0.07
137 I	21743	2.540E+00	4.7					19.95 0.87 5.961E+00 (I) 0.9A
	12926	3.000E+00	20.0					(E) 0.9
XE	942	5.820E+00	10.0					-0.24
CS	942	5.820E+00	10.0					-0.85
	414	5.320E+00	3.0					-2.47
	413	5.610E+00	5.0					-1.28
	21707	6.140E+00	8.5					0.34
	13272	6.200E+00	10.0					0.39
	235	6.300E+00	5.0					1.09
	22066	6.350E+00	3.5W					2.48
CHAIN	955	5.775E+00	4.7					-0.70
	959	5.812E+00	4.7					-0.56
	970	5.828E+00	3.5					-0.68
	965	5.881E+00	3.5					-0.40
	966	5.885E+00	3.5					-0.38
	958	5.935E+00	3.5					-0.13
	957	5.950E+00	3.5					-0.06
	21736	5.963E+00	6.1					0.01
	963	5.982E+00	3.5					0.10
	953	6.027E+00	3.5					0.32
	869	6.160E+00	10.0					0.46
	245	6.250E+00	5.0					0.94
	1109	6.250E+00	5.0					1.06
	969	6.267E+00	4.7					1.06
	21155	6.270E+00	20.0					0.25
138 I	21743	1.270E+00	4.7					0.51 0.17 6.513E+00 (I) 3.3A
XE	21743	5.740E+00	3.5					(E) 1.4
CS	942	6.120E+00	10.0					
BA	21624	6.348E+00	5.0					-0.71
BA	869	6.460E+00	5.0					0.57
CHAIN	245	6.610E+00	10.0					0.15
	21155	6.700E+00	20.0					0.14
139 I	21743	4.800E-01	6.2					1.88 0.47 6.383E+00 (I) 1.4A
XE	21743	4.200E+00	4.8					(E) 0.9
BA	40554	5.700E+00	10.5					-1.22
LA	1334	6.141E+00	3.5					0.57
	1369	6.760E+00	10.0					0.56
CHAIN	21155	6.440E+00	20.0					0.04
	924	6.540E+00	5.0					0.50
140 XE	21743	2.630E+00	3.8					45.79 1.17 5.865E+00 (I) 0.6
CS	21743	5.700E+00	1.4					(E) 0.6A
BA	161	5.000E+00	15.0					-1.15
	790	5.670E+00	5.0					-0.69

TABLE 25 CHAIN AND CUMULATIVE YIELDS FROM FAST FISSION OF 235U . (CONT)

A EL. NO.	REF.	EXPERIMENTAL YIELDS & SD	MEAN COMPONENT VALUE	R CH2/DF	CHI2	CHI2 EXTERNAL	TOTAL INT. EXT./DF	WEIGHTED STANDARD DEVIATION
141 XE	21743	6.300E-01	20.6					13.49 1.35 5.707E+00 (I) 1.3
BA	21743	5.800E+00	3.5					(E) 1.5A
CE	22066	5.690E+00	2.1					-0.19
	21707	5.830E+00	3.9					0.57
	625	6.080E+00	7.0					0.89
	161	6.100E+00	10.0					0.65
	625	6.280E+00	5.0					1.88
PR	283	5.880E+00	7.0					0.43
CHAIN	969	5.039E+00	4.1W					-2.33
	924	5.560E+00	5.0					-0.55
	21155	5.570E+00	20.0					-0.12
	21736	5.580E+00	4.0					-0.06
142 CS	21743	2.660E+00	3.8					4.05 0.51 5.702E+00 (I) 1.9A
BA	21743	5.640E+00	1.8					(E) 1.3
LA	21624	5.167E+00	6.1					-1.81
	40554	5.700E+00	7.0					0.00
	21743	5.800E+00	4.8					0.38
CE	869	5.780E+00	5.0					0.29
CHAIN	924	5.500E+00	5.0					-0.43
	21155	5.630E+00	20.0					-0.06
	837	5.770E+00	5.0					0.25
	245	5.820E+00	10.0					0.21
	1109	5.900E+00	4.0					0.94
143 CS	21743	1.230E+00	9.8					34.94 1.46 5.605E+00 (I) 0.7
BA	21743	4.810E+00	2.1					(E) 0.8A
CE	21624	5.214E+00	3.0W					-2.49
	21743	5.250E+00	5.3					-1.28
	40554	5.500E+00	2.2					-1.03
	869	5.500E+00	5.0					-0.19
	882	5.520E+00	8.0					0.61
	22057	5.810E+00	5.8					0.12
ND	659	5.640E+00	5.0					

TABLE 25 CHAIN AND CUMULATIVE YIELDS FROM FAST FISSION OF 235U . (CONT.)

A EL.	REF.	EXPERIMENTAL	NO.	YIELDS & SD	MEAN	R	CH12/DF	CH12	CH12	TOTAL	CH12	EXT./DF	MEAN	DEVIATION
NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.
153 SM	34r1.872E-01	15.8	1.10	8.04	1.34	1.550E-01	(I)	2.9						
CHAIN														
958r1.445E-01	6.6	-1.26												
957r1.450E-01	6.6	-0.57												
953r1.629E-01	6.6	0.81												
965r1.775E-01	6.6	2.09												
966r1.845E-01	50.2	0.32												
154 SM	869 7.200E-02	5.0												
CHAIN														
245 1.130E-01	5.0													
156 EU	625 1.350E-02	10.0M	-2.45											
103r2.101E-02	7.4	1.81												
34r2.185E-02	16.0	1.04												
CHAIN														
953r1.392E-02	17.2	-1.81												
958r1.478E-02	17.2	-1.37												
959r1.561E-02	5.7M	-2.41												
954r1.617E-02	5.7	-2.35												
956r1.640E-02	5.7	-2.06												
957r1.698E-02	5.7	-1.38												
964r1.789E-02	5.7	-0.35												
963r1.812E-02	5.7	-0.12												
965r1.900E-02	5.7	0.73												
966r1.942E-02	5.7	1.11												
970r1.943E-02	5.7M	2.48												
970r2.247E-02	5.7M	2.45												
971r2.286E-02	5.7M	2.44												
969r2.531E-02	5.7M	2.44												
159 GD	34r3.182E-03	16.4												
161 TB	34r4.587E-04	17.2	1.91											
CHAIN														
963r2.169E-04	21.7	-2.07												
965r2.538E-04	13.1	-1.87												
966r2.765E-04	10.2	-1.38												
972r3.438E-04	10.2	1.05												
969r4.040E-04	9.9M	2.50												

TABLE 26 CHAIN AND CUMULATIVE YIELDS FROM FAST FISSION OF 236U .

A EL.	REF.	EXPERIMENTAL	NO.	YIELDS & SD	MEAN	R	CH12/DF	CH12	CH12	TOTAL	CH12	EXT./DF	MEAN	DEVIATION
NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.
85 CHAIN	21736r1.385E+00	8.9												
89 CHAIN	989r3.327E+00	8.8												
91 SR	40878 5.440E+00	7.2	0.69											
CHAIN	21736r4.772E+00	6.5	-1.75											
92 SR	40878 4.420E+00	13.1												
Y	40878 5.360E+00	9.6												
CHAIN	21736r5.439E+00	15.8												
93 SR	40878 5.400E+00	5.9	1.69											
Y	40878 4.450E+00	12.8	-1.22											
CHAIN	21736r4.772E+00	6.5	-1.75											
94 Y	40878 4.700E+00	27.7												
CHAIN	21736r5.593E+00	15.8												
97 ZR	40878 5.340E+00	5.1	1.32											
CHAIN	21736r4.362E+00	15.8	-1.32											
99 MO	40878 5.30E+00	14.0	-0.56											
CHAIN	21736r4.772E+00	6.5	-1.75											
97 ZR	40878 5.340E+00	5.1	1.32											
CHAIN	21736r4.413E+00	300.0	-0.07											
101 MO	40878 5.010E+00	11.8	-0.38											
CHAIN	21736r4.362E+00	15.8	-1.32											
103 CHAIN	21736r3.643E+00	8.6												
106 CHAIN	21736r8.723E-01	20.6												
111 CHAIN	989r5.687E-02	10.4												
125 CHAIN	21736r1.693E-01	20.6	1.89											
CHAIN	21155 8.000E-02	40.0	-1.89											
126 CHAIN	21155 2.900E-01	20.0												
127 CHAIN	21736r1.796E-01	17.8	-2.46											
CHAIN	21155 3.850E-01	20.0	2.46											
128 SB	40878 1.100E-01	27.3												
CHAIN	21155 5.750E-01	20.0												
129 SB	40878 2.400E-01	58.3												
CHAIN	21155 9.600E-01	20.0												
130 SB	40878 8.200E-01	46.3												
CHAIN	21155 1.920E+00	20.0												
131 TE (M)	40878 7.100E-01	14.1												
XE	40877r1.199E+00	9.4												
CHAIN	21736r2.720E+00	15.8	-0.95											
132 TE	40878 3.970E+00	11.3	-0.23											
XE	40877r2.594E+00	8.7												
CHAIN	21736r3.849E+00	5.6	-1.69											

TABLE 26 CHAIN AND CUMULATIVE YIELDS FROM FAST FISSION OF 236U .

(CONT.)

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION			
133 TE(M)	40878	2.420E+00	16.1		0.19	0.19	6.674E+00	(I)	9.1A		
I	40878	5.730E+00	9.1					(E)	4.0		
	40878	5.420E+00	7.0								
CHAIN	21155	2.00E+00		-0.44							
	21155	2.00E+00		0.44							
	21736	6.425E+00	10.3								
134 TE	40878	6.180E+00	8.7		0.01	0.01	7.660E+00	(I)	5.6A		
	40878	6.590E+00	10.6					(E)	0.4		
I	40878	6.450E+00	12.0								
	40878	6.420E+00	9.7								
XE	40877	7.670E+00	5.8	0.08							
CHAIN	21155	7.550E+00	20.0	-0.08							
135 I	40878	6.90E+00		-0.08							
	40878	6.720E+00	7.1	1.28							
	40878	6.720E+00	7.1		4.58	1.15	6.184E+00	(I)	3.5A		
									(E)	4.1A	
XE	40877	7.5.601E+00	19.1	-0.56							
CHAIN	21736	7.5.183E+00	15.8	-1.28							
	21155	6.930E+00	10.0	1.14							
136 XE	40877	7.5.225E+00	7.4								
CHAIN	21155	6.200E+00	20.0								
137 CHAIN	21736	5.09E+00	22.3	-0.08							
	21155	6.070E+00	5.0	1.12							
138 CHAIN	21155	5.990E+00	20.0								
139 BA	40878	6.140E+00	11.7	-0.33							
	40878	6.500E+00	17.2	0.36							
CHAIN	21155	5.880E+00	20.0	-0.41							
140 BA	40878	4.970E+00	9.3								
	40878	5.200E+00	5.8		0.02	0.02	5.698E+00	(I)	8.6A		
									(E)	1.2	
CHAIN	989	5.585E+00	16.7	-0.14							
	21155	5.740E+00	10.0	0.14							
141 CHAIN	21736	4.977E+00	11.4	-0.67							
	21155	5.510E+00	10.0	0.67							
142 LA	40878	4.930E+00	10.5	-0.53							
	40878	5.180E+00	11.0	0.07							
CHAIN	21155	5.350E+00	10.0	0.47							
143 CHAIN	989	5.585E+00	16.7	-0.14							
	21155	5.740E+00	10.0	0.14							
	21155	5.200E+00	1.8	2.17							
					4.72	4.72	4.430E+00	(I)	8.6A		
									(E)	1.2	
144 CHAIN	989	4.436E+00	12.3	-0.41							
	21736	4.670E+00	7.4	0.21							
	21155	4.890E+00	20.0	0.28							
145 CHAIN	21155	3.690E+00	20.0								
146 PR	40878	3.370E+00	11.3	-0.15							
	40878	3.690E+00	15.4	0.57							
CHAIN	21155	3.160E+00	20.0	-0.44							
147 CHAIN	990	1.924E+00	12.4	-0.43							
	990	1.930E+00	12.4	-0.41							
	990	1.939E+00	12.4	-0.36							
	990	1.957E+00	12.4	-0.28							
	990	1.959E+00	12.4	-0.27							
	989	2.024E+00	12.4	-0.01							
	990	2.057E+00	12.4	0.14							
	990	2.079E+00	12.4	0.23							
	21736	2.104E+00	6.9	0.64							
	21155	2.500E+00	20.0	0.96							
148 CHAIN	21155	1.800E+00	20.0								
149 CHAIN	21155	1.470E+00	20.0								
150 CHAIN	21155	1.020E+00	20.0								

TABLE 26 CHAIN AND CUMULATIVE YIELDS FROM FAST FISSION OF 236U .

(CONT.)

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION			
151 CHAIN	21736	1.950E+00	19.0	-3.03							
	21155	7.400E+00	20.0								
152 CHAIN	21155	5.600E+00	20.0								
	989	2.969E+00	12.4								
156 CHAIN	989	2.969E+00	12.4								
	989	3.928E+00	14.8								
161 CHAIN	989	3.928E+00	14.8								

TABLE 27 CHAIN AND CUMULATIVE YIELDS FROM FAST FISSION OF 238U .

(CONT)

A EL.	REF.	EXPERIMENTAL	NO.	YIELDS & SD	MEAN	R	CH12/DF	CH12	CH12	TOTAL	CH12	EXT./DF	MEAN	STANDARD
NO.							COMPONENT	VALUE	EXTERNAL	INT.	EXT./DF			DEVIATION
148 CE	2004	1.760E+00	7.4							8.59	2.15	2.281E+00	(I)	1.0 >2
ND	870	2.080E+00	5.0			-2.01							(E)	1.4A
	22050	2.300E+00	1.0M			1.36								
	657	2.400E+00	9.0			0.56								
CHAIN	21155	2.000E+00	20.0			-0.70								
149 ND	40878	4.000E+00	45.0			1.29								
	870	2.080E+00	5.0			1.29								
	870	2.080E+00	5.0			1.29								
	1075	1.720E+00	18.0			0.18								
	35x1	8.77E+00	18.0			0.61								
SM	870	1.590E+00	5.0			-1.47								
CHAIN	21155	1.590E+00	20.0			-0.44								
150 ND	870	1.250E+00	5.0			-1.39				3.26	0.81	1.312E+00	(I)	3.3A
	22050x1	1.397E+00	10.1			0.63							(E)	3.0
	657	1.490E+00	10.0			1.25								
CHAIN	21155	1.190E+00	20.0			-0.52								
	721	1.350E+00	6.0			0.56								
151 PM	2109	6.280E-01	20.0			-1.44				7.96	1.14	8.088E-01	(I)	1.4
	1075	8.800E-01	9.0			0.91							(E)	1.5A
SM	870	7.940E-01	5.0			-0.39								
CHAIN	21155	7.300E-01	20.0			-0.54								
	1114	8.000E-01	5.0			-0.23								
	21736x8	0.025E-01	1.6			-0.91								
	1115x8	0.864E-01	6.1			1.47								
	721	8.900E-01	6.0			1.56								
152 SM	870	5.210E-01	5.0			0.07				0.07	0.07	5.573E-01	(I)	5.7A
CHAIN	21155	5.300E-01	20.0			-0.27								
	721	5.600E-01	6.0			0.27								
153 SM	2109	3.590E-01	10.0			-0.09				26.30	2.19	3.623E-01	(I)	3.1A
	35x4	0.18E-01	15.8			0.63								
	30743	4.030E-01	10.2			1.01								
	36	4.320E-01	15.0			1.09								
	1075	4.800E-01	9.0M			2.48								
CHAIN	999x2	5.93E-01	6.5M			-2.04								
	1000x3	3.50E-01	6.5			-1.36								
	1001x3	7.46E-01	6.5			0.54								
	1003x3	9.21E-01	6.5			1.24								
	1002x3	9.41E-01	6.5			1.32								
	1008x4	0.01E-01	6.5			1.54								
	1008x4	0.01E-01	6.5			1.78								
	1007x4	3.73E-01	6.5			2.14								
154 SM	870	2.130E-01	5.0									2.400E-01		7.0
CHAIN	721	2.400E-01	7.0											
156 EU	626	4.300E-02	19.0M			-2.50				25.06	1.39	6.734E-02	(I)	1.0
	2109	4.700E-02	20.0			-2.17							(E)	1.2A
	176	6.100E-02	15.0			-0.69								
	30743	6.200E-02	14.5			-0.60								
	105x6	5.25E-02	7.4			-0.44								
	35x6	8.00E-02	15.0			0.15								
	13379	7.300E-02	13.7			0.57								
	231	7.790E-02	14.0			0.97								
CHAIN	1009x6	3.33E-02	3.1			-2.16								

TABLE 27 CHAIN AND CUMULATIVE YIELDS FROM FAST FISSION OF 238U .

(CONT)

A EL.	REF.	EXPERIMENTAL	NO.	YIELDS & SD	MEAN	R	CH12/DF	CH12	CH12	TOTAL	CH12	EXT./DF	MEAN	STANDARD
NO.							COMPONENT	VALUE	EXTERNAL	INT.	EXT./DF			DEVIATION
159 GD	36	8.310E-03	15.0			-0.06				0.00	0.00	8.357E-03	(I)	11.0A
	35x8	4.13E-03	16.3			0.06							(E)	0.6
161 TB	105x1	1.78E-03	21.7			-0.22				12.21	1.74	1.161E-03	(I)	9
	2109	1.500E-03	30.0			1.92							(E)	6.4A
	35x1	6.86E-03	15.0			1.78								
	785	6.450E-04	40.0			-2.13								
CHAIN	1012x1	1.15E-03	10.1			-0.68								
	1006x1	1.17E-03	10.1			-0.65								
	1014x1	2.28E-03	9.0			0.50								
172 ER	785	9.400E-06	40.0									9.400E-06		40.0
175 TB	85	8.000E-06	40.0									8.000E-06		40.0
177 LU	784	1.400E-06	40.0			-1.93				3.71	3.71	1.624E-06	(I)	33.7 >2
	785	6.600E-06	40.0			1.93							(E)	65.0A

TABLE 29 CHAIN AND CUMULATIVE YIELDS FROM FAST FISSION OF 238NP.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
131 XE	40877r1	326E+00	6.9				1.326E+00	6.9
132 XE	40877r2	843E+00	6.0				2.843E+00	6.0
134 XE	40877r7	670E+00	5.4				7.670E+00	5.4
135 XE	40877r5	718E+00	30.0				5.718E+00	30.0
136 XE	40877r6	172E+00	26.1				6.172E+00	26.1

TABLE 30 CHAIN AND CUMULATIVE YIELDS FROM FAST FISSION OF 238PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
87 BR	12926	8.40E-01	15.5					
137 I	12926	1.500E+00	26.7					

TABLE 31 CHAIN AND CUMULATIVE YIELDS FROM FAST FISSION OF 239PU.

A EL.	REF.	EXPERIMENTAL	NO.	YIELDS & SD	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	EXT./DF	MEAN	WEIGHTED	STANDARD
NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.
3 H	PI	92043P1	413E-02	15.9										
4 HE	PI	2057I2	0.028E-01	10.5	-0.01	0.00	0.00	2.029E-01	(I)	8.7A				
92043I2	0.030E-01	15.4	0.01											
77 AS	623	1.180E-02	12.0	-5.33										
624	2.900E-02	10.0	5.33											
83 CHAIN	871	3.090E-01	5.0	-1.43										
246	3.660E-01	10.0	1.43											
84 CHAIN	871	4.900E-01	5.0	-1.13										
246	5.590E-01	10.0	1.13											
85 KR(M)	40554	5.000E-01	12.0											
947	6.100E-01	10.0												
CHAIN	871	5.950E-01	7.0	-0.97										
246	6.720E-01	10.0	0.97											
86 CHAIN	871	7.770E-01	5.0	-1.09										
246	8.820E-01	10.0	1.09											
87 BR	12926	8.000E-01	6.2											
KR	897	1.100E-01		0.33										
947	9.600E-01	10.0	-0.56											
40554	9.600E-01	6.2	-1.03											
CHAIN	871	1.030E+00	5.0	0.50										
246	1.160E+00	10.0	1.35											
88 KR	947	1.360E+00	10.0	-0.33										
40554	1.620E+00	6.2	2.49											
SR	871	1.310E+00	5.0	-2.06										
CHAIN	246	1.440E+00	10.0	0.28										
89 KR	947	1.490E+00	10.0											
SR	1029I1	5.79E+00	3.8	-2.13										
104I1	6.94E+00	4.1	0.03											
1035I1	7.02E+00	4.1	0.15											
1042I1	7.39E+00	3.8	0.78											
13438	1.760E+00	10.0	0.39											
3	1.800E+00	11.0	0.55											
627	1.820E+00	7.0	1.03											
90 SR	13438	2.100E+00	10.0	-0.20										
12	2.120E+00	10.0	0.30											
627	3.350E+00	12.0W	2.49											
CHAIN	871	2.020E+00	5.0	-0.41										
1042I2	2.43E+00	10.0	0.83											
91 SR	40554	2.670E+00	5.2	0.90										
892	3.020E+00	25.0	0.60											
Y (G)	1029I2	2.236E+00	5.8											
Y (M)	40554	1.710E+00	3.5											
ZR	871	2.480E+00	5.0	-1.03										
CHAIN	246	2.580E+00	10.0	0.04										
92 SR	40554	2.930E+00	5.1											
Y	892	3.490E+00	25.0	0.53										
ZR	871	3.020E+00	5.0	-0.16										
CHAIN	246	3.020E+00	10.0	-0.04										
93 ZR	871	3.800E+00	5.0	-0.25										
CHAIN	246	3.910E+00	10.0	0.25										
94 ZR	871	4.280E+00	5.0	-0.23										
CHAIN	246	4.390E+00	10.0	0.23										
95 ZR	761	3.720E+00	8.0W	-2.45										

TABLE 31 CHAIN AND CUMULATIVE YIELDS FROM FAST FISSION OF 239PU. (CONT)

A EL.	REF.	EXPERIMENTAL	NO.	YIELDS & SD	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	EXT./DF	MEAN	WEIGHTED	STANDARD
NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.	NO.
96 ZR	871	4.840E+00	5.0	-0.48										
CHAIN	246	5.110E+00	10.0	0.48										
97 ZR	761	3.780E+00	8.0W	-2.50										
40554	4.700E+00	7.9	-0.64											
21707	5.020E+00	5.0	0.35											
880	5.120E+00	5.0	0.74											
884	5.150E+00	8.0	0.53											
624	5.270E+00	6.0	1.08											
346	5.500E+00	15.0	0.69											
627	5.610E+00	7.0	2.04											
40554	4.800E+00	1.9	4.800E+00	0.00	1.06									
40554	4.430E+00	2.3	4.430E+00	0.00	0.00									
871	5.330E+00	5.0	0.00											
CHAIN	1035I4	4.482E+00	3.0W4	9.35E+00	-2.50	1.82	0.48							
1022I4	7.45E+00	3.0	-1.49											
1030I4	9.17E+00	3.0	-0.14											
1024I4	9.99E+00	3.0	0.47											
40554	5.660E+00	5.0	-0.23											
871	5.660E+00	5.0	0.23											
CHAIN	246	5.810E+00	10.0	0.23										
627	5.780E+00	5.0	-0.30											
619	5.800E+00	6.0	-0.18											
63	5.900E+00	10.0	0.07											
21707	5.940E+00	3.0	0.64											
13438	6.110E+00	10.0	0.42											
346	6.240E+00	15.0	0.41											
871	6.640E+00	5.0	-0.16											
CHAIN	246	6.760E+00	10.0	0.16										
101 CHAIN	246	6.880E+00	10.0											
102 CHAIN	246	6.970E+00	10.0											
103 RU	761	4.990E+00	8.0W	-2.34										
65	5.920E+00	11.0	-0.64											
21763	6.000E+00	11.0	-0.52											
880	6.600E+00	6.0	-0.17											
703	6.780E+00	5.0	0.59											
884	7.010E+00	8.0	0.76											
791	7.050E+00	7.0	0.96											
30752	7.180E+00	4.0	2.27											
40554	5.200E+00	12.5												
CHAIN	246	6.770E+00	10.0											
105 RU	40554	5.300E+00	2.1	0.24										
892	5.680E+00	25.0	0.28											
21707	5.220E+00	4.9	-0.30											
21707	3.960E+00	6.5	-1.49											
65	4.780E+00	17.0	0.82											

TABLE 31 CHAIN AND CUMULATIVE YIELDS FROM FAST FISSION OF 239PU. (CONT)

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
157 EU	623	1.020E-01	8.0	-0.51	0.26	0.26	1.055E-01	(I)	4.2A
	624	1.070E-01	5.0	0.51				(E)	2.2
161 CHAIN	1042r6.777E-03	9.1	-0.44		0.19	0.19	6.951E-03	(I)	6.8A
	1041r7.200E-03	10.2	0.44					(E)	3.0

TABLE 32 CHAIN AND CUMULATIVE YIELDS FROM FAST FISSION OF 240PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
72 ZN	1117	1.160E-04	7.0					1.160E-04	7.0
83 KR	1135	2.270E-01	2.9					2.270E-01	2.9
84 KR	1135	3.900E-01	3.0					3.900E-01	3.0
95 CHAIN	1135	4.370E-01	4.1					4.370E-01	4.1
	1135	6.300E-01	3.0					6.300E-01	3.0
87 BR	12926	9.200E-01	14.1					8.630E-01	4.2
RB	1135	8.630E-01	4.2						
88 SR	1135	9.790E-01	4.3					9.790E-01	4.3
89 SR	1117	1.490E+00	11.0					1.490E+00	11.0
90 SR	1117	1.930E+00	7.0	0.84		0.70	0.70	1.824E+00	(I) 2.5A
CHAIN	1135	1.810E+00	2.7	-0.84					(E) 2.1
91 SR	1117	2.320E+00	7.0	0.54		0.99	0.50	2.238E+00	(I) 2.7A
Y	1117	2.350E+00	7.0	0.73					(E) 1.9
ZR	1135	2.200E+00	3.3	-0.99					
92 ZR	1135	2.690E+00	3.3					2.690E+00	3.3
93 Y	1117	3.980E+00	7.0	1.49		2.22	2.22	3.597E+00	(I) 3.0 >2
ZR	1135	3.530E+00	3.3	-1.49					(E) 4.5A
94 ZR	1135	3.950E+00	3.2					3.950E+00	3.2
95 ZR	1117	4.490E+00	7.0	0.06		0.00	0.00	4.474E+00	(I) 3.1A
MO	1135	4.470E+00	3.5	-0.06					(E) 0.2
96 ZR	1135	4.760E+00	3.3					4.760E+00	3.3
97 ZR	1117	5.280E+00	7.0	0.19		0.04	0.04	5.216E+00	(I) 3.1A
MO	1135	5.200E+00	3.5	-0.19					(E) 0.6
98 MO	1135	5.540E+00	3.7					5.540E+00	3.7
99 MO	1117	6.180E+00	7.0					6.180E+00	7.0
100 MO	1135	6.860E+00	3.5					6.860E+00	3.5
101 RU	1135	6.620E+00	5.8					6.620E+00	5.8
102 RU	1135	6.820E+00	5.8					6.820E+00	5.8
103 RU	1117	7.090E+00	7.0					7.090E+00	7.0
104 RU	1135	7.030E+00	5.8					7.030E+00	5.8
105 RH	1117	5.740E+00	7.0					5.740E+00	7.0
106 RU	1135	5.120E+00	7.0	-0.44		0.19	0.19	5.228E+00	(I) 5.0A
	1135	5.120E+00	7.0	0.44					(E) 2.2
109 PD	1117	1.800E+00	9.0					1.800E+00	9.0
111 AG(G)	1117	5.010E-01	7.0					5.010E-01	7.0
112 AG	1117	2.340E-01	7.0					2.340E-01	7.0
113 AG(G)	1117	1.590E-01	14.0					1.590E-01	14.0
115 CD(G)	1117	6.100E-02	7.0	6.100E-02		0.00	0.00	6.504E-02	(I) 6.6A
CD(M)	1117	4.040E-03	7.0	4.040E-03					(E) 0.0
125 SB	1135	8.900E-02	12.4	0.46		0.21	0.21	8.610E-02	(I) 10.6A
CHAIN	21155	8.000E-02	20.0	-0.46					(E) 4.9
126 CHAIN	21155	2.150E-01	20.0					2.150E-01	20.0
127 SB	1117	4.470E-01	7.0	0.30		0.09	0.09	4.437E-01	(I) 6.6A
CHAIN	21155	4.200E-01	20.0	-0.30					(E) 2.0

TABLE 33 CHAIN AND CUMULATIVE YIELDS FROM FAST FISSION OF 241PU.

(CONT.)

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT. EXT./DF	MEAN	DEVIATION		
150 ND	1071 1.190E+00 3.0	-0.60	0.49	0.16	1.202E+00 (I)	2.5A		
	22050r1.227E+00 10.5	0.20			(E) 1.0			
CHAIN	21155 1.150E+00 20.0	-0.23						
	1182 1.235E+00 5.0	0.61						
151 SN	1071 9.140E-01 3.0	0.17	0.03	0.02	9.116E-01 (I)	2.6A		
CHAIN	21155 8.950E-01 20.0	-0.09						
	1182 9.060E-01 5.0	-0.14						
152 SM	1071 7.050E-01 3.0	-0.69	0.50	0.25	7.124E-01 (I)	2.6A		
CHAIN	21155 7.100E-01 20.0	-0.02						
	1182 7.350E-01 5.0	0.71						
154 SM	1071 3.700E-01 3.0	-0.36	0.13	0.13	3.721E-01 (I)	2.6A		
CHAIN	1182 3.780E-01 5.0	0.36						

TABLE 34 CHAIN AND CUMULATIVE YIELDS FROM FAST FISSION OF 242PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT. EXT./DF	MEAN	DEVIATION		
83 KR	1134 1.790E-01 5.0				1.790E-01	5.0		
84 KR	1134 3.440E-01 5.0				3.440E-01	5.0		
85 KR(M)	40678 3.700E-01 10.8				3.230E-01	20.0		
CHAIN	1134 3.230E-01 20.0							
86 KR	1134 5.420E-01 5.0				5.420E-01	5.0		
87 BR	12926 8.000E-01 16.3				6.230E-01	5.0		
KR	40678 1.470E+00 15.6							
RB	1134 6.230E-01 5.0							
88 KR	40678 7.700E-01 13.0	-0.61			0.37	0.37	8.262E-01 (I)	4.7A
SR	1134 8.360E-01 5.0	0.61						
90 CHAIN	1134 1.630E+00 5.0						1.630E+00	5.0
91 SR	40678 1.770E+00 7.9	-0.24			0.06	0.06	1.799E+00 (I)	4.0A
ZR	1134 1.810E+00 4.7	0.24						
92 ZR	40678 1.930E+00 5.7				0.01	0.01	2.176E+00 (I)	4.3A
Y	40678 2.150E+00 11.6	-0.11						
ZR	1134 2.180E+00 4.6	0.11						
93 Y	40678 3.320E+00 18.1	0.81			0.66	0.66	2.842E+00 (I)	4.5A
ZR	1134 2.820E+00 4.6	-0.81						
94 ZR	1134 3.130E+00 4.6						3.130E+00	4.6
95 ZR	40678 3.240E+00 11.7	-0.99			0.98	0.98	3.600E+00 (I)	2.9A
MO	1134 3.630E+00 3.0	0.99						
96 ZR	1134 4.290E+00 4.6						4.290E+00	4.6
97 ZR	40678 4.780E+00 6.7	0.96			0.92	0.92	4.496E+00 (I)	2.7A
MO	1134 4.450E+00 2.9	-0.96						
98 MO	1134 4.840E+00 2.9						4.840E+00	2.9
100 MO	1134 6.100E+00 3.0						6.100E+00	3.0
101 RU	1134 6.030E+00 7.6						6.030E+00	7.6
102 RU	1134 6.480E+00 7.6						6.480E+00	7.6
104 TC	40678 5.520E+00 10.0						6.840E+00	7.5
RU	1134 6.840E+00 7.5							
105 RU	40678 6.920E+00 6.2							
RH	40678 7.480E+00 6.3							
106 RU	1134 5.810E+00 7.6						5.810E+00	7.6
125 SB	1134 5.500E-02 13.0	-0.36			0.13	0.13	5.631E-02 (I)	10.9A
CHAIN	21155 6.000E-02 20.0	0.36						
126 CHAIN	21155 1.750E-01 20.0						1.750E-01	20.0
127 CHAIN	21155 3.400E-01 20.0						3.400E-01	20.0
128 SN	40678 6.300E-01 65.1	0.21			0.05	0.05	5.458E-01 (I)	19.1A
CHAIN	21155 5.400E-01 20.0	-0.21						
129 SB	40678 2.230E+00 33.2	1.51			2.27	2.27	1.159E+00 (I)	17.7 >2
CHAIN	21155 1.070E+00 20.0	-1.51						
130 SB(M)	40678 7.100E-01 9.9						1.920E+00	20.0
CHAIN	21155 1.920E+00 20.0							
131 TE(M)	40678 4.100E-01 14.6				0.20	0.10	3.105E+00 (I)	2.6A

TABLE 34 CHAIN AND CUMULATIVE YIELDS FROM FAST FISSION OF 242PU. (CONT.)

A EL. NO.	REF. NO.	EXPERIMENTAL YIELDS & SD	MEAN R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD DEVIATION
			COMPONENT VALUE	EXTERNAL	INT. EXT./DF	MEAN	
I	40678	3.190E+00	6.6			0.44	(E) 0.8
XE	1134	3.090E+00	2.8			-0.45	
CHAIN	21155	3.160E+00	20.0			0.09	
132 I	40678	4.640E+00	8.2			0.38	(E) 2.6A
XE	1134	4.490E+00	2.8			-0.31	(E) 0.7
CHAIN	21155	4.410E+00	20.0			-0.11	
133 I	40678	7.040E+00	6.0			0.47	(E) 2.4A
CS	1134	6.830E+00	2.7			-0.35	(E) 1.0
CHAIN	21155	6.460E+00	20.0			-0.31	
134 I	40678	6.750E+00	11.6			-0.75	(E) 2.4A
I	40678	6.830E+00	5.6			-1.45	(E) 2.4
XE	1134	7.500E+00	2.7			1.70	
CHAIN	21155	7.290E+00	20.0			-0.02	
135 I	40678	6.830E+00	5.6			-0.37	(E) 2.2A
XE	40678	6.990E+00	5.9			0.08	(E) 0.5
CS	1134	6.980E+00	2.6			0.21	
CHAIN	21155	7.080E+00	20.0			0.09	
136 XE	1134	6.920E+00	2.7			0.16	(E) 2.7A
CHAIN	21155	6.700E+00	20.0			-0.16	(E) 0.4
137 I	12926	3.500E+00	45.7			0.00	(E) 2.7A
CHAIN	21155	6.310E+00	20.0			-0.02	(E) 0.1
138 BA	1134	6.220E+00	3.1			-0.02	(E) 3.1A
CHAIN	21155	6.250E+00	20.0			0.02	(E) 0.1
139 BA	40678	5.870E+00	6.3			-0.46	(E) 3.3A
LA	1134	6.070E+00	4.0			0.42	(E) 1.1
CHAIN	21155	6.080E+00	20.0			0.06	
140 BA	40678	6.700E+00	10.3			1.53	(E) 2.9
LA	40678	6.490E+00	12.0			1.07	(E) 3.3A
CE	1134	5.560E+00	3.2			-1.81	
CHAIN	21155	5.780E+00	20.0			0.09	
141 CHAIN	21155	5.260E+00	20.0			5.260E+00	20.0
142 LA	40678	4.630E+00	8.0			-0.03	(E) 2.9A
CE	1134	4.640E+00	3.2			0.02	(E) 0.1
CHAIN	21155	4.660E+00	20.0			0.02	
143 CE	40678	3.950E+00	7.6			0.01	(E) 2.7A
ND	1134	4.600E+00	2.7			0.11	(E) 0.3
CHAIN	21155	4.500E+00	20.0			-0.11	
144 CHAIN	21155	4.160E+00	20.0			0.02	(E) 2.7A
1134	4.280E+00	2.7				0.14	(E) 0.4
145 ND	1134	3.410E+00	2.7			0.10	(E) 2.7A
CHAIN	21155	3.340E+00	20.0			-0.10	(E) 0.3
146 ND	1134	2.920E+00	2.7			0.07	(E) 2.7A
CHAIN	21155	2.880E+00	20.0			-0.07	(E) 0.2

TABLE 34 CHAIN AND CUMULATIVE YIELDS FROM FAST FISSION OF 242PU. (CONT.)

A EL. NO.	REF. NO.	EXPERIMENTAL YIELDS & SD	MEAN R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD DEVIATION
			COMPONENT VALUE	EXTERNAL	INT. EXT./DF	MEAN	
147 SM	1134	2.380E+00	2.7			0.00	(E) 2.7A
CHAIN	21155	2.380E+00	20.0			0.00	(E) 0.0
148 ND	1134	2.020E+00	2.8			0.10	(E) 2.8A
CHAIN	21155	1.960E+00	20.0			-0.10	(E) 0.3
149 ND	40678	1.510E+00	9.3			-0.58	(E) 4.3A
SM	1134	1.600E+00	5.0			0.46	(E) 1.8
CHAIN	21155	1.640E+00	20.0			0.19	
150 ND	1134	3.410E+00	20.0			3.08	(E) 4.9
CHAIN	21155	1.300E+00	5.0			-3.08	(E) 15.1A
151 SM	1134	9.970E-01	5.0			-0.11	(E) 4.9A
CHAIN	21155	1.020E+00	20.0			0.11	(E) 0.5
152 SM	1134	7.700E-01	5.0			-0.43	(E) 4.9A
CHAIN	21155	8.450E-01	20.0			0.43	(E) 2.1
154 SM	1134	4.300E-01	5.0			4.300E-01	5.0

TABLE 36 CHAIN AND CUMULATIVE YIELDS FROM PAST FISSION OF 242M.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
87 BR	12926	7.100E+01	7.0						
137 I	12926	2.400E+00	12.5						

TABLE 37 CHAIN AND CUMULATIVE YIELDS FROM PAST FISSION OF 243CM.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
95 ZR	2061	3.220E+00	1.0					3.220E+00	1.0
125 SB	2061	2.150E-01	1.2					2.150E-01	1.2
137 CS	2061	6.760E+00	1.0					6.760E+00	1.0
141 CE	2061	4.840E+00	1.1					4.840E+00	1.1
144 CE	2061	3.700E+00	1.1					3.700E+00	1.1

TABLE 38 CHAIN AND CUMULATIVE YIELDS FROM FAST FISSION OF 244CM.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	VALUE	EXT.	INT.	EXT./DF	DEVIATION
95 ZR	2061	3.000E+00	1.0					1.0
125 SB	2061	1.800E-01	1.3					1.3
137 CS	2061	6.680E+00	1.0					1.0
141 CB	2061	5.960E+00	1.3					1.3
144 CE	2061	4.020E+00	1.0					1.0
155 EU	2061	5.330E-01	1.5					1.5

TABLE 39 CHAIN AND CUMULATIVE YIELDS FROM FAST FISSION OF 245CM.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	VALUE	EXT.	INT.	EXT./DF	DEVIATION
87 BR	12926	5.100E-01	7.8					7.8
137 I	12926	2.200E+00	13.6					13.6

TABLE 40 CHAIN AND CUMULATIVE YIELDS FROM FAST FISSION OF 246CM.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT. EXT./DF	INT. EXT./DF	DEVIATION
95 ZR	2061	2.290E+00	1.1					1.1
125 SB	2061	1.160E-01	1.5					1.5
137 CS	2061	6.520E+00	1.1					1.1
141 CE	2061	5.940E+00	1.2					1.2
144 CE	2061	4.710E+00	1.2					1.2
155 EU	2061	7.060E-01	1.5					1.5

TABLE 41 CHAIN AND CUMULATIVE YIELDS FROM FAST FISSION OF 248CM.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT. EXT./DF	INT. EXT./DF	DEVIATION
95 ZR	2061	2.060E+00	1.0					1.0
125 SB	2061	8.760E-02	1.3					1.3
137 CS	2061	6.360E+00	1.0					1.0
141 CE	2061	6.650E+00	1.0					1.0
144 CE	2061	5.080E+00	1.2					1.2
155 EU	2061	7.430E-01	1.4					1.4

TABLE 42 CHAIN AND CUMULATIVE YIELDS FROM PAST FISSION OF 249CF.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
87 BR	12926	3.000E+01	10.0						
137 I	12926	1.250E+00	13.6						

TABLE 43 CHAIN AND CUMULATIVE YIELDS FROM PAST FISSION OF 252CF.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
137 I	12926	3.000E+00	10.0						
A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
87 BR	77500	6.540E+00	8.7					6.540E+00	8.7
91 SR	77500	7.950E+00	5.5					7.950E+00	5.5
92 RB	77500	6.540E+00	6.3					6.540E+00	6.3
97 Y (G)	77500	2.930E+00	5.8	-0.84			0.70	0.70 3.022E+00 (I)	4.3A
ZR	77500	3.150E+00	6.3	0.84					(E) 3.6
99 NB	77500	1.910E+00	5.8	-1.09			1.19	1.19 1.995E+00 (I)	3.9
MO	77500	2.080E+00	5.2	1.09					(E) 4.3A
132 SB(G)	77500	1.590E+00	10.1	-2.81			7.89	7.89 1.971E+00 (I)	4.3 >2
TE	77500	2.120E+00	4.7	2.81					(E) 12.1A
133 TE	77500	3.760E+00	5.9					3.760E+00	5.9
134 TE	77500	4.410E+00	6.8					4.410E+00	6.8
142 BA	77500	8.260E+00	5.2					8.260E+00	5.2
143 LA	77500	7.600E+00	4.2					7.600E+00	4.2
A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
125 CHAIN	2099	2.900E-01	20.0					2.900E-01	20.0
127 CHAIN	2099	4.400E-01	10.0					4.400E-01	10.0

TABLE 46 CHAIN AND CUMULATIVE YIELDS FROM HIGH ENERGY FISSION OF ^{232}Th .

[illegible]

TABLE 46 CHAIN AND CUMULATIVE YIELDS FROM HIGH ENERGY FISSION OF ^{232}Th .

A. EL. NO.	REF. NO.	EXPERIMENTAL YIELDS & SD.	MEAN COMPONENT VALUE	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	INT. EXT./DF	WEIGHTED MEAN	STANDARD DEVIATION
159 GD	348	4.400E-03	10.0							4.400E-03	10.0
161 TB	348	1.060E-03	5.0							1.060E-03	5.0
166 DY	348	2.900E-05	7.0								
169 FR	348	2.300E-05	35.0								

TABLE 47 CHAIN AND CUMULATIVE YIELDS FROM HIGH ENERGY FISSION OF 231PA.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
84 BR	645	2.780E+00	5.0				2.780E+00	5.0
91 SR	645	5.560E+00	6.0				5.560E+00	6.0
93 Y	645	6.630E+00	5.0				6.630E+00	5.0
97 ZR	645	4.290E+00	5.0				4.290E+00	5.0
105 RU	645	1.310E+00	7.0				1.310E+00	7.0
113 AG	645	2.050E+00	8.0				2.050E+00	8.0
129 SB	645	2.460E+00	5.0				2.460E+00	5.0
131 I	645	3.370E+00	10.0				3.370E+00	10.0
132 TE	645	4.880E+00	5.0	0.47	0.22	0.22	4.797E+00 (I)	3.5A
I	645	4.720E+00	5.0	-0.47				(E) 1.7
133 I	169	5.740E+00	5.0	-1.09	1.19	1.19	5.952E+00 (I)	3.5
XE	169	6.200E+00	5.0					(E) 3.9A
134 I	169	9.180E+00	5.0	1.09			9.180E+00	5.0
135 XE	169	6.500E+00	6.0				6.500E+00	6.0
143 CE	645	3.000E+00	35.0				3.000E+00	35.0

TABLE 48 CHAIN AND CUMULATIVE YIELDS FROM HIGH ENERGY FISSION OF 233U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
1 H PI	2065	9.018E-03	41.4				9.018E-03	41.4
3 H PI	2065	2.480E-02	22.6				2.480E-02	22.6
4 HE PI	2065	1.957E-01	10.6				1.957E-01	10.6
66 NI	565	7.178E-04	13.0				7.178E-04	13.0
67 CU	565	1.657E-03	13.9				1.657E-03	13.9
72 ZN	565	1.364E-02	7.1				1.364E-02	7.1
83 BR	71	1.330E+00	7.0				1.330E+00	7.0
84 BR	71	2.020E+00	5.0					
85 KR (M)	934	1.860E+00	19.0					
87 KR	934	3.330E+00	20.0				3.330E+00	20.0
88 KR	934	4.250E+00	7.0				4.250E+00	7.0
89 SR	71	4.820E+00	11.0				4.820E+00	11.0
91 SR	655	4.200E+00	13.0	-1.61	4.99	2.49	5.009E+00 (I)	4.3 >2
	934	5.60E+00	7.0	0.94				(E) 6.8A
	71	5.60E+00	7.0					
92 SR	934	4.570E+00	7.0	-2.24			5.04 5.04 5.018E+00 (I)	5.0 >2
	71	5.720E+00	7.0	2.24				(E) 11.2A
93 Y	934	5.50E+00	12.0	-0.43			0.19 0.19 5.760E+00 (I)	5.8A
	934	5.50E+00	12.0	0.43				(E) 7.0
95 ZR	934	4.990E+00	10.0	-0.32			0.16 0.08 5.133E+00 (I)	4.2A
	21708	5.130E+00	5.5	-0.01				(E) 1.2
	565	5.257E+00	8.6	0.31				
97 ZR	934	4.850E+00	11.0	0.00			0.00 0.00 4.850E+00 (I)	5.8A
	21708	4.850E+00	5.7	0.00				(E) 0.0
99*MO	62	3.500E+00	9.0	-1.48			7.60 1.90 3.925E+00 (I)	3.3
	71	3.640E+00	6.0	-1.63				(E) 4.5A
	565	3.841E+00	12.1	-0.19				
	21708	4.400E+00	5.0W	2.36				
103 RU	62	2.310E+00	13.0	-1.49			2.24 1.12 2.718E+00 (I)	4.6
	934	2.760E+00	12.0	0.14				(E) 4.8A
	21708	2.810E+00	5.3	1.11				
105 RU	71	1.630E+00	12.0	-1.45			2.21 1.11 1.840E+00 (I)	7.1
	934	1.940E+00	14.0	0.42				(E) 7.5A
RH	565	2.062E+00	11.2	1.16				
106 RU	62	1.520E+00	14.0				1.520E+00	14.0
109 PD	71	1.200E+00	20.0	-1.50			2.26 2.26 1.477E+00 (I)	10.4 >2
	877	1.670E+00	12.0	1.50				(E) 15.7A
111 AG	71	1.210E+00	13.0	-1.03			6.21 2.07 1.349E+00 (I)	6.0 >2
	82	1.220E+00	10.0	-1.40				(E) 8.6A
	565	1.657E+00	18.7	1.03				
112*PD	565	1.769E+00	7.8	1.07			7.27 1.82 1.642E+00 (I)	4.2
	877	1.770E+00	6.0	1.65				(E) 5.6A
	655	1.800E+00	15.0	0.61				
AG	71	1.080E+00	15.0W	-2.22				
	934	1.710E+00	13.0	0.32				
113*AG	71	1.060E+00	11.0W	-1.59			8.73 4.37 1.313E+00 (I)	6.7 >2
	877	1.580E+00	10.0	2.37				(E) 14.0A
	934	1.840E+00	14.0	2.26				
115 AG	71	1.030E+00	13.0	-1.51			8.54 2.14 1.196E+00 (I)	6.4 >2
CD (G)	877	1.450E+00	10.0	2.07				(E) 9.4A
	62	9.800E-01	20.0	-1.20				
CHAIN	565	1.567E+00	15.8	-0.74				
	565	1.567E+00	15.8	1.58				
121 SN	71	1.060E+00	7.0	-2.14			4.58 4.58 1.091E+00 (I)	6.7 >2
	877	1.880E+00	20.0	2.14				(E) 14.3A

TABLE 48 CHAIN AND CUMULATIVE YIELDS FROM HIGH ENERGY FISSION OF 233U .

(CONT.)

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXT.	INT.	EXT./DF	INT.	EXT./DF	MEAN	DEVIATION
125 SN	71	1.510E+00	6.0							1.510E+00	6.0
127 SB	655	1.730E+00	15.0	-1.73		3.36	1.12	2.145E+00	(I)	4.6	(E) 4.9A
	934	2.160E+00	11.0	0.07							
	877	2.200E+00	6.0	0.62							
	877	2.370E+00	12.0	0.84							
131 I	71	3.400E+00	8.0	-3.36		11.27	11.27	4.078E+00	(I)	4.5	>2
	21708	4.630E+00	5.3	3.36						15.0A	
132 TE	21708	3.140E+00	5.3			0.15	0.15	3.689E+00	(I)	7.1A	(E) 2.8
	565r3.238E+00	13.9									
	62	3.980E+00	9.0								
I	655	3.700E+00	15.0	-0.39							
	71	3.950E+00	8.0	0.39							
133 I	655	4.40E+00	15.0	0.11		0.01	0.01	4.377E+00	(I)	7.8A	(E) 0.8
	655	4.440E+00	15.0								
134 I	71	4.650E+00	6.0					4.650E+00		6.0	
135 I	71	4.960E+00	8.0					4.960E+00		8.0	
XE	21708	3.460E+00	7.0								
136 CS	21708	8.370E-01	6.0								
137 CS	62	4.700E+00	11.0	-0.67		0.45	0.45	4.962E+00	(I)	6.8A	(E) 4.5
	565r5.156E+00	8.6		0.67							
139 BA	71	5.790E+00	5.0					5.790E+00		5.0	
140 BA	565r4.054E+00	15.8		-1.12							
	21708	4.390E+00	10.0	-0.93							
	875	5.320E+00	11.0	1.23							
	875	5.320E+00	11.0	1.23							
141 CE	21708	4.240E+00	6.1	-1.26		2.85	0.95	4.489E+00	(I)	3.7A	(E) 3.6
	565r4.245E+00	11.2		-0.55							
	934	4.710E+00	6.0	0.97							
	62	5.000E+00	10.0	1.08							
143 CE	934	3.140E+00	6.0	-0.29		0.27	0.14	3.183E+00	(I)	3.7A	(E) 1.3
	21708	3.170E+00	5.5	-0.10							
	565r3.315E+00	8.6		0.51							
144 CE	21708	2.430E+00	8.0								
	565r2.516E+00	13.0									
147 ND	934	1.130E+00	20.0	-0.61		1.12	0.56	1.261E+00	(I)	5.0A	(E) 3.8
	565r1.203E+00	8.6		-0.71							
	21708	1.320E+00	6.5	1.02							
151 PM	934	5.200E-01	17.0					5.200E-01		17.0	
153 SM	565r1.455E-01	11.2		0.11				1.455E-01		11.2	
156 EU	565r4.447E-02	7.8						4.447E-02		7.8	
159 GD	565r1.082E-02	13.0						1.082E-02		13.0	
	565r4.751E-03	8.6						4.751E-03		8.6	
161 TB	565r2.426E-04	15.8						2.426E-04		15.8	
166 DY	565r8.492E-05	8.6						8.492E-05		8.6	
169 ER	565r1.829E-05	9.5						1.829E-05		9.5	
172 ER	565r1.921E-06	16.8						1.921E-06		16.8	

TABLE 49 CHAIN AND CUMULATIVE YIELDS FROM HIGH ENERGY FISSION OF 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXT.	INT.	EXT./DF	INT.	EXT./DF	MEAN	DEVIATION
1 H PI	2065r6.335E-03	40.4								6.335E-03	40.4
3 H PI	2065r1.742E-02	20.7								1.742E-02	20.7
4 HE PI	2050	1.456E-01	40.0	-0.37		0.29	0.15	1.667E-01	(I)	5.3A	(E) 2.0
	2065r1.614E-01	10.6		0.46							
	2052r1.694E-01	6.2									
66 NI	349	2.800E-04	10.0	-2.46		6.04	6.04	3.195E-04	(I)	7.2	>2
	403	4.000E-04	10.0	2.46						17.6A	(E) 14.0
67 CU	349	6.500E-04	14.0							6.500E-04	14.0
72 ZN	1309r1.785E-03	34.8W		-49		5.27	2.63	1.653E-03	(E)	7.6A	>2
	349	6.300E-03	5.0W	0.65							
	403	7.800E-03	10.0W	0.97							
73 GA	403	1.150E-02	10.0							1.150E-02	10.0
74 AS	403	6.800E-02	10.0							6.800E-02	10.0
81 SE(G)	403	3.000E-01	10.0								
SE(M)	403	5.100E-02	10.0								
83 BR	403	8.300E-01	10.0							1.154E+00	4.8
CHAIN	987r1.154E+00	4.8									
84 BR(G)	403	1.030E+00	10.0								
85 KR(M)	943	1.840E+00	10.0								
87 KR	943	2.670E+00	10.0							2.670E+00	10.0
88 KR	943	3.760E+00	10.0							3.760E+00	10.0
89 KR	943	4.040E+00	10.0	-0.15		6.80	0.97	4.099E+00	(I)	1.7A	(E) 1.6
SR	1309r1.3.805E+00	6.1		-1.33							
	102r3.962E+00	3.6		-1.10							
	162	4.200E+00	10.0	0.24							
	203r4.268E+00	3.6		1.24							
	280	4.450E+00	10.0	0.80							
CHAIN	985r3.987E+00	3.7		-0.86							
	987r4.307E+00	3.7		1.46							
90 SR	5	4.400E+00	5.0	-0.65		1.02	0.51	4.527E+00	(I)	2.2A	(E) 1.6
CHAIN	986r4.477E+00	3.5		-0.41							
	986r4.652E+00	3.5		0.97							
91 SR	203r4.613E+00	3.9		-0.03		1.60	0.53	4.618E+00	(I)	2.5A	(E) 1.8
	987r4.656E+00	4.2		0.24							
	280	4.960E+00	8.0	0.90							
Y (G)	1309r1.4.348E+00	6.9		-0.98							
93 Y	349	5.400E+00	10.0							5.400E+00	10.0
95 ZR	162	4.300E+00	10.0	-2.03		5.13	1.71	5.129E+00	(I)	2.6	3.4A
	130r5.010E+00	5.0		-0.56							
	21708	5.330E+00	3.8	1.32							
97 ZR	162	4.400E+00	10.0	-1.91		8.60	2.15	5.195E+00	(I)	2.6	>2
	21708	5.030E+00	5.0	-0.79							
	1309r5.032E+00	6.1		-0.60							
	280	6.000E+00	5.0W	2.32							
CHAIN	987r5.151E+00	5.7		-0.17							
99 MO	617	5.010E+00	3.0	-0.61		1.88	0.63	5.072E+00	(I)	2.2A	(E) 1.7
	21708	5.050E+00	3.8	-0.14							
	162	5.650E+00	8.0	1.52							
103 RU	21708	3.080E+00	4.1	-1.71		3.44	1.72	3.208E+00	(I)	3.2	4.2A
	162	3.250E+00	10.0	0.14							
CHAIN	987r3.524E+00	5.8		1.79							
105 RU	280	1.450E+00	7.0W	-2.43		8.82	4.41	1.783E+00	(I)	3.4	>2
	162	2.950E+00	10.0W	2.49							
CHAIN	987r1.895E+00	4.1W		0.66							

TABLE 49 CHAIN AND CUMULATIVE YIELDS FROM HIGH ENERGY FISSION OF 235U .

(CONT.)

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION				
106 RU	162 2.300E+00 12.0	2.27	5.16	5.16	1.695E+00 (I)	4.3	>2				
CHAIN	987r1.650E+00 4.6	-2.27				(E)	9.7A				
109 PD	203r1.436E+00 9.2	1.48	2.24	1.12	1.265E+00 (I)	5.1					
PD(G)	1309i1.188E+00 12.0	-0.60				(E)	5.4A				
CHAIN	987r1.220E+00 7.0	-0.78									
111 AG	162 1.050E+00 10.0	-1.52	4.70	0.94	1.205E+00 (I)	2.0A					
	280 1.140E+00 5.0	-1.26				(E)	2.0				
	203r1.248E+00 4.2	0.93									
CHAIN	985r1.216E+00 5.0	0.20									
	987r1.247E+00 5.0	0.74									
112 PD	1309r3.974E-01 12.3	-1.36	7.15	3.57	7.962E-01 (I)	5	>2				
	203r6.995E-01 12.3					(E)	10.1A				
CHAIN	987r9.215E-01 6.5W	1.91									
113 AG	280 1.140E+00 10.0					1.140E+00	10.0				
115*CD(G)	280 1.610E+00 5.0W9.126E-01 2.26 1.44										
	102r8.783E-01 6.9	-1.01									
	1309i1r8.870E-01 8.2	-0.51									
	162 9.500E-01 10.0	0.48									
	331 9.800E-01 15.0	0.49									
CD(M)	162 6.100E-02 15.0 6.514E-02 0.70 0.15										
	102r6.550E-02 9.1	0.10									
	203r6.715E-02 9.1	0.54									
	331 6.900E-05 15.0W	-0.01									
121 AG	128i3 1.520E-01 122.0		0.00	0.00	1.141E+00 (I)	9.7A					
SN(G)	162 1.100E+00 10.0 1.100E+00					(E)	0.0				
SN(M)	203r1.809E-01 29.8 1.809E-01										
123 IN	128i3 1.130E+00 21.2										
125 SN(M)	203r1.112E+00 6.5										
126 CHAIN	987r1.873E+00 10.2					1.873E+00	10.2				
127 SB	21708 1.760E+00 7.5					2.056E+00	5.6				
	203r1.900E+00 7.1										
CHAIN	987r2.056E+00 5.6										
129 SB	203r1.330E+00 12.5					1.582E+00	5.3				
TE	162 1.580E+00 8.0										
CHAIN	987r1.582E+00 5.3										
131 I	203r3.796E+00 4.5	-1.50	7.18	1.80	4.024E+00 (I)	2.0					
	395r4.127E+00 5.8	0.46				(E)	2.7A				
	280 4.230E+00 6.0	1.09									
	21708 4.320E+00 4.0	1.94									
CHAIN	987r3.872E+00 3.5	-1.36									
132 TE	203r4.134E+00 6.0	-1.08	15.15	2.52	4.384E+00 (I)	2.0	>2				
	21708 4.140E+00 5.0	-1.31				(E)	3.2A				
	395r4.213E+00 6.0	-0.73									
I	395r4.832E+00 3.9W	2.42									
XE	1111 4.920E+00 5.0	2.34									
CHAIN	987r4.030E+00 5.7	-1.67									
133 I	21708 5.430E+00 5.0					5.430E+00	5.0				
134 I	395r3.640E+00 15.5					5.580E+00	5.0				
XE	1111 5.580E+00 5.0										
135 XE	21708 4.970E+00 6.4										
136 XE	1111 5.080E+00 5.0					5.080E+00	5.0				

(CONT.)

TABLE 49 CHAIN AND CUMULATIVE YIELDS FROM HIGH ENERGY FISSION OF 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION				
CS	21708 2.160E-01 9.0										
137 XE	943 4.450E+00 10.0	-1.96	3.85	3.85	4.976E+00 (I)	7.1	>2				
CS	162 5.900E+00 10.0	1.96				(E)	14.0A				
138 XE	943 3.670E+00 10.0										
139 CHAIN	987r4.701E+00 4.1					4.701E+00	4.1				
140*BA	162 4.200E+00 7.0	-0.82	13.86	1.54	4.435E+00 (I)	1.2					
	349 4.250E+00 5.0	-0.91									
	203r4.530E+00 4.2	0.53									
	102r4.586E+00 3.1	1.19									
	21708 4.610E+00 4.2	0.95									
	1309i1r5.037E+00 5.8	2.11									
CHAIN	987r4.051E+00 2.9W	-2.17									
	987r4.524E+00 3.1	0.70									
	985r4.596E+00 3.1	1.24									
141 CE	162 3.800E+00 10.0	-1.73	2.99	1.49	4.409E+00 (I)	3.2					
	21708 4.500E+00 4.0	0.82				(E)	3.9A				
	1309i1r4.527E+00 6.4	0.47									
143 CE	21708 3.750E+00 4.1										
	203r3.758E+00 4.3										
	102r3.795E+00 3.9										
CHAIN	985r3.867E+00 2.9										
144*CE	203r2.978E+00 5.1	-1.15	7.69	1.54	3.148E+00 (I)	0.9					
	102r3.087E+00 4.2	-0.49				(E)	1.1A				
	21708 3.150E+00 1.0	0.13									
	1309i1r3.843E+00 6.5W	2.49									
CHAIN	987r3.124E+00 5.2	-0.15									
	985r3.127E+00 5.2	-0.13									
147 ND	21708 1.620E+00 4.8	-0.28	1.16	0.29	1.639E+00 (I)	2.2A					
	349 1.640E+00 7.0	0.01				(E)	1.2				
	102r1.665E+00 4.0	0.45									
	1309i1r1.722E+00 6.3	0.80									
CHAIN	985r1.601E+00 3.9	-0.73									
148*CHAIN	1183r1.175E+00 5.5W	2.35	9.89	3.30	5.861E-01 (I)	2.9	>2				
	1183r4.327E-01 5.5W	-1.17				(E)	5.3A				
	1183r8.162E-01 5.5W	1.26									
	1183r8.162E-01 5.5W	1.26									
153 SM	349 2.200E-01 10.0	-0.50	0.25	0.25	2.287E-01 (I)	5.9A					
	1309i1r2.338E-01 7.2	0.50				(E)	2.9				
156 EU	102r5.136E-02 5.8	-0.37	1.54	0.39	5.228E-02 (I)	2.1A					
	102r5.136E-02 5.8	0.41				(E)	1.3				
CHAIN	987r5.116E-02 3.5	-0.80									
	985r5.391E-02 3.5	1.07									
159 CH	349 1.270E-02 10.0										
161 TB	102r4.450E-03 9.2	-1.56	8.39	2.80	4.979E-03 (I)	4.6	>2				
	349 5.600E-03 7.0	1.96				(E)	7.7A				
	1309i1r6.318E-03 13.2	1.67									
CHAIN	985r4.403E-03 10.2	-1.48									
166 DY	349 2.800E-04 7.0					2.800E-04	7.0				
169 ER	349 8.000E-05 8.0					8.000E-05	8.0				
172 ER	349 1.800E-05 11.0					1.800E-05	11.0				

TABLE 50 CHAIN AND CUMULATIVE YIELDS FROM HIGH ENERGY FISSION OF 238U . (CONT)

A EL.	REF.	EXPERIMENTAL	NO.	YIELDS & SD	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	INT.	EXT./DF	MEAN	DEVIATION
NO.															
136 XE			639	5.650E+00	7.0	-0.18		0.03	0.03	5.709E+00	(I)	4.1A			
CHAIN			363	5.740E+00	5.0	0.18									
137 XE			945	4.630E+00	10.0			5.01	1.67	5.365E+00	(I)	4.0			
CS			30639	5.210E+00	6.9	-0.53									
CHAIN			164	6.600E+00	9.0	2.23									
138 XE			30639	5.210E+00	10.0	-0.62									
CHAIN			30639	5.210E+00	6.9	-0.53									
139 BA			48	4.690E+00	12.0	0.16		1.57	0.31	4.603E+00	(I)	2.6A			
CHAIN			30639	4.510E+00	5.1	-0.47									
140 BA			30639	4.530E+00	4.9	-0.40									
141 CE			917	5.080E+00	16.0	0.59									
CHAIN			30639	4.610E+00	4.8	0.04									
142 LA			644	4.320E+00	7.0	-2.28		8.19	1.17	4.953E+00	(I)	2.4			
CHAIN			30639	4.460E+00	2.9	-1.64									
143 BA			352	4.920E+00	10.0	-0.07									
CHAIN			30639	5.130E+00	4.9	0.80									
144 CE			895	5.570E+00	8.0	1.44									
CHAIN			30639	4.920E+00	15.0	-0.05									
145 PR			895	2.910E+00	5.0	-0.79									
CHAIN			30639	3.390E+00	6.5	-1.28									
146 CE			30639	3.390E+00	6.5	-1.28									
147 ND			917	2.000E+00	7.0	-1.05									
CHAIN			30639	2.300E+00	4.3	0.84									
148 CHAIN			1184	1.266E+00	10.1	-1.85									
149 ND			30639	1.290E+00	10.6	-0.70									
CHAIN			30639	1.290E+00	10.6	-0.70									
150 PM			895	1.690E+00	10.0	2.02									
CHAIN			30639	1.290E+00	10.6	-0.70									
151 PM			895	6.550E-01	15.0	-1.66									
CHAIN			30639	1.290E+00	10.6	-0.70									
152 SM			895	3.700E-01	20.0	-0.37									
CHAIN			30639	1.290E+00	10.6	-0.70									
153 SM			895	3.700E-01	20.0	-0.37									
CHAIN			30639	1.290E+00	10.6	-0.70									
154 EU			895	1.120E-01	18.0	-1.99									
CHAIN			30639	1.290E+00	10.6	-0.70									
155 GD			350	2.600E-02	12.0	0.39									
CHAIN			30639	1.290E+00	10.6	-0.70									

TABLE 50 CHAIN AND CUMULATIVE YIELDS FROM HIGH ENERGY FISSION OF 238U . (CONT)

A EL.	REF.	EXPERIMENTAL	NO.	YIELDS & SD	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	INT.	EXT./DF	MEAN	DEVIATION
NO.															
143 CE			352	3.510E+00	10.0	-1.13									
CHAIN			30639	3.600E+00	5.3	-1.64									
144 CE			79	2.680E+00	10.0W	-2.38									
CHAIN			30639	3.390E+00	6.5	-1.28									
145 PR			895	2.910E+00	5.0	-0.79									
CHAIN			30639	3.390E+00	6.5	-1.28									
146 CE			30639	1.920E+00	12.2	-1.32									
147 ND			917	2.000E+00	7.0	-1.05									
CHAIN			30639	2.300E+00	4.3	0.84									
148 CHAIN			1184	1.266E+00	10.1	-1.85									
149 ND			30639	1.290E+00	10.6	-0.70									
CHAIN			30639	1.290E+00	10.6	-0.70									
150 PM			895	1.690E+00	10.0	2.02									
CHAIN			30639	1.290E+00	10.6	-0.70									
151 PM			895	6.550E-01	15.0	-1.66									
CHAIN			30639	1.290E+00	10.6	-0.70									
152 SM			895	3.700E-01	20.0	-0.37									
CHAIN			30639	1.290E+00	10.6	-0.70									
153 SM			895	3.700E-01	20.0	-0.37									
CHAIN			30639	1.290E+00	10.6	-0.70									
154 EU			895	1.120E-01	18.0	-1.99									
CHAIN			30639	1.290E+00	10.6	-0.70									
155 GD			350	2.600E-02	12.0	0.39									
CHAIN			30639	1.290E+00	10.6	-0.70									

TABLE 50 CHAIN AND CUMULATIVE YIELDS FROM HIGH ENERGY FISSION OF 238U .

(cont.)

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT. EXT./DF	MEAN	DEVIATION		
161 FB	350 8.900E-03	15.0	0.79	0.62	0.62	7.988E-03 (1)	8.4A	
CHAIN	1016r7.684E-03	10.0	-0.79				(E) 6.6	
166 DY	350 6.300E-04	10.0				6.300E-04	10.0	
169 ER	350 1.290E-04	8.0				1.290E-04	8.0	
172 ER	350 2.100E-05	34.0				2.100E-05	34.0	

TABLE 51 CHAIN AND CUMULATIVE YIELDS FROM HIGH ENERGY FISSION OF 237NP.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT. EXT./DF	MEAN	DEVIATION		
1 H PI	2065r1.902E-02	41.4				1.902E-02	41.4	
3 H PI	2065r3.329E-02	22.6				3.329E-02	22.6	
4 HE PI	2065r2.010E-01	10.6				2.010E-01	10.6	
39 RB	2108 1.370E+00	15.0				1.370E+00	15.0	
91 SR	615 2.710E+00	10.0	-0.84			2.710E+00 (1)	9.0A	
	2108 3.310E+00	20.0	0.84			0.70 0.70 2.796E+00 (E)	7.5	
93 Y	615 4.940E+00	15.0				4.940E+00	15.0	
97 ZR	2108 5.430E+00	10.0	0.00			0.00 0.00 5.430E+00 (E)	0.7A	
	615 5.430E+00	9.0	0.00				0.0	
99 MO	615 4.940E+00	5.0	-0.62			0.39 0.39 4.973E+00 (1)	4.9A	
	2108 5.660E+00	20.0	0.62				(E) 3.0	
103 RU	2108 1.070E+00	20.0				1.070E+00	20.0	
105 RU	2108 3.630E+00	20.0	0.17			0.03 0.03 3.510E+00 (1)	5.7A	
RH	615 3.500E+00	6.0	-0.17				(E) 1.0	
109 PD	615 1.460E+00	17.0				1.460E+00	17.0	
111 AG	615 1.230E+00	5.0				1.230E+00	5.0	
112 PD	615 1.230E+00	5.0	-0.50			0.25 0.25 1.237E+00 (1)	4.9A	
	2108 1.370E+00	20.0	0.50				(E) 2.4	
115 CHAIN	615 1.230E+00	5.0				1.230E+00	5.0	
123 SN(M)	2108 7.000E-01	20.0						
125 SN(M)	2108 5.000E-01	50.0						
127 SB	615 2.520E+00	10.0	-0.56			0.31 0.31 2.542E+00 (E)	5.7A	
	2108 2.850E+00	20.0	0.56				3.2	
128 SB(G)	2108 1.420E+00	30.0				1.420E+00	30.0	
129 SB	2108 2.560E+00	20.0				2.560E+00	20.0	
130 SB(G)	2108 1.060E+00	20.0				1.060E+00	20.0	
131 I	2108 3.300E+00	10.0	-0.36			0.13 0.13 3.358E+00 (1)	8.6A	
	615 3.550E+00	17.0	0.36				3.1	
132 TE	2108 1.420E+00	10.0	-0.06			0.00 0.00 4.253E+00 (1)	0.6A	
	615 4.290E+00	17.0	0.06				0.0	
133 I (G)	2108 5.850E+00	10.0						
134 TE	2108 3.460E+00	20.0				4.680E+00	30.0	
I (G)	2108 1.620E+00	90.0						
CHAIN	2108 4.680E+00	30.0				4.690E+00	10.0	
135 I	2108 4.690E+00	10.0						
138 XE	2108 8.640E-01	90.0				0.29 0.29 3.714E+00 (1)	19.0A	
CS(G)	2108 2.770E+00	30.0	2.770E+00	0.00	0.09		(E) 10.3	
CS(M)	2108 3.650E+00	20.0	3.650E+00	0.00	0.00			
CHAIN	2108 4.300E+00	30.0	4.300E+00	0.00	0.21			
139 BA	615 4.840E+00	7.0				4.840E+00	7.0	
140 BA	615 4.890E+00	7.0				4.890E+00	7.0	
142 LA	2108 3.760E+00	15.0				3.760E+00	15.0	
143 CE	615 3.600E+00	21.0				3.600E+00	21.0	
146 PR	2108 1.530E+00	30.0				1.530E+00	30.0	
147 ND	615 1.730E+00	14.0				1.730E+00	14.0	
150 BA	2108 4.970E+00	15.0				4.970E+00	15.0	
153 SM	615 3.200E-01	8.0				3.200E-01	8.0	

TABLE 52 CHAIN AND CUMULATIVE YIELDS FROM HIGH ENERGY FISSION OF 239PU.

(CONT)

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED	STANDARD
NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION		
141 CE	21708 3.680E+00	4.1				3.680E+00	4.1		
143 CE	21708 2.930E+00	4.0							
144 CE	21708 2.590E+00	7.3				3.34	1.67	2.515E+00 (I)	4.5
								(E)	5.8A
CHAIN 1038r2.681E+00	6.8								
147 ND	106 1.470E+00	10.0				1.96	0.98	1.640E+00 (I)	3.2A
	21708 1.640E+00	4.2						(E)	3.2
CHAIN 1038r1.720E+00	5.9								
156 EU	106 1.700E-01	10.0				4.23	4.23	1.986E-01 (I)	4.9 >2
								(E)	10.1A
CHAIN 1038r2.127E-01	5.6								
161 TE	106 1.400E-02	15.0				0.95	0.95	1.553E-02 (I)	9.0A
								(E)	8.8
CHAIN 1038r1.674E-02	11.2								

TABLE 53 CHAIN AND CUMULATIVE YIELDS FROM HIGH ENERGY FISSION OF 240PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED	STANDARD
NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION		
66 NI	1076 6.040E-05	44.0				6.040E-05	44.0		
67 CU	1076 1.310E-04	35.0				1.310E-04	35.0		
72 ZN	1076 4.470E-03	17.0				4.470E-03	17.0		
73 GA	1076 8.340E-03	10.0				8.340E-03	10.0		
87 KR	1076 1.220E+00	12.0				1.220E+00	12.0		
88 KR	1076 1.390E+00	9.0				1.390E+00	9.0		
89 SR	1076 1.740E+00	7.0				1.740E+00	7.0		
90 SR	1076 1.940E+00	7.0				1.940E+00	7.0		
91 SR	1076 2.390E+00	7.0				0.17	0.17	2.438E+00 (I)	5.0A
								(E)	2.0
Y	1076 2.490E+00	7.0				0.41			
92 SR	1076 2.770E+00	7.0				-0.53			
								0.28	0.28
Y	1076 2.930E+00	8.0				0.53			(E) 2.8
93 Y	1076 2.880E+00	7.0						2.880E+00	7.0
95 ZR	1076 3.680E+00	7.0						3.680E+00	7.0
97 ZR	1076 4.180E+00	7.0						4.180E+00	7.0
99 MO	1076 4.850E+00	7.0						4.850E+00	7.0
103 RU	1076 5.270E+00	7.0						5.270E+00	7.0
105 RU	1076 5.250E+00	7.0				1.95		3.82	3.82
								4.695E+00 (I)	5.0 >2
								(E)	9.7A
RH	1076 4.320E+00	7.0				-1.95			
106 RU	1076 4.00E+00	7.0						4.00E+00	7.0
109 PD	1076 2.290E+00	7.0						2.290E+00	7.0
111 PD(M)	1076 9.900E-01	13.0						1.660E+00	7.0
AG	1076 1.660E+00	7.0							
112 PD	1076 1.560E+00	7.0						1.560E+00	7.0
115 CD(G)	1076 1.090E+00	7.0				0.00	0.00	1.162E+00 (I)	6.6A
								(E)	0.0
CD(M)	1076 1.60E-02	7.0							
117 CD(G)	1076 6.010E-01	24.0				0.00	0.00	8.580E-01 (I)	18.3A
								(E)	0.0
CD(M)	1076 2.570E-01	24.0						4.950E-01	10.0
118 CD	1076 4.950E-01	10.0							
125 SN(G)	1076 8.440E-01	7.0						1.570E+00	7.0
SB	1076 1.570E+00	7.0							
127 SN(G)	1076 1.430E+00	24.0						1.950E+00	7.0
SB	1076 1.950E+00	7.0							
128 SB(G)	1076 1.010E+00	7.0							
129 SB	1076 1.910E+00	7.0							
130 SB(G)	1076 1.710E+00	9.0							
131 TE(M)	1076 1.540E+00	7.0						4.450E+00	7.0
I	1076 4.450E+00	7.0							
132 TE	1076 3.550E+00	7.0						3.550E+00	7.0
133 I	1076 5.380E+00	8.0						5.380E+00	8.0
135 I	1076 3.860E+00	8.0						5.790E+00	8.0
XE	1076 5.790E+00	8.0							
CS(G)	1076 4.970E+00	8.0							
137 CS	1076 4.480E+00	8.0						4.480E+00	8.0

TABLE 53 CHAIN AND CUMULATIVE YIELDS FROM HIGH ENERGY FISSION OF 240PU.

(CONT.)

A EL. NO.	REF. NO.	EXPERIMENTAL YIELDS & SD	MEAN R	CHI2/DF COMPONENT VALUE	CHI2 EXTERNAL	TOTAL CHI2 INT. EXT./DF	WEIGHTED MEAN DEVIATION
138 CS	1076	5.190E+00	14.0			5.190E+00	14.0
139 BA	1076	4.560E+00	7.0			4.560E+00	7.0
140 BA	1076	3.770E+00	7.0			3.770E+00	7.0
141 CE	1076	3.570E+00	7.0			3.570E+00	7.0
142 LA	1076	3.880E+00	12.0			3.880E+00	12.0
143 CE	1076	3.090E+00	7.0			3.090E+00	7.0
144 CE	1076	2.650E+00	7.0			2.650E+00	7.0
145 PR	1076	2.690E+00	14.0			2.690E+00	14.0
147 ND	1076	1.780E+00	7.0			1.780E+00	7.0
149 ND	1076	1.450E+00	7.0			1.450E+00	7.0
PM	1076	1.290E+00	7.0	-1.18		1.18	(E) 5.8A
151 PM	1076	8.050E-01	10.0			8.050E-01	10.0
153 SN	1076	5.800E-04	8.0			5.800E-04	8.0
155 EU	1076	2.780E-01	7.0			2.780E-01	7.0
156 EU	1076	2.250E-01	7.0			2.250E-01	7.0
157 EU	1076	1.580E-01	7.0			1.580E-01	7.0
159 GD	1076	6.800E-02	19.0			6.800E-02	19.0
161 TB	1076	3.460E-02	7.0			3.460E-02	7.0
169 ER	1076	1.150E-03	8.0			1.150E-03	8.0

TABLE 54 CHAIN AND CUMULATIVE YIELDS FROM HIGH ENERGY FISSION OF 242PU.

A EL. NO.	REF. NO.	EXPERIMENTAL YIELDS & SD	MEAN R	CHI2/DF COMPONENT VALUE	CHI2 EXTERNAL	TOTAL CHI2 INT. EXT./DF	WEIGHTED MEAN DEVIATION
85 KR(M)	21983	6.720E-01	7.1			6.720E-01	7.1
87 KR	21983	9.930E-01	7.6			9.930E-01	7.6
88 KR	21983	1.160E+00	8.1			1.160E+00	8.1
89 RB	21983	1.330E+00	11.0			1.330E+00	11.0
91 SR	21983	2.110E+00	7.1	0.30		0.13	0.07 2.071E+00 (I) 3.7A
Y (M)	21983	2.030E+00	7.9	-0.29			(E) 1.0
CHAIN 21983	2.070E+00	5.3	-0.02				
92 SR	21983	2.260E+00	13.0	-0.46		0.30	0.15 2.377E+00 (I) 6.2A
Y	21983	2.490E+00	12.0	0.44			(E) 2.4
CHAIN 21983	2.380E+00	8.8	0.02				
93 Y	21983	2.600E+00	13.0				2.600E+00 13.0
94 Y	21983	2.790E+00	10.0				2.790E+00 10.0
95 ZR	21983	3.370E+00	8.9				3.370E+00 8.9
97 ZR	21983	4.230E+00	7.5	0.02		0.00	0.00 4.225E+00 (I) 5.2A
NB	21983	4.220E+00	7.1	-0.02			(E) 0.1
99 MO	21983	4.970E+00	7.2	0.43		0.29	0.15 4.836E+00 (I) 3.7A
TC(M)	21983	4.700E+00	7.4	-0.45			(E) 1.4
CHAIN 21983	4.840E+00	5.2	0.03				
101 TC	21983	5.040E+00	99.0				5.040E+00 99.0
103 RB	21983	5.640E+00	79.0				5.640E+00 79.0
104 TC	21983	5.450E+00	12.0				5.450E+00 12.0
105 RU	21983	5.580E+00	7.5	0.22		0.07	0.04 5.501E+00 (I) 3.9A
RH	21983	5.420E+00	7.9	-0.22			(E) 0.7
CHAIN 21983	5.500E+00	5.5	0.00				
107 RH	21983	3.800E+00	10.0				3.800E+00 10.0
109 PD	21983	2.530E+00	8.6				2.530E+00 8.6
111 PD(M)	21983	9.400E-05	64.0				2.200E+00 11.0
AG	21983	2.200E+00	11.0				
112 PD	21983	1.920E+00	7.2				1.920E+00 7.2
113 AG	21983	1.600E+00	10.0	-0.61		0.37	0.37 1.653E+00 (I) 8.1A
CHAIN 21983	1.780E+00	14.0	0.61				(E) 5.0
115 CD	21983	1.120E+00	13.0				1.120E+00 13.0
117 CD(G)	21983	5.030E-01	20.0	5.030E-01 0.00	0.00 0.0	0.00	0.00 6.521E-01 (I) 11.6A
CD(M)	21983	1.510E-01	20.0	1.510E-01 0.00	0.00		(E) 0.3
CHAIN 21983	6.500E-01	16.9	6.500E-01 0.00	0.00			
118 CD	21983	4.200E-01	16.0				
121 SN	21983	6.580E-01	20.0	-0.47		0.22	0.22 6.962E-01 (I) 15.0A
CHAIN 21983	7.600E-01	22.4	0.47				(E) 7.1
125 SN	21983	6.840E-01	16.0				1.350E+00 18.0
SB	21983	1.350E+00	18.0				
126 SB	21983	1.200E-01	60.0				
127 SN	21983	1.660E+00	11.0				1.860E+00 12.2
SB	21983	1.870E+00	11.2				
CHAIN 21983	1.880E+00	12.2					

TABLE 54 CHAIN AND CUMULATIVE YIELDS FROM HIGH ENERGY FISSION OF 242PU.

(CONT.)

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXT./DF	MEAN	DEVIATION	INT.	EXT./DF	MEAN	DEVIATION
128 SN	21983	1.290E+00 20.0	-0.79	2.49	0.83	1.466E+00 (I)	8.8A			
	21983	1.300E+00 17.0	-0.92				(E)	8.0		
SB	21983	6.780E-01 11.0								
CHAIN	21983	1.700E+00 21.2	0.69							
	21983	1.710E+00 14.0	1.21							
129 SB	21983	2.000E+00 10.0	-0.49	0.33	0.11	2.086E+00 (I)	4.6A			
TE	21983	2.160E+00 10.0	0.38				(E)	1.5		
CHAIN	21983	2.070E+00 10.1	-0.09							
	21983	2.110E+00 7.6	0.19							
130 SB	21983	1.420E+00 12.0				1.610E+00	12.4			
CHAIN	21983	1.610E+00 12.4								
131 SB	21983	2.400E+00 13.0				3.550E+00	14.9			
TE(M)	21983	1.590E+00 10.0								
I	21983	3.910E+00 6.1								
CHAIN	21983	3.550E+00 14.9								
132 TE	21983	4.560E+00 7.4		0.33	0.33	5.060E+00 (I)	3.9A			
I	21983	5.270E+00 5.3					(E)	2.2		
CHAIN	21983	4.880E+00 7.6	-0.57							
	21983	5.130E+00 4.5	0.57							
133 TE(M)	21983	1.430E+00 13.0		0.07	0.02	5.581E+00 (I)	3.3A			
I	21983	5.520E+00 7.2	-0.17				(E)	0.5		
XE	21983	5.660E+00 7.6	0.20							
CHAIN	21983	5.540E+00 7.2	-0.12							
	21983	5.600E+00 5.4	0.08							
134 I	21983	5.990E+00 12.0				5.830E+00	12.0			
CHAIN	21983	5.830E+00 12.0								
135 I	21983	5.100E+00 8.7		0.43	0.21	5.739E+00 (I)	4.6A			
XE	21983	5.520E+00 8.9	-0.53				(E)	2.1		
CHAIN	21983	5.750E+00 6.6	0.04							
	21983	6.010E+00 9.5	0.54							
138 CS	21983	5.000E+00 9.1				5.020E+00	9.2			
CHAIN	21983	5.020E+00 9.2								
139 BA	21983	4.930E+00 7.7								
140 BA	21983	4.840E+00 9.0	-0.16	0.07	0.02	4.906E+00 (I)	3.5A			
LA	21983	4.950E+00 7.8	0.13				(E)	0.4		
CHAIN	21983	4.850E+00 9.1	-0.14							
	21983	4.910E+00 6.1	0.02							
	21983	4.950E+00 7.9	0.13							
141 CE	21983	4.860E+00 8.2				4.860E+00	8.2			
142 LA	21983	4.340E+00 7.6								
143 CE	21983	3.660E+00 7.1				3.660E+00	7.1			
144 CE	21983	3.190E+00 8.4								
146 PR	21983	2.180E+00 8.7								
149 ND	21983	1.610E+00 9.9								
151 PM	21983	9.150E-01 9.7				9.200E-01	9.8			
CHAIN	21983	9.200E-01 9.8								

TABLE 55 CHAIN AND CUMULATIVE YIELDS FROM HIGH ENERGY FISSION OF 241AM.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXT./DF	MEAN	DEVIATION	INT.	EXT./DF	MEAN	DEVIATION
87 KR	1154	1.050E+00	4.0				1.050E+00	4.0		
88 KR	1154	1.070E+00	3.0				1.070E+00	3.0		
91 SR	1154	2.010E+00	3.0	-0.81			0.65	0.65	2.044E+00	(I) 2.1A
Y	1154	2.080E+00	3.0	0.81						(E) 1.7
92 SR	1154	2.150E+00	3.0						2.150E+00	3.0
94 Y	1154	2.550E+00	3.0						2.550E+00	3.0
95 ZR	1154	3.140E+00	3.0						3.140E+00	3.0
97 ZR	1154	3.390E+00	3.0						3.390E+00	3.0
99 MO	1154	4.360E+00	3.0						4.360E+00	3.0
103 RU	1154	5.070E+00	3.0						5.070E+00	3.0
104 TC	1154	4.630E+00	3.0						4.630E+00	3.0
105 RH	1154	4.760E+00	3.0						4.760E+00	3.0
106 RU	1154	4.100E+00	3.0						4.100E+00	3.0
107 RH	1154	3.800E+00	3.0						3.800E+00	3.0
109 PD	1154	3.240E+00	3.0						3.240E+00	3.0
111 PD(M)	1154	1.770E-01	8.4						2.310E+00	3.0
AG	1154	2.310E+00	3.0							
112 PD	1154	2.420E+00	3.0						2.420E+00	3.0
113 AG	1154	2.210E+00	3.0						2.210E+00	3.0
115 CD(G)	1154	1.600E+00	3.0	1.600E+00			0.00	0.00	1.730E+00	(I) 2.8A
CD(M)	1154	1.300E-01	3.0	1.300E-01						(E) 0.0
126 SB(G)	1154	6.890E-01	13.0							
127 SB	1154	2.230E+00	5.0						2.230E+00	5.0
128 SN	1154	4.930E-01	3.0							
SB(G)	1154	1.170E+00	3.0							
130 I	1154	6.670E-01	4.0							
131 TE(M)	1154	1.400E+00	7.0						4.450E+00	3.0
I	1154	4.450E+00	3.0							
132 TE	1154	2.160E+00	3.0							
CS	1154	7.850E-03	14.0							
133 I	1154	4.300E+00	3.0						4.600E+00	3.0
XE	1154	4.600E+00	3.0							
134 CS	1154	2.250E-01	5.0							
135 I	1154	1.810E+00	4.0						4.490E+00	3.0
XE	1154	4.490E+00	3.0							
136 CS	1154	1.240E+00	3.0							
137 CS	1154	4.250E+00	3.0						4.250E+00	3.0
139 BA	1154	4.020E+00	3.0						4.020E+00	3.0
140 BA	1154	3.340E+00	3.0						3.340E+00	3.0
141 CE	1154	3.230E+00	3.0						3.230E+00	3.0
142 LA	1154	2.960E+00	3.0						2.960E+00	3.0
143 CE	1154	2.690E+00	3.0						2.690E+00	3.0
144 CE	1154	2.490E+00	3.0						2.490E+00	3.0
147 ND	1154	1.810E+00	3.0						1.810E+00	3.0

TABLE 55 CHAIN AND CUMULATIVE YIELDS FROM HIGH ENERGY FISSION OF 241AM.

(CONT.)

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	CHI2/DF	COMPONENT VALUE	EXTERNAL	INT. EXT./DF	MEAN	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	SD	COMPONENT	VALUE	EXTERNAL	INT. EXT./DF	MEAN	DEVIATION				
149 PM	1154	1.300E+00	3.0					1.300E+00	3.0				
151 PM	1154	8.850E-01	3.0					8.850E-01	3.0				
153 SM	1154	6.680E-01	3.0					6.680E-01	3.0				
155 EU	1154	3.390E-01	3.0					3.390E-01	3.0				
156 SM	1154	2.200E-01	3.0					2.700E-01	3.0				
EU	1154	2.700E-01	3.0										
157 EU	1154	6.90E-01	3.0					6.90E-01	3.0				
159 GD	1154	1.310E-01	5.0					1.310E-01	5.0				
161 TB	1154	6.010E-02	3.0					6.010E-02	3.0				

TABLE 56 CHAIN AND CUMULATIVE YIELDS FROM SPONTANEOUS FISSION OF 232TH.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	CHI2/DF	COMPONENT VALUE	EXTERNAL	INT. EXT./DF	MEAN	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	SD	COMPONENT	VALUE	EXTERNAL	INT. EXT./DF	MEAN	DEVIATION				
83 KR	326	3.600E-02	69.4					3.600E-02	69.4				
84 KR	326	1.800E-01	22.2					1.800E-01	22.2				
86 KR	326	8.600E-01	14.0					8.600E-01	14.0				
131 XE	326	5.090E-01	3.9					5.090E-01	3.9				
132 XE	326	3.630E+00	2.2					3.630E+00	2.2				
134 XE	326	5.120E+00	1.9					5.120E+00	1.9				
136 XE	326	6.000E+00	20.0					6.000E+00	20.0				

TABLE 58 CHAIN AND CUMULATIVE YIELDS FROM SPONTANEOUS FISSION OF 240PU.

A EL. NO.	REF. NO.	EXPERIMENTAL YIELDS & SD	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD DEVIATION
			COMPONENT VALUE	EXTERNAL	INT.	EXT./DF		
4 HE DT	850	3.190E+01	10.0					3.190E+01
89 CHAIN	21482	8.000E+01	40.0					8.000E+01
91 CHAIN	21482	1.510E+00	11.3					1.510E+00
97 CHAIN	21482	6.480E+00	3.2					6.480E+00
99 CHAIN	21482	6.820E+00	1.0					6.820E+00
105 CHAIN	21482	7.100E+00	7.8					7.100E+00
109 CHAIN	21482	9.400E+01	12.8					9.400E+01
111 CHAIN	21482	3.500E+02	25.7					3.500E+02
115 CHAIN	21482	3.000E+02	100.0					3.000E+02
131 CHAIN	21482	2.340E+00	2.1					2.340E+00
133 CHAIN	21482	8.200E+00	1.5					8.200E+00
135 CHAIN	21482	6.940E+00	9.7					6.940E+00
140 CHAIN	21482	5.990E+00	3.7					5.990E+00
141 CHAIN	21482	6.020E+00	6.5					6.020E+00
143 CHAIN	21482	4.780E+00	8.2					4.780E+00
147 CHAIN	21482	1.220E+00	30.3					1.220E+00

TABLE 59 CHAIN AND CUMULATIVE YIELDS FROM SPONTANEOUS FISSION OF 242PU.

A EL. NO.	REF. NO.	EXPERIMENTAL YIELDS & SD	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD DEVIATION
			COMPONENT VALUE	EXTERNAL	INT.	EXT./DF		
4 HE DT	851	2.740E+01	10.0					2.740E+01
121 CHAIN	40194	1.280E+01	20.0					1.280E+01
122 CHAIN	40194	1.280E+01	20.0					1.280E+01
123 CHAIN	40194	1.690E+01	20.0					1.690E+01
124 CHAIN	40194	2.360E+01	20.0					2.360E+01
125 CHAIN	40194	3.170E+01	20.0					3.170E+01
126 CHAIN	40194	4.370E+01	20.0					4.370E+01
127 CHAIN	40194	6.840E+01	20.0					6.840E+01
128 CHAIN	40194	1.116E+00	20.0					1.116E+00
129 CHAIN	40194	1.966E+00	20.0					1.966E+00
130 CHAIN	40194	2.953E+00	20.0					2.953E+00
131 CHAIN	40194	4.065E+00	20.0					4.065E+00
132 I	662	5.008E+00	14.0	-0.22		0.05	0.05	5.084E+00 (I) 11.5A
CHAIN	40194	5.275E+00	20.0	0.22				(E) 2.5
133 I	662	5.300E+00	13.2	-0.75		0.56	0.56	5.552E+00 (I) 11.1A
CHAIN	40194	6.393E+00	20.0	0.75				(E) 8.3
134 I	662	6.700E+00	14.9	-0.28		0.08	0.08	6.857E+00 (I) 12.0A
CHAIN	40194	7.181E+00	20.0	0.28				(E) 3.3
135 I	662	4.900E+00	16.3	-1.51		2.29	2.29	5.470E+00 (I) 12.9 >2
CHAIN	40194	7.458E+00	20.0	1.51				(E) 19.5A
136 CHAIN	40194	7.701E+00	20.0					7.701E+00 20.0
137 CHAIN	40194	7.601E+00	20.0					7.601E+00 20.0
138 CHAIN	40194	6.866E+00	20.0					6.866E+00 20.0
139 CHAIN	40194	5.983E+00	20.0					5.983E+00 20.0
140 CHAIN	40194	5.556E+00	20.0					5.556E+00 20.0
141 CHAIN	40194	4.942E+00	20.0					4.942E+00 20.0
142 CHAIN	40194	4.230E+00	20.0					4.230E+00 20.0
143 CHAIN	40194	3.635E+00	20.0					3.635E+00 20.0
144 CHAIN	40194	3.193E+00	20.0					3.193E+00 20.0
145 CHAIN	40194	2.797E+00	20.0					2.797E+00 20.0
146 CHAIN	40194	2.167E+00	20.0					2.167E+00 20.0
147 CHAIN	40194	1.657E+00	20.0					1.657E+00 20.0
148 CHAIN	40194	1.318E+00	20.0					1.318E+00 20.0
149 CHAIN	40194	1.097E+00	20.0					1.097E+00 20.0
150 CHAIN	40194	8.300E+01	20.0					8.300E+01 20.0
151 CHAIN	40194	5.460E+01	20.0					5.460E+01 20.0
152 CHAIN	40194	3.550E+01	20.0					3.550E+01 20.0
153 CHAIN	40194	2.680E+01	20.0					2.680E+01 20.0
154 CHAIN	40194	2.110E+01	20.0					2.110E+01 20.0
155 CHAIN	40194	1.700E+01	20.0					1.700E+01 20.0
156 CHAIN	40194	1.180E+01	20.0					1.180E+01 20.0
157 CHAIN	40194	7.200E+02	20.0					7.200E+02 20.0
158 CHAIN	40194	5.200E+02	20.0					5.200E+02 20.0
159 CHAIN	40194	3.600E+02	20.0					3.600E+02 20.0

TABLE 59 CHAIN AND CUMULATIVE YIELDS FROM SPONTANEOUS FISSION OF 242PU.

(cont.)

A EL. NO.	REF. NO.	EXPERIMENTAL YIELDS & SD.	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD DEVIATION
			COMPONENT VALUE	EXTERNAL	INT.	EXT./DF		
160 CHAIN	40194	2.300E-02	20.0					2.300E-02
161 CHAIN	40194	1.100E-02	20.0					1.100E-02
162 CHAIN	40194	1.200E-02	20.0					1.200E-02

TABLE 60 CHAIN AND CUMULATIVE YIELDS FROM SPONTANEOUS FISSION OF 242CM.

A EL. NO.	REF. NO.	EXPERIMENTAL YIELDS & SD.	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD DEVIATION
			COMPONENT VALUE	EXTERNAL	INT.	EXT./DF		
4 HE FI	2049	2.940E-01	20.0	-1.35				1.82
	848	3.80E-01	10.0					1.82
91 SR	613	9.400E-01	31.9					9.400E-01
92 SR	613	1.100E+00	27.3					1.100E+00
99 MO	613	5.700E+00	12.3					5.700E+00
103 RU	613	7.200E+00	20.8					
105 RU	613	9.500E+00	9.5					9.500E+00
106 RU	613	7.400E+00	10.8					7.400E+00
109 PD(M)	613	2.900E+00	13.8					2.900E+00
112 PD	613	9.500E-01	15.8					9.500E-01
115 PD(M)	613	1.300E-02	30.3					1.300E-02
127 SB	613	3.500E-01	28.6					3.500E-01
129 SB	613	1.300E+00	23.1					1.300E+00
131 TE	613	2.300E+00	21.7					2.300E+00
I								
	613	2.000E+00	20.0					
132 TE	613	5.800E+00	15.5					5.800E+00
133 I	613	5.700E+00	14.0					5.700E+00
134 I	613	6.900E+00	14.5					6.900E+00
135 I	613	3.900E+00	15.4					
139 BA	613	6.600E+00	10.6					6.600E+00
140 BA	613	5.900E+00	13.6					5.900E+00

TABLE 61 CHAIN AND CUMULATIVE YIELDS FROM SPONTANEOUS FISSION OF 244CM.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	YIELDS & SD	COMPONENT VALUE	MEAN	EXT./DF	EXT./DF	EXT./DF	EXT./DF	DEVIATION
1 H PI	2065r1.221E-02	41.0						1.221E-02
3 H PI	2065r2.197E-02	22.0						2.197E-02
4 HE PI	2065r2.426E-01	10.6						2.17
	2054 3.145E-01	10.0						1.12
	849 3.190E-01	10.0						1.26
77 AS	720 2.500E-03	36.0						2.500E-03
83 BR	720 1.160E-01	10.3						1.160E-01
84 KR	720 1.600E-01	20.5						1.600E-01
85 KR(M)	720 3.070E-01	10.1						3.070E-01
86 KR	720 2.890E-01	15.6						2.890E-01
89 SR	720 7.160E-01	5.0						7.160E-01
90 SR	720 8.080E-01	10.0						8.080E-01
91 SR	720 8.250E-01	10.1						8.250E-01
95 ZR	720 1.630E+00	9.8						1.630E+00
97 ZR	720 3.040E+00	9.9						3.040E+00
99 MO	720 3.750E+00	1.0						3.750E+00
	2104 4.030E+00	5.0						4.030E+00
103 RU	720 6.940E+00	10.1						6.940E+00
105 RU	720 9.430E+00	10.0						9.430E+00
RE	720 9.060E+00	10.0						9.060E+00
106 RU	720 7.400E+00	10.0						7.400E+00
109 PD	720 5.020E+00	10.0						5.020E+00
111 AG	720 2.870E+00	4.9						2.870E+00
112 PD	720 2.030E+00	9.8						2.030E+00
113 AG(G)	720 7.900E-01	10.1						7.900E-01
115 CD(G)	720 2.330E-01	5.2						2.330E-01
CD(M)	720 2.500E-02	8.0						2.500E-02
125 SN(G)	720 6.700E-03	19.4						6.700E-03
127 SB	720 2.000E-01	10.0						2.000E-01
129 SB	720 7.400E-01	9.5						7.400E-01
TE(G)	720 4.700E-01	10.6						4.700E-01
131 I	720 3.150E+00	10.2						3.150E+00
XE	720 3.030E+00	5.0						3.030E+00
	13256r3.036E+00	7.1						3.036E+00
132 TE	720 4.270E+00	5.2						4.270E+00
XE	13256r4.235E+00	7.1						4.235E+00
133 I	720 7.450E+00	20.1						7.450E+00
XE	13256r5.753E+00	7.1						5.753E+00
134 XE	13256r6.892E+00	7.1						6.892E+00
	720 6.940E+00	5.0						6.940E+00
135 I	720 5.480E+00	20.1						5.480E+00
XE	720 7.500E+00	5.1						7.500E+00
	13256r7.651E+00	7.1						7.651E+00
136 XE	720 7.590E+00	5.0						7.590E+00
137 CS	720 8.140E+00	9.9						8.140E+00
139 BA	720 7.160E+00	10.1						7.160E+00

TABLE 61 CHAIN AND CUMULATIVE YIELDS FROM SPONTANEOUS FISSION OF 244CM.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	YIELDS & SD	COMPONENT VALUE	MEAN	EXT./DF	EXT./DF	EXT./DF	EXT./DF	DEVIATION
140 BA	720 6.040E+00	5.3						6.040E+00
	2104 6.300E+00	10.0						6.300E+00
141 CE	720 5.790E+00	5.0						5.790E+00
143 CE	720 3.900E+00	5.1						3.900E+00
144 CE	720 4.040E+00	9.9						4.040E+00
147 ND	720 1.440E+00	20.1						1.440E+00
149 ND	720 1.540E+00	9.7						1.540E+00
PM	720 1.660E+00	10.2						1.660E+00
151 PM	720 7.000E-01	10.0						7.000E-01
153 SM	720 5.200E-01	9.6						5.200E-01
156 SM	720 2.300E-01	13.0						2.300E-01
EU	720 1.900E-01	10.5						1.900E-01

TABLE 62 CHAIN AND CUMULATIVE YIELDS FROM SPONTANEOUS FISSION OF 246CM.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	YIELDS & SD.	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION	
95 ZR	10986	1.990E+00	14.1			1.990E+00	1.990E+00	4.1
97 ZR	10986	2.370E+00	12.2			2.370E+00	2.370E+00	12.2
99 MO	10986	4.240E+00	8.5			4.240E+00	4.240E+00	8.5
103 RU	10986	6.860E+00	8.8			6.860E+00	6.860E+00	8.8
112 AG	10986	4.050E+00	13.3			4.050E+00	4.050E+00	13.3
105 RU	10986	6.820E+00	14.1			6.820E+00	6.820E+00	14.1
111 AG	10986	4.640E+00	42.5			4.640E+00	4.640E+00	42.5
112 AG	10986	4.050E+00	13.3			4.050E+00	4.050E+00	13.3
131 I	10986	3.390E+00	8.6			3.390E+00	3.390E+00	8.6
132 TE	10986	4.680E+00	8.1			4.680E+00	4.680E+00	8.1
133 I	10986	5.810E+00	9.1			5.810E+00	5.810E+00	9.1
135 I	10986	6.310E+00	10.0			6.310E+00	6.310E+00	10.0
140 BA	10986	6.540E+00	9.9			6.540E+00	6.540E+00	9.9
141 CE	10986	5.470E+00	10.2			5.470E+00	5.470E+00	10.2
142 LA	10986	5.740E+00	24.6			5.740E+00	5.740E+00	24.6
143 CE	10986	5.460E+00	10.3			5.460E+00	5.460E+00	10.3
144 CE	10986	5.190E+00	17.5			5.190E+00	5.190E+00	17.5
147 ND	10986	2.620E+00	9.2			2.620E+00	2.620E+00	9.2

TABLE 63 CHAIN AND CUMULATIVE YIELDS FROM SPONTANEOUS FISSION OF 248CM.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	YIELDS & SD.	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION	
83 CHAIN	12711	3.600E-02	11.1	-1.37		1.87	3.800E-02	9.8
	10979	5.100E-02	20.0					13.4A
84 CHAIN	12711	7.400E-02	12.2				7.400E-02	12.2
85 CHAIN	12711	9.600E-02	11.5				9.600E-02	11.5
86 CHAIN	12711	1.610E-01	9.9				1.610E-01	9.9
89 CHAIN	10979	4.200E-01	20.0				4.200E-01	20.0
91 CHAIN	10979	5.800E-01	20.0	-0.18		0.03	5.942E-01	14.1A
	10979	6.100E-01	20.0	0.18				2.5
95 CHAIN	10979	1.600E+00	20.0				1.600E+00	20.0
97 CHAIN	10979	2.570E+00	20.0				2.570E+00	20.0
99 CHAIN	10979	3.960E+00	20.0	-0.46		0.21	4.199E+00	14.2A
	10979	5.300E+00	20.0	0.46				6.5
103 CHAIN	10979	5.300E+00	20.0	-0.10		0.01	5.373E+00	14.1A
	10979	5.450E+00	20.0	0.10				1.4
105 CHAIN	10979	6.320E+00	20.0				6.320E+00	20.0
106 CHAIN	10979	5.980E+00	20.0	-0.24		0.06	6.176E+00	14.2A
	10979	6.400E+00	20.0	0.24				3.4
109 CHAIN	10979	5.910E+00	20.0				5.910E+00	20.0
111 CHAIN	10979	5.190E+00	20.0				5.190E+00	20.0
112 CHAIN	10979	3.940E+00	20.0	-0.66		0.44	4.273E+00	14.2A
	10979	4.760E+00	20.0	0.66				9.4
113 CHAIN	10979	2.820E+00	20.0				2.820E+00	20.0
115 CHAIN	10979	1.390E+00	20.0	0.00		0.00	1.390E+00	20.0
	10979	1.300E+00	20.0	0.00				0.0
125 CHAIN	10979	6.600E-03	20.0				6.600E-03	20.0
127 CHAIN	10979	3.100E-02	20.0				3.100E-02	20.0
129 CHAIN	10979	3.200E-01	20.0				3.200E-01	20.0
131 CHAIN	12711	2.210E+00	9.9	-0.94		0.98	0.49	2.316E+00
	10979	2.510E+00	20.0	0.42				8.2A
	10979	2.740E+00	20.0	0.83				5.7
132 CHAIN	12711	3.730E+00	9.9	0.90		0.82	0.41	3.900E+00
	10979	4.310E+00	20.0	0.51				8.1A
	10979	4.450E+00	20.0	0.66				5.2
133 CHAIN	10979	4.910E+00	20.0	-0.29		0.08	0.08	5.103E+00
	10979	5.330E+00	20.0	0.29				14.2A
	10979	5.330E+00	20.0	0.41				4.1
134 CHAIN	12711	4.890E+00	10.0				4.890E+00	10.0
135 CHAIN	10979	5.620E+00	20.0				5.620E+00	20.0
136 CHAIN	12711	4.550E+00	9.9				4.550E+00	9.9
137 CHAIN	10979	6.050E+00	20.0				6.050E+00	20.0
139 CHAIN	10979	6.200E+00	20.0				6.200E+00	20.0
140 CHAIN	10979	5.660E+00	20.0	-0.41		0.17	0.17	5.969E+00
	10979	6.360E+00	20.0	0.41				14.2A
141 CHAIN	10979	5.440E+00	20.0	-0.45		0.20	0.20	5.763E+00
	10979	6.180E+00	20.0	0.45				14.2A
								6.4
142 CHAIN	10979	6.280E+00	20.0				6.280E+00	20.0
143 CHAIN	10979	5.440E+00	20.0				5.440E+00	20.0
144 CHAIN	10979	5.750E+00	20.0	-0.17		0.03	0.03	5.888E+00
	10979	6.040E+00	20.0	0.17				14.1A
								2.5
147 CHAIN	10979	3.120E+00	20.0				3.120E+00	20.0
151 CHAIN	10979	1.180E+00	20.0				1.180E+00	20.0
153 CHAIN	10979	7.900E-01	20.0				7.900E-01	20.0

TABLE 64 CHAIN AND CUMULATIVE YIELDS FROM SPONTANEOUS FISSION OF 250CF.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	YIELDS & SD.	NO.	YIELDS & SD.	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION		
1 H	PI 2048 9.000E-03	25.0						9.000E-03	25.0		
3 H	PI 2048 2.700E-02	20.0						2.700E-02	20.0		
4 H	PI 2048 3.980E-01	10.0						3.980E-01	10.0		
83 CHAIN	12713 4.300E-02	16						8.01 8.01 4.632E-02	(I) 0.53		>2
											20.6
84 CHAIN	12711 8.200E-02	12.2						8.200E-02	12.2		
85 CHAIN	12711 1.120E-01	10.7						1.120E-01	10.7		
86 CHAIN	12711 4.00E-01	10.0						4.00E-01	10.0		
89 CHAIN	10979 4.800E-01	20.0						4.800E-01	20.0		
91 CHAIN	10979 5.600E-01	20.0						0.06 0.06 5.786E-01	(I) 14.2A		
								0.24			3.4
95 CHAIN	10979 1.310E+00	20.0						0.30 0.30 1.403E+00	(I) 14.2A		
								0.55			(E) 7.7
97 CHAIN	10979 1.560E+00	20.0						0.05 0.05 1.607E+00	(I) 14.1A		
								0.22			(E) 3.1
99 CHAIN	10979 3.280E+00	20.0						0.00 0.00 3.295E+00	(I) 14.1A		
								0.03			(E) 0.5
101 TC	12710 3.990E+00	27.8						3.990E+00	27.8		
103 CHAIN	10979 5.350E+00	20.0						0.01 0.01 5.273E+00	(I) 14.1A		
								0.10			
104 TC	12710 6.560E+00	14.0						6.560E+00	14.0		
105 RU	12710 6.380E+00	8.3						0.05 0.05 6.422E+00	(I) 7.7A		
								0.22			(E) 1.7
106 CHAIN	10979 6.680E+00	20.0						0.16 0.16 7.031E+00	(I) 14.2A		
								0.39			(E) 5.6
107 RE	12710 7.330E+00	14.5						7.330E+00	14.5		
109 CHAIN	10979 6.370E+00	20.0						6.370E+00	20.0		
111 CHAIN	10979 4.970E+00	20.0						4.970E+00	20.0		
112 CHAIN	10979 3.470E+00	20.0						0.31 0.31 3.723E+00	(I) 14.2A		
								0.56			(E) 8.0
113 CHAIN	10979 3.560E+00	20.0						3.560E+00	20.0		
115 CHAIN	10979 1.840E+00	20.0						0.20 0.20 1.949E+00	(I) 14.2A		
								0.45			(E) 6.4
121 CHAIN	10979 2.900E-02	20.0						2.900E-02	20.0		
125 CHAIN	10979 2.200E-02	20.0						2.200E-02	20.0		
127 CHAIN	10979 1.140E-01	20.0						1.140E-01	20.0		
129 CHAIN	10979 4.000E-01	20.0						4.000E-01	20.0		
131 CHAIN	12711 1.130E+00	9.7						3.95 1.98 1.218E+00	(I) 8.1		11.4A
											(E) 11.4A
132 CHAIN	10979 1.450E+00	20.0						2.91 1.46 1.805E+00	(I) 8.1		
											(E) 10.1A
133 I	12710 3.660E+00	11.2						0.13 0.07 3.745E+00	(I) 8.6A		
											(E) 2.3
134 CHAIN	12711 2.810E+00	10.0						2.810E+00	10.0		
135 CHAIN	10979 4.030E+00	20.0						4.030E+00	20.0		
136 CHAIN	12711 3.300E+00	10.0						3.300E+00	10.0		
139 BA	12710 6.320E+00	9.0						0.00 0.00 6.304E+00	(I) 8.2A		
											(E) 0.5

TABLE 64 CHAIN AND CUMULATIVE YIELDS FROM SPONTANEOUS FISSION OF 250CF. (CONT.)

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	YIELDS & SD.	NO.	YIELDS & SD.	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION		
140 CHAIN	10979 5.170E+00	20.0						0.13 0.13 5.417E+00	(I) 14.2A		
								0.36			(E) 5.1
141 CHAIN	10979 5.870E+00	20.0						0.00 0.00 5.885E+00	(I) 14.1A		
								0.02			(E) 0.3
142 LA	12710 6.660E+00	10.4						6.660E+00	10.4		
143 CHAIN	10979 5.540E+00	20.0						0.02 0.02 5.655E+00	(I) 14.1A		
								0.15			(E) 2.1
144 CHAIN	10979 5.660E+00	20.0						0.37 0.13 4.869E+00	(I) 14.2A		
								0.37			
147 CHAIN	10979 3.830E+00	20.0						3.830E+00	20.0		
149 CHAIN	10979 3.270E+00	20.0						3.270E+00	20.0		
151 CHAIN	10979 2.060E+00	20.0						2.060E+00	20.0		
153 CHAIN	10979 1.220E+00	20.0						1.220E+00	20.0		

TABLE 66 CHAIN AND CUMULATIVE YIELDS FROM SPONTANEOUS FISSION OF 254CF.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION	
93 CHAIN	13467 6.900E+01	10.0				6.900E+01	10.0	
97 CHAIN	13467 8.900E+01	10.0				8.900E+01	10.0	
99 CHAIN	13467 2.000E+00	10.0				2.000E+00	10.0	
105 CHAIN	13467 4.800E+00	10.0				4.800E+00	10.0	
109 CHAIN	13467 5.600E+00	13.0				5.600E+00	13.0	
111 CHAIN	13467 5.300E+00	10.0				5.300E+00	10.0	
112 CHAIN	13467 4.400E+00	10.0				4.400E+00	10.0	
113 CHAIN	13467 5.200E+00	10.0				5.200E+00	10.0	
115 CHAIN	13467 3.200E+00	10.0				3.200E+00	10.0	
131 CHAIN	13467 2.600E+00	10.0				2.600E+00	10.0	
132 CHAIN	13467 2.900E+00	10.0				2.900E+00	10.0	
133 CHAIN	13467 4.900E+00	10.0				4.900E+00	10.0	
134 CHAIN	13467 5.400E+00	10.0				5.400E+00	10.0	
135 CHAIN	13467 4.600E+00	13.0				4.600E+00	13.0	
139 CHAIN	13467 5.700E+00	10.0				5.700E+00	10.0	
140 CHAIN	13467 5.900E+00	10.0				5.900E+00	10.0	
141 CHAIN	13467 5.300E+00	13.0				5.300E+00	13.0	
143 CHAIN	13467 5.900E+00	10.0				5.900E+00	10.0	
145 CHAIN	13467 5.600E+00	18.0				5.600E+00	18.0	
147 CHAIN	13467 4.700E+00	10.0				4.700E+00	10.0	
149 CHAIN	13467 3.000E+00	10.0				3.000E+00	10.0	
151 CHAIN	13467 2.600E+00	12.0				2.600E+00	12.0	
153 CHAIN	13467 1.500E+00	10.0				1.500E+00	10.0	
157 CHAIN	13467 6.000E+01	10.0				6.000E+01	10.0	

TABLE 67 CHAIN AND CUMULATIVE YIELDS FROM SPONTANEOUS FISSION OF 253ES.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION	
83 SR	926 6.110E-02	9.8				6.110E-02	9.8	
89 SR	926 3.660E-01	10.1				3.660E-01	10.1	
91 SR	926 5.280E-01	7.0				5.280E-01	7.0	
93 I	926 6.740E-01	9.9				6.740E-01	9.9	
95 ZR	926 1.130E+00	17.7				1.130E+00	17.7	
97 ZR	926 1.840E+00	4.9				1.840E+00	4.9	
99 MO	926 3.090E+00	4.8				3.090E+00	4.8	
103 RU	926 5.830E+00	5.0				5.830E+00	5.0	
105 RU	926 6.180E+00	15.0				6.180E+00	15.0	
106 RU	926 6.450E+00	7.4				6.450E+00	7.4	
109 PD	926 5.470E+00	10.1				5.470E+00	10.1	
111 AG	926 4.690E+00	5.1				4.690E+00	5.1	
112 PD	926 3.770E+00	10.1				3.770E+00	10.1	
115 CD(G)	926 2.610E+00	5.0	2.610E+00	0.00				
CD(M)	926 2.120E-01	5.7	2.120E-01	0.00				
CHAIN	926 2.820E+00	5.0	2.820E+00	0.00				
121 SN	926 1.390E-01	10.1				1.600E-01	10.0	
CHAIN	926 1.600E-01	10.0						
125 SN	926 9.180E-03	9.8				1.930E-02	10.4	
CHAIN	926 1.930E-02	10.4						
127 SB	926 6.390E-02	9.4				6.390E-02	9.4	
129 SB	926 3.130E-01	7.7				3.130E-01	7.7	
131 TE	926 1.150E+00	10.4				1.150E+00	10.4	
132 TE	926 2.400E+00	10.0				2.400E+00	10.0	
133 I	926 2.680E+00	10.1				2.680E+00	10.1	
135 I	926 3.900E+00	10.0				3.900E+00	10.0	
139 BA	926 5.930E+00	10.1				5.930E+00	10.1	
140 BA	926 5.620E+00	5.0				5.620E+00	5.0	
141 CE	926 5.810E+00	10.0				5.810E+00	10.0	
143 CE	926 6.480E+00	4.9				6.480E+00	4.9	
144 CE	926 5.160E+00	10.1				5.160E+00	10.1	
149 PM	926 3.170E+00	10.1				3.170E+00	10.1	
151 PM	926 1.930E+00	9.8				1.930E+00	9.8	
153 SM	926 1.500E+00	10.0				1.500E+00	10.0	
157 EU	926 7.500E-01	10.7				7.500E-01	10.7	
159 GD	926 5.700E-01	10.5				5.700E-01	10.5	

TABLE 68 CHAIN AND CUMULATIVE YIELDS FROM SPONTANEOUS FISSION OF 254Fm.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD.	COMPONENT VALUE	COMPONENT	EXTERNAL	INTERNAL	EXT./DF	MEAN	DEVIATION		
88 CHAIN	759	8.000E-02	10.0					8.000E-02	10.0		
91 SR	10642	3.800E-01	10.5					3.800E-01	10.5		
93 Y	10642	4.800E-01	10.4					4.800E-01	10.4		
95 ZR	10642	5.400E-01	14.8	0.21			0.04	0.04	5.259E-01	(I)	8.3A
CHAIN	759	5.200E-01	10.0	-0.21						(E)	1.7
97 ZR	10642	1.350E+00	9.6	0.91			0.82	0.82	1.263E+00	(I)	7.0A
CHAIN	759	1.190E+00	10.0	-0.91						(E)	6.3
99 CHAIN	759	1.540E+00	10.0					1.540E+00	10.0		
103 RU	10642	3.130E+00	9.9	-0.18			0.03	0.03	3.169E+00	(I)	7.0A
CHAIN	759	3.210E+00	10.0	0.18						(E)	1.3
105 CHAIN	759	4.910E+00	10.0					4.910E+00	10.0		
106 RU	10642	5.750E+00	10.1	1.43			2.06	2.06	5.101E+00	(I)	7.1 >2
CHAIN	759	4.680E+00	10.0	-1.43						(E)	10.2A
109 PD	10642	5.670E+00	10.1					5.670E+00	10.1		
111 AG	10642	5.500E+00	5.5					5.500E+00	5.5		
112 PD	10642	5.060E+00	10.1					6.420E+00	10.0		
CHAIN	759	6.420E+00	10.0								
115 CD(G)	10642	4.470E+00	9.8	4.470E+00	0.00	0.00	0.01	0.01	5.078E+00	(I)	5.9A
CD(M)	10642	5.800E-01	10.3	5.800E-01	0.00	0.00				(E)	0.5
CHAIN	2014	5.100E+00	7.8	5.100E+00	0.00	0.00					
121 SN(G)	10642	6.660E-01	10.1	-0.90			0.81	0.81	7.049E-01	(I)	7.3A
CHAIN	2014	7.600E-01	10.5	0.90						(E)	6.6
125 SN(G)	10642	6.600E-02	10.6					6.600E-02	10.6		
127 SB	10642	2.400E-01	12.5	-0.74			0.55	0.55	2.566E-01	(I)	7.8A
CHAIN	759	2.700E-01	10.0	0.74						(E)	5.8
129 SB	10642	8.600E-01	10.2					8.600E-01	10.2		
131 I	10642	2.580E+00	10.1	0.72			0.51	0.51	2.441E+00	(I)	7.1A
CHAIN	759	2.330E+00	10.0	-0.72						(E)	5.1
132 TE	10642	3.020E+00	9.9	0.21			0.05	0.05	2.974E+00	(I)	7.0A
CHAIN	759	2.930E+00	10.0	-0.21						(E)	1.5
133 I	10642	3.290E+00	10.0					4.740E+00	10.0		
CHAIN	759	4.740E+00	10.0								
135 CHAIN	759	4.300E+00	10.0					4.300E+00	10.0		
139 CHAIN	759	5.130E+00	10.0					5.130E+00	10.0		
140 BA	10642	5.490E+00	10.0	0.66			0.44	0.44	5.222E+00	(I)	7.1A
CHAIN	759	5.000E+00	10.0	-0.66						(E)	4.7
141 CE	10642	6.290E+00	8.0	2.03			4.14	4.14	5.561E+00	(I)	6.3 >2
CHAIN	759	4.870E+00	10.0	-2.03						(E)	12.8A
142 CHAIN	759	5.140E+00	10.0					5.140E+00	10.0		
143 CE	10642	5.640E+00	5.3	1.89			3.59	3.59	5.330E+00	(I)	4.7 >2
CHAIN	759	4.600E+00	10.0	-1.89						(E)	8.9A
144 CE	10642	5.090E+00	9.8	1.23			1.52	1.52	4.623E+00	(I)	7.0
CHAIN	759	4.280E+00	10.0	-1.23						(E)	8.7A
147 CHAIN	759	3.560E+00	10.0					3.560E+00	10.0		

TABLE 68 CHAIN AND CUMULATIVE YIELDS FROM SPONTANEOUS FISSION OF 254Fm. (CONT.)

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD.	COMPONENT VALUE	COMPONENT	EXTERNAL	INTERNAL	EXT./DF	MEAN	DEVIATION		
149 CHAIN	759	2.980E+00	10.0					2.980E+00	10.0		
153 SM	10642	1.420E+00	9.9					1.420E+00	9.9		
157 EU	10642	6.200E-01	9.7					6.200E-01	9.7		
159 GD	10642	4.400E-01	9.1					4.400E-01	9.1		

TABLE 69 CHAIN AND CUMULATIVE YIELDS FROM SPONTANEOUS FISSION OF 256FM.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	YIELDS & SD	NO.	YIELDS & SD	COMPONENT VALUE	EXT.	INT.	EXT./DF	INT.	EXT./DF	MEAN	DEVIATION
1 H	PI 2048 7.00E-03	30.0						7.00E-03	30.0		
3 H	PI 2048 3.90E-02	15.0						3.90E-02	15.0		
4 HE	PI 2048 4.62E-01	15.0	-0.21		0.05	0.05	4.74E-01	(I) 8.3A			
		2814 4.80E-01	0.21					(E) 1.8			
91 SR	686 2.40E-01	12.5						2.40E-01	12.5		
97 ZR	686 7.50E-01	20.0						7.50E-01	20.0		
105 RU	686 3.10E+00	12.9						3.10E+00	12.9		
109 PD	686 3.60E+00	27.8						3.60E+00	27.8		
111 AG	686 5.40E+00	7.4						5.40E+00	7.4		
112 PD	2014 4.40E+00	13.6	-0.35		0.12	0.12	4.55E+00	(I) 9.3A			
AG	686 4.70E+00	12.8	0.35					(E) 3.3			
113 AG	686 4.00E+00	7.5						4.00E+00	7.5		
115 CD(G)	2014 5.20E+00	9.6	-0.51		0.26	0.26	5.36E+00	(I) 7.2A			
CHAIN	2014 5.60E+00	10.7	0.51					(E) 3.7			
118 CD	686 5.70E+00	17.5						5.70E+00	17.5		
121 SN(G)	2014 2.10E+00	9.5						2.50E+00	12.0		
CHAIN	2014 2.50E+00	12.0									
125 SN(G)	2014 5.60E-01	35.7						5.60E-01	35.7		
127 SB	686 4.40E-01	18.2						4.40E-01	18.2		
129 SB	686 8.80E-01	17.0						8.80E-01	17.0		
131 I	686 2.60E+00	19.2						2.60E+00	19.2		
132 TE	686 3.90E+00	12.8						3.90E+00	12.8		
133 I	686 3.90E+00	20.5						3.90E+00	20.5		
135 I	686 5.40E+00	18.5						5.40E+00	18.5		
139 BA	686 6.20E+00	12.9						6.20E+00	12.9		
140 BA	686 6.00E+00	8.3						6.00E+00	8.3		
141 LA	686 7.10E+00	19.7						7.10E+00	19.7		
143 CE	686 6.10E+00	8.2						6.10E+00	8.2		
145 PR	686 5.20E+00	19.2						5.20E+00	19.2		
149 PM	686 2.70E+00	14.8						2.70E+00	14.8		
151 PM	686 2.10E+00	14.3						2.10E+00	14.3		
153 SM	686 1.40E+00	21.4						1.40E+00	21.4		
155 SM	686 7.10E+00	28.6						7.10E+00	28.6		
157 EU	686 5.30E-01	13.2						5.30E-01	13.2		
159 GD	686 5.00E-01	14.0						5.00E-01	14.0		

TABLE 70 CHAIN AND CUMULATIVE YIELDS FROM SPONTANEOUS FISSION OF 257FM.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	YIELDS & SD	NO.	YIELDS & SD	COMPONENT VALUE	EXT.	INT.	EXT./DF	INT.	EXT./DF	MEAN	DEVIATION
4 HE	PI 2048 3.76E-01	10.0						3.76E-01	10.0		
	2814 4.30E-01	10.0						4.30E-01	10.0		
								-0.95	0.89	0.89	3.994E-01 (E) 6.7

TABLE 71 CHAIN AND CUMULATIVE YIELDS FROM 2.000E+06 eV FISSION IN 232TH.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED	STANDARD
NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION			
83 SE(M)	1162 9.300E+01	23.0				9.300E+01	23.0			
84 BR(G)	1162 4.540E+00	11.0				4.540E+00	11.0			
85 KR(M)	1162 5.130E+00	4.1								
87 KR	1162 7.370E+00	4.6				7.370E+00	4.6			
88 KR	1162 6.930E+00	4.2				6.930E+00	4.2			
89 RB	1162 7.700E+00	8.3				7.700E+00	8.3			
91 SR	1162 7.820E+00	3.1				7.820E+00	3.1			
92 SR	1162 7.240E+00	12.0				7.240E+00	12.0			
93 Y	1162 5.610E+00	7.0				5.610E+00	7.0			
94 Y	1162 5.790E+00	6.2				5.790E+00	6.2			
97 ZR	1162 4.500E+00	2.7				4.500E+00	2.7			
99 MO	1162 2.870E+00	5.9				2.870E+00	5.9			
101 TC	1162 8.200E-01	18.3				8.200E-01	18.3			
111 AG	1162 4.000E-03	100.0				4.000E-03	100.0			
115 CD(G)	1162 5.000E-03	20.0				5.000E-03	20.0			
127 SB	1162 3.000E-03	33.0				3.000E-03	33.0			
129 SB	1162 1.100E-01	18.0				1.100E-01	18.0			
131 I	1162 1.400E+00	5.0				1.400E+00	5.0			
132 TE	1162 2.740E+00	5.0				2.740E+00	5.0			
133	1162 4.110E+00	5.0								
134 TE	1162 6.970E+00	6.3				6.970E+00	6.3			
135 I	1162 5.920E+00	5.0				5.920E+00	5.0			
136 CS	1162 6.360E+00	5.0				6.360E+00	5.0			
139 BA	1162 8.340E+00	7.7				8.340E+00	7.7			
140 BA	1162 8.950E+00	5.0				8.950E+00	5.0			
141 BA	1162 8.900E+00	5.1				8.900E+00	5.1			
142 LA	1162 7.230E+00	5.3				7.230E+00	5.3			
143 CE	1162 6.790E+00	5.6				6.790E+00	5.6			
146 CE	1162 4.450E+00	14.6				4.450E+00	14.6			
147 ND	1162 3.400E+00	28.5				3.400E+00	28.5			
149 ND	1162 1.380E+00	15.2				1.380E+00	15.2			

TABLE 72 CHAIN AND CUMULATIVE YIELDS FROM 2.500E+06 eV FISSION IN 232TH.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED	STANDARD
NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION			
4 HE PI	2050 8.403E-02	40.0				8.403E-02	40.0			

TABLE 73 CHAIN AND CUMULATIVE YIELDS FROM 3.000E+06 eV FISSION IN 232TH.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION		
77 AS	634	1.00E-02	50.0					1.00E-02	50.0		
78 AS	634	3.60E-02	12.0					3.60E-02	12.0		
79 AS	634	7.50E-02	11.0					7.50E-02	11.0		
81 AS	634	5.00E-02	10.0					5.00E-02	10.0		
83 SE(M)	1163	1.120E+00	18.0					2.130E+00	7.0		
BR	622	2.130E+00	7.0								
84 SR	622	3.230E+00	17.0	-1.43		2.05	2.05	3.350E+00	(I) 6.2	>2	
85 KR(M)	1163	4.380E+00	3.9								
87 KR	1163	6.860E+00	4.8					6.860E+00	4.8		
88 KR	1163	6.640E+00	4.0					6.640E+00	4.0		
89 RB	1163	7.570E+00	8.9					7.570E+00	8.9		
91 SR	50	6.190E+00	10.0	-2.20		6.11	3.05	7.481E+00	(I) 2.7	>2	
	1163	7.710E+00	2.9	2.35					(E) 4.7A		
Y	634	6.900E+00	10.0	-0.88							
92 SR	50	6.390E+00	10.0	-0.77		0.59	0.59	6.679E+00	(I) 7.7A		
	1163	7.230E+00	12.2	0.77					(E) 6.0		
93 Y	634	7.340E+00	10.0					7.340E+00	10.0		
94 Y	1163	6.070E+00	11.0					6.070E+00	11.0		
97 ZR	1163	4.870E+00	3.1	-0.53		0.75	0.38	4.910E+00	(I) 2.7A		
	622	5.350E+00	10.0	0.85					(E) 1.6		
CHAIN	913	4.930E+00	6.0	0.07							
99 MO	1163	3.150E+00	5.8					3.150E+00	5.8		
101 TC	1163	1.080E+00	11.0					1.080E+00	11.0		
102 RU	1163	1.500E+00	100.0					1.500E+00	100.0		
105 RU	1163	1.100E-02	100.0					1.100E-02	100.0		
109 PD	1163	1.600E-02	44.0					1.600E-02	44.0		
111 AG	1163	2.700E-02	11.0					2.700E-02	11.0		
112 PD	1163	2.800E-02	14.3					2.800E-02	14.3		
113 AG	50	4.500E-02	20.0					4.500E-02	20.0		
115 CD(G)	1163	2.300E-02	17.4					2.300E-02	17.4		
129*SB	622	1.600E-01	10.0W	2.29		6.91	3.45	1.363E-01	(I) 8.9	>2	
	1163	2.000E-01	25.0	1.32					(E) 16.5A		
	1163	9.000E-02	22.0W	-2.18							
131 I	1163	1.370E+00	13.0	-4.60							
	50	1.370E+00	13.0	4.60							
132*TE	1163	3.250E+00	2.8W	0.50							
	622	3.370E+00	10.0	0.93							
I	50	2.420E+00	8.0W	-2.35							
133*I	50	3.150E+00	11.0W	-2.40		5.91	2.95	4.624E+00	(I) 2.8	>2	
	1163	4.850E+00	3.1W	0.64					(E) 4.8A		
CHAIN	913	4.990E+00	8.0	1.25							
134 TE	1163	7.440E+00	10.2	0.04		0.00	0.00	7.419E+00	(I) 7.8A		
I	50	7.390E+00	12.0	-0.04							
135 I	50	5.390E+00	12.0	-1.59		2.61	1.31	6.235E+00	(I) 5.9		
	1163	6.180E+00	28.0	-0.03					(E) 6.8A		
CHAIN	913	6.680E+00	7.0	1.56							
138 CS	1163	6.290E+00	4.3					6.290E+00	4.3		
139 BA	50	6.560E+00	7.0	-1.20		1.44	1.44	6.864E+00	(I) 5.6		

TABLE 73 CHAIN AND CUMULATIVE YIELDS FROM 3.000E+06 eV FISSION IN 232TH.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION		
140 BA	1163	8.600E+00	2.7					8.600E+00	2.7		
141 BA	1163	7.690E+00	5.3	1.41				1.97	1.97	7.389E+00	(I) 4.7
CE	634	6.600E+00	10.0	-1.41							(E) 6.6A
142 LA	1163	6.610E+00	5.9					6.610E+00	5.9		
143 CE	634	6.000E+00	10.0	-0.74		0.66	0.33	6.405E+00	(I) 3.9A		
	1163	6.450E+00	4.7	0.26					(E) 2.2		
	622	6.690E+00	10.0	0.46							
145 PR	634	4.700E+00	10.0	-0.83		0.70	0.70	4.960E+00	(I) 7.1A		
	622	5.290E+00	10.0	0.83					(E) 5.9		
146 CE	1163	3.710E+00	19.0					3.710E+00	19.0		
147 ND	1163	3.320E+00	14.8	-2.08		4.33	4.33	2.367E+00	(E) 17.5A	>2	
	1163	3.320E+00	14.8	2.08							
149 ND	1163	1.060E+00	15.1	0.32		0.10	0.10	1.017E+00	(I) 8.3A		
PM	634	1.000E+00	10.0	-0.32							(E) 2.7
151 PM	634	1.000E-01	20.0					1.000E-01	20.0		
153 SM	634	3.000E-02	13.0					3.000E-02	13.0		
156 SM	634	1.300E-03	40.0					1.300E-03	40.0		

TABLE 74 CHAIN AND CUMULATIVE YIELDS FROM 4.000E+06 eV FISSION IN 232TH.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	YIELDS & SD	COMPONENT	VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION		
83 SE(M)	1164 9.100E+01	16.5					9.100E+01	26.5		
84 BR(G)	1164 1.500E+01	26.6					1.500E+01	26.6		
85 KR(M)	1164 4.170E+00	3.8								
87 KR	1164 6.210E+00	4.8					6.210E+00	4.8		
88 KR	1164 6.160E+00	4.1					6.160E+00	4.1		
89 RB	1164 7.180E+00	8.1					7.180E+00	8.1		
91 SR	1164 7.300E+00	2.9					7.300E+00	2.9		
92 SR	1164 6.930E+00	12.4					6.930E+00	12.4		
93 Y	1164 5.680E+00	6.7					5.680E+00	6.7		
94 Y	1164 6.200E+00	5.6					6.200E+00	5.6		
97 ZR	1164 4.850E+00	2.7					4.850E+00	2.7		
99 MO	1164 3.410E+00	4.4					3.410E+00	4.4		
101 TC	1164 1.250E+00	5.8					1.250E+00	5.8		
103 RU	1164 1.500E+01	26.6					1.500E+01	26.6		
105 RU	1164 3.700E+02	10.8					3.700E+02	10.8		
109 PD	1164 3.600E+02	13.9					3.600E+02	13.9		
111 AG	1164 7.600E+02	10.3					7.600E+02	10.3		
112 PD	1164 9.700E+02	11.3					9.700E+02	11.3		
115 CD(G)	1164 9.900E+02	15.0					9.900E+02	15.0		
127 SB	1164 5.600E+02	19.6					5.600E+02	19.6		
129 SB	1164 3.200E+01	18.8					3.200E+01	18.8		
SB(G)	1164 3.400E+01	14.7					3.400E+01	14.7		
131 I	1164 2.130E+00	3.8					2.130E+00	3.8		
132 TE	1164 3.420E+00	2.9					3.420E+00	2.9		
133 I	1164 5.190E+00	3.3					5.190E+00	3.3		
134 TE	1164 7.680E+00	7.9					7.680E+00	7.9		
135 I	1164 6.120E+00	2.8					6.120E+00	2.8		
138 CS(G)	1164 6.180E+00	5.7					6.180E+00	5.7		
139 BA	1164 7.560E+00	7.9					7.560E+00	7.9		
140 BA	1164 8.010E+00	2.5					8.010E+00	2.5		
141 BA	1164 8.140E+00	5.0					8.140E+00	5.0		
142 LA	1164 6.270E+00	5.7					6.270E+00	5.7		
145 CE	1164 5.970E+00	8.9					5.970E+00	8.9		
146 CE	1164 3.330E+00	12.9					3.330E+00	12.9		
147 ND	1164 2.640E+00	13.9					2.640E+00	13.9		
149 ND	1164 1.100E+00	13.6					1.100E+00	13.6		

TABLE 75 CHAIN AND CUMULATIVE YIELDS FROM 5.900E+06 eV FISSION IN 232TH.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	YIELDS & SD	COMPONENT	VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION		
84 BR(G)	1165 4.020E+00	19.0					4.020E+00	19.0		
85 KR(G)	1165 4.000E+00	5.0								
87 KR	1165 5.280E+00	5.9					5.280E+00	5.9		
88 KR	1165 5.710E+00	4.7					5.710E+00	4.7		
89 RB	1165 7.490E+00	13.4					7.490E+00	13.4		
91 SR	1165 6.630E+00	3.2					6.630E+00	3.2		
92 SR	1165 6.560E+00	13.1					6.560E+00	13.1		
93 Y	1165 4.850E+00	10.1					4.850E+00	10.1		
97 ZR	1165 4.800E+00	2.7					4.800E+00	2.7		
99 MO	1165 3.790E+00	6.1					3.790E+00	6.1		
101 TC	1165 1.770E+00	12.4					1.770E+00	12.4		
103 RU	1165 6.700E+01	14.9					6.700E+01	14.9		
105 RU	1165 2.400E+01	20.8					2.400E+01	20.8		
109 PD	1165 1.900E+01	15.8					1.900E+01	15.8		
111 AG	1165 2.900E+01	10.3					2.900E+01	10.3		
112 PD	1165 3.000E+01	13.3					3.000E+01	13.3		
115 CD(G)	1165 2.700E+01	14.8					2.700E+01	14.8		
121 SN(G)	1165 1.900E+01	15.8					1.900E+01	15.8		
127 SB	1165 2.200E+01	18.2					2.200E+01	18.2		
129 SB	1165 1.400E+01	20.3					1.400E+01	20.3		
SB(G)	1165 9.000E+01	14.4					9.000E+01	14.4		
131 I	1165 2.750E+00	5.8					2.750E+00	5.8		
132 TE	1165 8.000E+00	6.6					8.000E+00	6.6		
133 I	1165 5.640E+00	3.4					5.640E+00	3.4		
134 TE	1165 8.080E+00	6.6					8.080E+00	6.6		
135 I	1165 5.960E+00	3.2					5.960E+00	3.2		
138 CS	1165 5.930E+00	4.7					5.930E+00	4.7		
139 BA	1165 7.240E+00	12.2					7.240E+00	12.2		
140 BA	1165 7.750E+00	7.1					7.750E+00	7.1		
141 BA	1165 7.370E+00	7.5					7.370E+00	7.5		
142 LA	1165 5.760E+00	7.5					5.760E+00	7.5		
143 CE	1165 5.590E+00	6.3					5.590E+00	6.3		
146 CE	1165 3.070E+00	36.0					3.070E+00	36.0		
149 ND	1165 1.450E+00	24.0					1.450E+00	24.0		

TABLE 76 CHAIN AND CUMULATIVE YIELDS FROM 6.400E+06 eV FISSION IN 232TH.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED	STANDARD
NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION		
77 AS	1166 3.900E+02	15.4				3.900E+02	15.4		
78 AS	1166 6.500E+02	15.4				6.500E+02	15.4		
83 SE(M)	1166 1.250E+00	21.6				1.250E+00	21.6		
84 BR(G)	1166 5.340E+00	12.2				5.340E+00	12.2		
85 KR(M)	1166 5.700E+00	3.9							
88 KR	1166 6.460E+00	3.9				6.460E+00	3.9		
89 RB	1166 7.970E+00	8.9				7.970E+00	8.9		
91 SR	1166 6.930E+00	2.3				6.930E+00	2.3		
92 SR	1166 6.260E+00	12.2				6.260E+00	12.2		
93 Y	1166 4.710E+00	7.9				4.710E+00	7.9		
94 Y	1166 4.750E+00	19.6				4.750E+00	19.6		
97 ZR	1166 3.380E+00	3.3				3.380E+00	3.3		
99 MO	1166 2.600E+00	5.0				2.600E+00	5.0		
101 TC	1166 1.220E+00	12.3				1.220E+00	12.3		
103 RU	1166 1.600E+01	25.0				1.600E+01	25.0		
105 RU	1166 1.300E+01	15.4				1.300E+01	15.4		
109 PD	1166 1.400E+01	21.4				1.400E+01	21.4		
111 AG	1166 2.000E+01	15.0				2.000E+01	15.0		
112 PD	1166 2.400E+01	16.8				2.400E+01	16.8		
115 CD(G)	1166 2.300E+01	17.2				2.300E+01	17.2		
121 SN(G)	1166 1.400E+01	21.4				1.400E+01	21.4		
127 SB	1166 1.800E+01	16.7				1.800E+01	16.7		
129 SB	1166 6.100E+01	14.8				6.100E+01	14.8		
131 I	1166 2.010E+00	4.5				2.010E+00	4.5		
132 TE	1166 2.980E+00	9.0				2.980E+00	9.0		
133 I	1166 4.510E+00	3.3				4.510E+00	3.3		
134 TE	1166 6.330E+00	6.3				6.330E+00	6.3		
135 I	1166 5.420E+00	29.0				5.420E+00	29.0		
138 CS	1166 6.040E+00	6.0				6.040E+00	6.0		
139 BA	1166 7.050E+00	9.8				7.050E+00	9.8		
140 BA	1166 8.080E+00	2.8				8.080E+00	2.8		
142 LA	1166 6.510E+00	6.5				6.510E+00	6.5		
143 CE	1166 6.660E+00	6.0				6.660E+00	6.0		
146 CE	1166 3.670E+00	6.9				3.670E+00	6.9		
147 ND	1166 3.020E+00	21.2				3.020E+00	21.2		
149 ND	1166 1.170E+00	25.6				1.170E+00	25.6		

TABLE 77 CHAIN AND CUMULATIVE YIELDS FROM 6.900E+06 eV FISSION IN 232TH.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED	STANDARD
NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION		
83 SE(M)	1167 1.440E+00	18.1				1.440E+00	18.1		
84 BR(G)	1167 5.500E+00	12.9				5.500E+00	12.9		
85 KR(M)	1167 6.820E+00	4.8							
87 KR	1167 7.610E+00	5.1				7.610E+00	5.1		
88 KR	1167 7.550E+00	4.5				7.550E+00	4.5		
89 RB	1167 6.980E+00	9.5				6.980E+00	9.5		
91 SR	1167 7.280E+00	7.2				7.280E+00	7.2		
92 SR	1167 6.460E+00	12.5				6.460E+00	12.5		
93 Y	1167 5.210E+00	8.4				5.210E+00	8.4		
94 Y	1167 4.790E+00	26.2				4.790E+00	26.2		
97 ZR	1167 3.500E+00	2.9				3.500E+00	2.9		
99 MO	1167 2.090E+00	7.7				2.090E+00	7.7		
101 TC	1167 7.800E+01	41.0				7.800E+01	41.0		
105 RU	1167 1.800E+01	16.7				1.800E+01	16.7		
109 PD	1167 1.300E+01	15.4				1.300E+01	15.4		
111 AG	1167 1.700E+01	11.8				1.700E+01	11.8		
112 PD	1167 1.800E+01	16.7				1.800E+01	16.7		
115 CD(G)	1167 2.000E+01	15.0				2.000E+01	15.0		
127 SB	1167 1.500E+01	20.0				1.500E+01	20.0		
129 SB	1167 3.700E+01	19.0				3.700E+01	19.0		
131 I	1167 1.670E+00	6.0				1.670E+00	6.0		
132 TE	1167 2.720E+00	4.0				2.720E+00	4.0		
133 I	1167 4.230E+00	3.3				4.230E+00	3.3		
134 TE	1167 6.620E+00	6.2				6.620E+00	6.2		
135 I	1167 5.420E+00	3.0				5.420E+00	3.0		
138 CS	1167 6.150E+00	6.0				6.150E+00	6.0		
139 BA	1167 8.160E+00	9.4				8.160E+00	9.4		
140 BA	1167 8.700E+00	4.0				8.700E+00	4.0		
141 BA	1167 8.000E+00	10.4				8.000E+00	10.4		
142 LA	1167 7.550E+00	12.5				7.550E+00	12.5		
143 CE	1167 7.670E+00	6.0				7.670E+00	6.0		
146 CE	1167 3.130E+00	14.7				3.130E+00	14.7		
147 ND	1167 3.110E+00	18.3				3.110E+00	18.3		
149 ND	1167 1.290E+00	17.1				1.290E+00	17.1		

TABLE 78 CHAIN AND CUMULATIVE YIELDS FROM 7.600E+06 eV FISSION IN 232TH.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION	
77 AS	1168 2.900E+02	13.8				2.900E+02	13.8	
78 AS	1168 7.800E+02	15.4				7.800E+02	15.4	
83 SE(M)	1168 1.380E+00	15.9				1.380E+00	15.9	
84 BR(G)	1168 5.050E+00	11.9				5.050E+00	11.9	
85 KR(M)	1168 6.010E+00	4.2				6.010E+00	4.2	
87 KR	1168 7.100E+00	4.9				7.100E+00	4.9	
88 KR	1168 7.030E+00	4.3				7.030E+00	4.3	
89 RB	1168 7.070E+00	9.1				7.070E+00	9.1	
91 SR	1168 7.150E+00	2.9				7.150E+00	2.9	
92 SR	1168 6.450E+00	12.1				6.450E+00	12.1	
93 Y	1168 5.260E+00	7.2				5.260E+00	7.2	
94 Y	1168 5.580E+00	11.8				5.580E+00	11.8	
97 ZR	1168 3.620E+00	3.6				3.620E+00	3.6	
99 MO	1168 2.210E+00	5.9				2.210E+00	5.9	
101 TC	1168 1.000E+00	12.0				1.000E+00	12.0	
109 PD	1168 1.800E+01	22.2				1.800E+01	22.2	
111 AG	1168 2.200E+01	13.6				2.200E+01	13.6	
112 PD	1168 2.600E+01	15.4				2.600E+01	15.4	
115 CD(G)	1168 2.000E+01	15.0				2.000E+01	15.0	
127 SB	1168 2.000E+01	15.0				2.000E+01	15.0	
129 SB(G)	1168 4.800E+01	14.6	-0.30		0.09	4.950E+01	(I) 10.0A	
131 I	1168 1.760E+00	4.5	0.30			1.760E+00	(E) 3.0	
132 TE	1168 2.780E+00	4.0				2.780E+00	4.0	
133 I	1168 4.340E+00	3.2				4.340E+00	3.2	
134 TE	1168 6.800E+00	7.5				6.800E+00	7.5	
135 I	1168 5.490E+00	2.9				5.490E+00	2.9	
138 CS	1168 5.850E+00	5.6				5.850E+00	5.6	
139 BA	1168 7.490E+00	8.4				7.490E+00	8.4	
140 BA	1168 8.380E+00	2.7				8.380E+00	2.7	
141 BA	1168 7.640E+00	8.0				7.640E+00	8.0	
142 BA	1168 7.010E+00	6.2				7.010E+00	6.2	
143 CE	1168 6.950E+00	5.9				6.950E+00	5.9	
146 CE	1168 3.300E+00	16.1				3.300E+00	16.1	
148 ND	1168 3.110E+00	8.3				3.110E+00	8.3	
149 ND	1168 1.020E+00	21.6				1.020E+00	21.6	

TABLE 79 CHAIN AND CUMULATIVE YIELDS FROM 8.000E+06 eV FISSION IN 232TH.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION	
83 SE(M)	1169 1.850E+00	15.1				1.850E+00	15.1	
84 BR(G)	1169 5.470E+00	9.7				5.470E+00	9.7	
85 KR(M)	1169 5.810E+00	3.4				5.810E+00	3.4	
87 KR	1169 3.440E+00	4.0				3.440E+00	4.0	
88 KR	1169 6.710E+00	11.2				6.710E+00	11.2	
89 RB	1169 7.760E+00	10.8				7.760E+00	10.8	
91 SR	1169 7.150E+00	2.8				7.150E+00	2.8	
92 SR	1169 6.620E+00	12.2				6.620E+00	12.2	
93 Y	1169 5.010E+00	7.8				5.010E+00	7.8	
94 Y	1169 5.190E+00	7.5				5.190E+00	7.5	
97 ZR	1169 3.590E+00	2.8				3.590E+00	2.8	
99 MO	1169 2.250E+00	10.2				2.250E+00	10.2	
101 TC	1169 1.080E+00	13.9				1.080E+00	13.9	
109 PD	1169 1.800E+01	22.2				1.800E+01	22.2	
111 AG	1169 2.800E+01	10.7				2.800E+01	10.7	
112 PD	1169 2.800E+01	17.9				2.800E+01	17.9	
115 CD(G)	1169 2.900E+01	13.8				2.900E+01	13.8	
127 SB	1169 2.600E+01	19.2				2.600E+01	19.2	
129 SB(G)	1169 4.000E+01	20.0	-1.62		2.62	4.763E+01	(I) 13.6 >2	
131 I	1169 1.690E+00	5.3	1.62			1.690E+00	5.3	
132 TE	1169 2.770E+00	3.2				2.770E+00	3.2	
133 I	1169 4.320E+00	2.8				4.320E+00	2.8	
134 TE	1169 7.160E+00	4.5				7.160E+00	4.5	
135 I	1169 5.580E+00	2.7				5.580E+00	2.7	
138 CS	1169 5.950E+00	5.7				5.950E+00	5.7	
139 BA	1169 6.610E+00	10.7				6.610E+00	10.7	
140 BA	1169 7.870E+00	4.4				7.870E+00	4.4	
141 BA	1169 7.220E+00	7.8				7.220E+00	7.8	
142 LA	1169 6.840E+00	5.3				6.840E+00	5.3	
143 CE	1169 6.940E+00	4.8				6.940E+00	4.8	
146 CE	1169 3.880E+00	12.6				3.880E+00	12.6	
147 CE	1169 2.800E+00	11.1				2.800E+00	11.1	
149 ND	1169 1.080E+00	15.7				1.080E+00	15.7	

TABLE 80 CHAIN AND CUMULATIVE YIELDS FROM 1.100E+07 eV FISSION IN 232TH.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT VALUE	EXT.	INT.	EXT./DF	INT.	DEVIATION
77 AS	614	2.200E-02	20.0					2.200E-02	20.0
91 SR	614	5.600E+00	20.0					5.600E+00	20.0
97 ZR	614	4.950E+00	20.0					4.950E+00	20.0
99 MO	614	3.100E+00	20.0					3.100E+00	20.0
103 RU	614	5.100E+00	20.0					5.100E+00	20.0
106 RU	614	5.300E+00	20.0					5.300E+00	20.0
111 AG	614	6.300E-01	20.0					6.300E-01	20.0
115 CD(G)	614	7.600E-01	20.0						
117 CD(G)	614	3.700E-01	50.0						
131 I	614	2.300E+00	20.0					2.300E+00	20.0
132 TE	614	1.800E+00	50.0					1.800E+00	50.0
139 BA	614	9.000E+00	20.0					9.000E+00	20.0
144 CE	614	7.200E+00	20.0					7.200E+00	20.0

TABLE 81 CHAIN AND CUMULATIVE YIELDS FROM 1.400E+07 eV FISSION IN 232TH.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT VALUE	EXT.	INT.	EXT./DF	INT.	DEVIATION
4 HE FI	2050	9.578E-02	40.0					9.578E-02	40.0

TABLE 82 CHAIN AND CUMULATIVE YIELDS FROM 3.000E+06 eV FISSION IN 231PA.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	VALUE	EXT./DF	EXT.	INT.	EXT./DF	DEVIATION
83 BR	75	2.580E+00	9.0						5.0
84 BR	75	3.910E+00	5.0						5.0
91 SR	75	5.890E+00	5.0						5.0
97 ZK	75	3.960E+00	5.0						5.0
99 MO	75	2.570E+00	5.0						5.0
105 RU	75	2.400E-01	9.0						9.0
113 AG	75	7.200E-02	14.0						14.0
129 SB	75	9.200E-01	6.0						6.0
143 CE	75	5.200E+00	5.0						5.0
145 PR	75	3.220E+00	6.0						6.0

TABLE 83 CHAIN AND CUMULATIVE YIELDS FROM 3.300E+05 eV FISSION IN 233U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	VALUE	EXT./DF	EXT.	INT.	EXT./DF	DEVIATION
4 HE FI	205772	2.540E-01	10.8						10.8

TABLE 84 CHAIN AND CUMULATIVE YIELDS FROM 6.900E+05 eV FISSION IN 233U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	VALUE	EXTERNAL	INTERNAL	EXT./DF	DEVIATION
4 HE PI	2057r1	1.920E-01	10.8						1.920E-01

TABLE 85 CHAIN AND CUMULATIVE YIELDS FROM 1.160E+06 eV FISSION IN 233U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	VALUE	EXTERNAL	INTERNAL	EXT./DF	DEVIATION
4 HE PI	2057r1	1.838E-01	10.8						1.838E-01

TABLE 86 CHAIN AND CUMULATIVE YIELDS FROM 1.990E+06 eV FISSION IN 233U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT VALUE	INT. EXT./DF	INT. EXT./DF	INT. EXT./DF	INT. EXT./DF	DEVIATION
4 HE PI	2057r2	2.168E-01	10.8						10.8

TABLE 87 CHAIN AND CUMULATIVE YIELDS FROM 1.000E+06 eV FISSION IN 234U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT VALUE	INT. EXT./DF	INT. EXT./DF	INT. EXT./DF	INT. EXT./DF	DEVIATION
4 HE PI	858	2.146E-01	10.0						10.0

TABLE 88 CHAIN AND CUMULATIVE YIELDS FROM 1.100E+00 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT.	EXT./DF	INT.	DEVIATION
111 AG	13436	2.000E-02	20.0						2.000E-02
115 CD	13436	1.300E-02	20.0						1.300E-02
127 SB	13436	1.100E-01	20.0						1.100E-01

TABLE 89 CHAIN AND CUMULATIVE YIELDS FROM 3.100E+00 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT.	EXT./DF	INT.	DEVIATION
111 AG	13436	1.900E-02	20.0						1.900E-02
115 CD	13436	8.000E-03	20.0						8.000E-03

TABLE 90 CHAIN AND CUMULATIVE YIELDS FROM 4.850E+00 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT.	EXT./DF	INT.	DEVIATION
99 MO	312	5.450E+00	3.0						3.0
									5.450E+00

TABLE 91 CHAIN AND CUMULATIVE YIELDS FROM 9.500E+00 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT.	EXT./DF	INT.	DEVIATION
111 AG	13436	1.800E-02	20.0						20.0
									1.800E-02
115 CD	13436	1.000E-02	20.0						20.0
									1.000E-02

TABLE 92 CHAIN AND CUMULATIVE YIELDS FROM 9.500E-01 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
99 MO	312	6.100E+00	3.0					6.100E+00	3.0

TABLE 93 CHAIN AND CUMULATIVE YIELDS FROM 1.300E+05 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
99 MO	796	5.700E+00	6.9					5.700E+00	6.9
111 AG	797	1.500E-02	8.1					1.500E-02	8.1
140 BA	797	6.100E+00	6.6					6.100E+00	6.6
147 ND	797	2.350E+00	6.1					2.350E+00	6.1
153 SM	797	1.320E-01	9.9					1.320E-01	9.9

TABLE 94 CHAIN AND CUMULATIVE YIELDS FROM 1.500E+05 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
1 H PI	1199	2.567E-03	31.9				2.567E-03	31.9
3 H PI	1199	1.397E-02	30.2				1.397E-02	30.2
4 HE PI	1199	2.226E-01	30.2				2.226E-01	30.2

TABLE 95 CHAIN AND CUMULATIVE YIELDS FROM 1.700E+05 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
84 BR	12729	1.700E+00	15.3					
85 KR(M)	12729	1.350E+00	6.7					
87 KR	12729	2.380E+00	8.0					
88 KR	12729	3.290E+00	4.6					
89 RB	12729	4.270E+00	12.2					
91 SR	12729	5.820E+00	4.0				5.820E+00	4.0
92 SR	12729	5.780E+00	7.3					
93 Y	12729	6.640E+00	5.3				6.640E+00	5.3
95 ZR	12729	6.810E+00	5.3				6.810E+00	5.3
97 ZR	12729	5.910E+00	3.7					
99 MO	12729	5.940E+00	4.5				5.940E+00	4.5
103 RU	12729	3.600E+00	5.3				3.600E+00	5.3
105 RU	12729	1.110E+00	7.2				1.110E+00	7.2
109 PD	12729	2.700E-02	18.5				2.700E-02	18.5
111 AG	12729	1.600E-02	12.5				1.600E-02	12.5
112 PD	12729	1.200E-02	16.7					
115 CD	12729	1.000E-02	20.0				1.000E-02	20.0
121 SN	12729	9.000E-03	22.2				9.000E-03	22.2
125 SN	12729	9.000E-03	22.2					
127 SB	12729	1.300E-01	15.4					
129 SB	12729	8.900E-01	7.9					
131 I	12729	3.530E+00	5.1					
132 TE	12729	4.650E+00	4.3					
133 I	12729	6.630E+00	4.2					
134 TE	12729	6.180E+00	4.8					
135 I	12729	6.460E+00	3.9					
138 XE	12729	5.320E+00	5.8					
139 BA	12729	6.270E+00	7.3					
140 BA	12729	6.450E+00	5.3					
142 LA	12729	5.350E+00	6.7					
143 CE	12729	5.570E+00	4.7					
144 CE	12729	5.260E+00	11.2					
147 ND	12729	2.180E+00	8.3				2.180E+00	8.3
149 PM	12729	1.170E+00	9.4				1.170E+00	9.4
151 PM	12729	4.300E-01	7.0					

TABLE 96 CHAIN AND CUMULATIVE YIELDS FROM 1.750E+05 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
3 H PI	813r2	2.142E-02	27.3					2.142E-02	27.3

TABLE 97 CHAIN AND CUMULATIVE YIELDS FROM 2.100E+05 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
1 H PI	1199r2	2.567E-03	31.9					2.567E-03	31.9
3 H PI	1199r1	4.90E-02	30.2	-2.24		5.01	5.01	2.172E-02	(I) 15.3 >2
4 HE PI	1199r1	9.54E-01	30.2	2.24				34.2A	(E) 34.2A

TABLE 98 CHAIN AND CUMULATIVE YIELDS FROM 2.250E+05 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	INT. EXT./DF	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT VALUE	COMPONENT	EXTERNAL	EXTERNAL	EXTERNAL	INT. EXT./DF	DEVIATION
1 H	PI	1199+6.673E-03	31.9							31.9
3 H	PI	1199+2.003E-02	30.2							6.673E-03
3 H	PI	1199+2.003E-02	30.2							2.003E-02
4 HE	PI	1199+2.192E-01	30.2							2.192E-01

TABLE 99 CHAIN AND CUMULATIVE YIELDS FROM 2.850E+05 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	INT. EXT./DF	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT VALUE	COMPONENT	EXTERNAL	EXTERNAL	EXTERNAL	INT. EXT./DF	DEVIATION
3 H	PI	814+2.701E-02	14.5							2.701E-02
										14.5

TABLE 100 CHAIN AND CUMULATIVE YIELDS FROM 3.00E+05 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	MEAN	COMPONENT	EXTERNAL	INT.	EXT./DF	DEVIATION
3 H	PI	615E-2,422E-02	8.0						6.0
99 MO	798	5.550E+00	6.7						6.7
111 AG	798	1.800E-02	22.5						22.5
140 BA	798	5.790E+00	6.0						6.0
147 ND	798	2.610E+00	6.4						6.4
153 SM	798	1.520E-01	5.9						5.9

TABLE 101 CHAIN AND CUMULATIVE YIELDS FROM 3.30E+05 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	MEAN	COMPONENT	EXTERNAL	INT.	EXT./DF	DEVIATION
4 HE	PI	205771.699E-01	15.4						15.4
									1.699E-01

TABLE 102 CHAIN AND CUMULATIVE YIELDS FROM 3.450E+05 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXT.	INT.	EXT./DF	MEAN	WEIGHTED STANDARD DEVIATION
3 H	PI	815±2.776E-02	20.4					2.776E-02	20.4

TABLE 103 CHAIN AND CUMULATIVE YIELDS FROM 3.550E+05 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXT.	INT.	EXT./DF	MEAN	WEIGHTED STANDARD DEVIATION
3 H	PI	816±2.804E-02	13.5					2.804E-02	13.5

TABLE 104 CHAIN AND CUMULATIVE YIELDS FROM 3.700E+05 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXT.	INT.	EXT./DF	INT.	DEVIATION
3 H	PI	816E+1.630E-02	35.2						1.630E-02
									35.2

TABLE 105 CHAIN AND CUMULATIVE YIELDS FROM 3.850E+05 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXT.	INT.	EXT./DF	INT.	DEVIATION
3 H		816E+2.086E-02	11.6						2.086E-02
									11.6

TABLE 110 CHAIN AND CUMULATIVE YIELDS FROM 5.000E+05 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	INT. EXT./DF	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	VALUE	EXTERNAL	EXTERNAL	INT. EXT.	DF	DEVIATION
3 H PI	2043	1.095E-02 18.4	-1.81		3.28	3.28	1.222E-02	1	15.5	>2
		818E-2 142E-02 25.3	1.81						28.0A	
4 HE PI	2043	1.871E-01 6.2							1.871E-01	6.2

TABLE 111 CHAIN AND CUMULATIVE YIELDS FROM 5.250E+05 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	INT. EXT./DF	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	VALUE	EXTERNAL	EXTERNAL	INT. EXT.	DF	DEVIATION
3 H	819	2.235E-02 27.3							2.235E-02	27.3

TABLE 112 CHAIN AND CUMULATIVE YIELDS FROM 5.500E+05 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL	CHI2	INT. EXT./DF	WEIGHTED	STANDARD
NO.	YIELDS & SD	NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	EXTERNAL	EXTERNAL	EXTERNAL	EXTERNAL	EXTERNAL	EXTERNAL	EXTERNAL
1 H	PI	1199t1.540E-02	31.9								1.540E-02	31.9
3 H	PI	1199t3.260E-02	30.2								3.260E-02	30.2
4 HE	PI	1199t1.665E-01	30.2								1.665E-01	30.2
85 KR(M)		12729 1.740E+00	7.5									
87 KR		12729 2.480E+00	6.0									
88 KR		12729 3.260E+00	5.8									
91 SR		12729 5.530E+00	4.0								5.530E+00	4.0
92 SR		12729 5.380E+00	8.2									
93 Y		12729 6.360E+00	8.7								6.360E+00	8.7
95 ZK		12729 6.710E+00	4.2								6.710E+00	4.2
97 ZK		12729 5.780E+00	3.8									
99 MO		12729 5.420E+00	5.3								5.420E+00	5.3
103 RU		12729 3.510E+00	5.1								3.510E+00	5.1
105 RU		12729 1.160E+00	7.8								1.160E+00	7.8
109 PD		12729 2.700E-02	18.5								2.700E-02	18.5
111 AG		12729 2.400E-02	16.7								2.400E-02	16.7
115 CD		12729 1.700E-02	17.6								1.700E-02	17.6
121 SN		12729 1.400E-02	14.3								1.400E-02	14.3
125 SN		12729 1.500E-02	13.3									
127 SB		12729 4.00E-01	14.3									
129 SB		12729 8.800E-01	9.1									
131 I		12729 3.630E+00	4.4									
133 I		12729 6.690E+00	4.3									
134 TE		12729 5.940E+00	7.9									
135 I		12729 6.290E+00	3.8									
138 XB		12729 5.860E+00	6.3									
139 BA		12729 6.400E+00	4.8									
140 BA		12729 6.300E+00	4.0									
141 CE		12729 6.370E+00	8.9								6.370E+00	8.9
142 LA		12729 5.550E+00	6.7									
143 CE		12729 6.140E+00	5.9									
147 ND		12729 2.510E+00	6.8								2.510E+00	6.8
149 PM		12729 1.400E+00	11.4								1.400E+00	11.4
151 PM		12729 3.800E-01	10.5									

TABLE 113 CHAIN AND CUMULATIVE YIELDS FROM 5.600E+05 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL	CHI2	INT. EXT./DF	WEIGHTED	STANDARD
NO.	YIELDS & SD	NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	EXTERNAL	EXTERNAL	EXTERNAL	EXTERNAL	EXTERNAL	EXTERNAL	EXTERNAL
3 H	PI	819t1.937E-02	75.1								1.937E-02	75.1

TABLE 114 CHAIN AND CUMULATIVE YIELDS FROM 6.200E+05 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL NO.	YIELDS & SD	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	INT. EXT./DF	WEIGHTED STANDARD DEVIATION
3 H		8202	2.962E-02	35.2							2.962E-02
											35.2

TABLE 115 CHAIN AND CUMULATIVE YIELDS FROM 6.250E+05 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL NO.	YIELDS & SD	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	INT. EXT./DF	WEIGHTED STANDARD DEVIATION
3 H		8212	2.030E-02	25.3							2.030E-02
											25.3

TABLE 116 CHAIN AND CUMULATIVE YIELDS FROM 6.950E+05 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
3 H	821r	3.558E-02	14.5					3.558E-02	14.5

TABLE 117 CHAIN AND CUMULATIVE YIELDS FROM 7.000E+05 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
99 MO	799	5.608E+00	5.7					5.608E+00	5.7
111 AG	799	2.400E-02	10.4					2.400E-02	10.4
140 BA	799	6.080E+00	5.9					6.080E+00	5.9
147 ND	799	2.510E+00	6.9					2.510E+00	6.9
153 SM	799	1.540E-01	6.1					1.540E-01	6.1

TABLE 118 CHAIN AND CUMULATIVE YIELDS FROM 7.650E+05 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
3 H	822r1	1.607E-02	10.7					1.607E-02	10.7

TABLE 119 CHAIN AND CUMULATIVE YIELDS FROM 9.000E+05 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
99 MO	800	5.760E+00	5.6					5.760E+00	5.6
111 AG	800	3.500E-02	15.7					3.500E-02	15.7
140 BA	800	6.010E+00	5.7					6.010E+00	5.7
147 ND	800	2.450E+00	5.7					2.450E+00	5.7
153 SM	800	1.590E-01	9.0					1.590E-01	9.0

TABLE 120 CHAIN AND CUMULATIVE YIELDS FROM 1.000E+06 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCH2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	YIELDS & SD.	COMPONENT	VALUE	COMPONENT	VALUE	EXTERNAL	INTERNAL	EXT./DF	MEAN	DEVIATION	
3 H	PI	2043r1.665E-02	20.4						1.665E-02	20.	
4 HE	PI	857 1.873E-01	10.0	-0.25					0.06	0.06	1.906E-01 (I) 7.0A
		2043r1.939E-01	9.7	0.25						(E) 1.7	
84 BR		12729 1.240E+00	17.7								
85 KR(M)		12729 1.490E+00	4.0								
87 KR		12729 2.710E+00	5.2								
88 KR		12729 3.350E+00	4.5								
90 SR		12729 5.810E+00	4.0								
92 SR		12729 5.860E+00	11.4								
93 Y		12729 6.430E+00	5.0								
95 ZR		12729 6.570E+00	5.8								
97 ZR		12729 6.120E+00	3.8								
99 MO		12729 5.710E+00	5.2								
103 RU		12729 3.440E+00	5.2								
105 RU		12729 1.230E+00	4.9								
109 PD		12729 4.700E-02	14.9								
111 AG		12729 2.300E-02	13.0								
112 PD		12729 2.500E-02	16.0								
115 CD		12729 2.000E-02	15.0								
121 SN		12729 1.400E-02	14.3								
125 SN		12729 1.400E-02	14.3								
127 SB		12729 1.200E-01	16.7								
129 SB		12729 9.900E-01	13.1								
131 I		12729 3.560E+00	3.9								
132 TE		12729 4.840E+00	3.7								
133 I		12729 6.920E+00	4.3								
134 TE		12729 6.460E+00	5.0								
135 I		12729 6.390E+00	4.1								
138 XB		12729 5.870E+00	5.5								
139 BA		12729 6.910E+00	6.8								
140 BA		12729 6.230E+00	4.5								
142 LA		12729 5.610E+00	7.0								
143 CB		12729 5.500E+00	6.5								
147 ND		12729 2.330E+00	9.4								
149 PM		12729 1.240E+00	12.1								
151 PM		12729 4.000E-01	10.0								

TABLE 121 CHAIN AND CUMULATIVE YIELDS FROM 1.160E+06 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCH2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	YIELDS & SD.	COMPONENT	VALUE	COMPONENT	VALUE	EXTERNAL	INTERNAL	EXT./DF	MEAN	DEVIATION	
4 HE	PI	2057r1.393E-01	15.4						1.393E-01	15.4	

TABLE 122 CHAIN AND CUMULATIVE YIELDS FROM 1.300E+06 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT.	EXT./DF	MEAN DEVIATION
99 MO	801	5.550E+00	6.0					6.0
111 AG	801	4.400E-02	5.6					5.550E+00
140 BA	801	5.970E+00	6.0					4.400E-02
147 ND	801	2.560E+00	6.6					5.970E+00
153 SM	801	1.760E-01	7.6					2.560E+00
								1.760E-01
								7.6

TABLE 123 CHAIN AND CUMULATIVE YIELDS FROM 1.700E+06 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT.	EXT./DF	MEAN DEVIATION
99 MO	802	5.550E+00	7.0					5.550E+00
111 AG	802	5.300E-02	7.8					7.8
140 BA	802	5.750E+00	5.5					5.750E+00
147 ND	802	2.420E+00	5.6					2.420E+00
153 SM	802	1.720E-01	7.4					1.720E-01
								7.4

TABLE 124 CHAIN AND CUMULATIVE YIELDS FROM 2.000E+06 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	YIELDS & SD	COMPONENT	VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION			
3 H	PI 2043r1.047E-03	25.3					6.047E-03	25.3			
4 HE	PI 2043r1.137E-01	7.9					1.137E-01	7.9			
85 KR(M)	12729 1.760E+00	6.2									
87 KR	12729 2.610E+00	5.7									
88 KR	12729 3.220E+00	5.3									
91 SR	12729 5.360E+00	3.9					5.360E+00	3.9			
92 SR	12729 5.170E+00	8.1									
93 Y	12729 6.620E+00	6.0					6.620E+00	6.0			
95 ZR	12729 6.650E+00	8.6					6.650E+00	8.6			
97 ZR	12729 5.760E+00	3.8									
99 MO	12729 5.410E+00	5.4					5.410E+00	5.4			
103 RU	12729 3.330E+00	5.4					3.330E+00	5.4			
105 RU	12729 1.100E+00	8.2					1.100E+00	8.2			
109 PD	12729 6.100E-02	14.8					6.100E-02	14.8			
111 AG	12729 4.700E-02	14.9					4.700E-02	14.9			
112 PD	12729 4.800E-02	14.6									
115 CD	12729 5.100E-02	15.7					5.100E-02	15.7			
121 SN	12729 3.300E-02	15.2					3.300E-02	15.2			
125 SN	12729 3.300E-02	15.2									
127 SB	12729 2.300E-01	13.6									
129 SB	12729 1.060E+00	9.4									
131 I	12729 3.690E+00	4.3									
133 I	12729 6.370E+00	4.2									
134 TE	12729 5.710E+00	5.2									
135 I	12729 6.320E+00	3.8									
138 XB	12729 6.460E+00	5.6									
139 BA	12729 5.870E+00	6.0									
140 BA	12729 6.110E+00	3.9									
141 CE	12729 6.260E+00	8.5					6.260E+00	8.5			
142 LA	12729 5.560E+00	5.8									
143 CE	12729 5.760E+00	5.7									
144 CE	12729 5.480E+00	13.0									
147 ND	12729 2.470E+00	6.5					2.470E+00	6.5			
149 PM	12729 1.410E+00	10.6					1.410E+00	10.6			
151 PM	12729 4.300E-01	9.3									

TABLE 125 CHAIN AND CUMULATIVE YIELDS FROM 2.500E+06 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	YIELDS & SD	COMPONENT	VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION			
4 HE	PI 2050 1.399E-01	40.0					0.45	2.94	1.47	1.648E-01	5.7
	2052r1.609E-01	6.2					-0.21				
	2057r2.192E-01	15.4					1.67				6.9A

TABLE 126 CHAIN AND CUMULATIVE YIELDS FROM 3.000E+06 eV FISSION IN 235U .

A	EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	COMPONENT	VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION			
4 HE PI	2059	2.039E-01	6.2					2.039E-01	6.2			
86 SE	21743	9.200E-01	3.3	1.89				3.56	3.56	8.800E-01	(I)	2.4 >2
BR	21743	8.400E-01	3.6	-1.89							(E)	4.5A
87 BR	21743	2.050E+00	3.9W	-1.05				1.94	0.97	2.251E+00	(I)	3.1A
KE	2046	2.580E+00	14.0	1.14							(E)	3.0
	21743	2.900E+00	5.2W	0.82								
88 BR	21743	2.030E+00	3.9					2.030E+00	3.9			
89 KE	21743	4.410E+00	5.0					4.410E+00				
90 BR	21743	6.500E-01	15.4	-15.12				228.70	228.70	1.314E+00	(I)	6.8 >2
KE	21743	4.100E+00	5.0	15.12							(E)	103.5A
91 KE	21743	2.590E+00	3.9W	-0.95				2.00	1.00	3.201E+00	(I)	2.6A
SR	2046	5.580E+00	5.0W	0.18							(E)	2.8
	21743	5.600E+00	5.0W	1.55								
92 SR	21743	5.850E+00	4.8					5.850E+00	4.8			
93 RB	21743	3.590E+00	4.2W	-2.06				2.29	1.14	4.641E+00	(I)	2.4
SR	21743	5.800E+00	4.8W	0.31							(E)	2.5A
	21743	5.920E+00	3.4W	1.08								
94 RB	21743	1.910E+00	6.8W	-0.47				0.32	0.16	3.755E+00	(I)	2.5A
SR	21743	5.700E+00	2.6W	0.63							(E)	1.0
Y	21743	6.350E+00	5.3W	0.13								
95 SR	21743	5.200E+00	5.8	-2.92				8.54	8.54	5.641E+00	(I)	3.5 >2
Y	21743	6.400E+00	4.4	2.92							(E)	10.2A
97 ZR	2046	5.940E+00	11.0	-0.06				0.00	0.00	5.975E+00	(I)	3.8A
	21743	5.980E+00	4.0	0.06							(E)	0.2
MO	21743	6.150E+00	5.2					6.150E+00				
101 MO	21743	5.050E+00	5.0					5.050E+00	5.0			
102 TC	21743	4.400E+00	5.0					4.400E+00	5.0			
103 RU	21743	3.480E+00	5.2					3.480E+00	5.2			
104 TC	21743	2.150E+00	4.7					2.150E+00	4.7			
105 RU	21743	1.250E+00	4.8					1.250E+00	4.8			
127 SB	21743	3.100E-01	6.5					3.100E-01	6.5			
131 SN	21743	5.700E-01	8.8W	-1.52				0.67	0.33	1.060E+00	(I)	4.2A
SB	21743	2.560E+00	4.3W	0.64							(E)	2.4
I	21743	3.950E+00	5.1W	0.13								
132 SN	21743	4.900E-01	10.2	-17.30				299.44	299.44	6.595E-01	(I)	7.4 >2
TE	21743	4.900E+00	5.1	17.30							(E)	128.6A
133 SB	21743	1.820E+00	5.5W	-0.39				3.32	1.11	2.314E+00	(I)	4.1
TE(M)	2046	3.570E+00	20.0W	0.74							(E)	4.3A
I	2046	6.570E+00	12.0W	1.67								
	21743	6.700E+00	4.9W	0.77								
134 SB	21743	5.000E-01	16.0W	-1.50				0.50	0.25	1.603E+00	(I)	4.4A
TE	21743	5.370E+00	2.8W	0.07							(E)	2.2
I	2046	6.400E+00	16.0W	0.58								
135 TE	21743	2.080E+00	3.9	-4.21				17.76	17.76	2.117E+00	(I)	3.8 >2
I	2046	5.120E+00	14.0	4.21							(E)	15.8A
136 TE	21743	8.500E-01	4.7					8.500E-01	4.7			

TABLE 126 CHAIN AND CUMULATIVE YIELDS FROM 3.000E+06 eV FISSION IN 235U .

A	EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	COMPONENT	VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION			
137 I	21743	2.540E+00	4.7					2.540E+00	4.7			
138 I	21743	1.270E+00	4.7W	-1.06				0.48	0.24	1.657E+00	(I)	3.5A
XE	21743	5.740E+00	3.5W	0.12							(E)	1.7
CS	2046	2.500E+00	14.0W	0.66								
139 I	21743	4.800E-01	6.2	-18.40				338.61	338.61	5.619E-01	(I)	5.3 >2
XE	21743	4.200E+00	4.8	18.40							(E)	97.2A
140 XE	21743	2.630E+00	3.8W	-0.54				0.33	0.17	4.646E+00	(I)	1.3A
CS	21743	5.700E+00	1.4W	0.62							(E)	0.5
BA	21743	6.100E+00	3.3W	0.07								
141 XE	21743	6.300E-01	20.6	-21.68				469.89	469.89	2.161E+00	(I)	5.0 >2
BA	21743	5.800E+00	3.5	21.68							(E)	109.2A
142 CS	21743	2.660E+00	3.8W	-0.23				0.15	0.07	4.251E+00	(I)	1.6A
BA	21743	5.640E+00	1.8W	0.50							(E)	0.4
LA	21743	5.800E+00	4.8W	0.15								
143 CS	21743	1.230E+00	9.8W	-1.63				1.85	0.62	3.507E+00	(I)	2.1A
BA	21743	4.810E+00	2.1W	0.37							(E)	1.6
CE	21743	5.250E+00	5.3W	0.55								
	2046	5.690E+00	11.0W	0.54								
144 CS	21743	3.800E-01	7.9	-14.88				221.50	221.50	4.462E-01	(I)	6.6 >2
BA	21743	3.390E+00	5.9	14.88							(E)	98.9A
145 CE	21743	3.760E+00	5.3					3.760E+00	5.3			
147 ND	21743	2.260E+00	4.4					2.260E+00	4.4			
151 PM	21743	4.900E-01	4.1					4.900E-01	4.1			

TABLE 127 CHAIN AND CUMULATIVE YIELDS FROM 4.000E+06 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD.	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION			
84 BR	12729	1.400E+00	15.0								
85 KR(M)	12729	1.700E+00	4.1								
87 KR	12729	2.890E+00	5.2								
88 KR	12729	3.240E+00	4.9								
89 RB	12729	4.220E+00	13.3								
91 SR	12729	5.200E+00	3.9								
92 SR	12729	5.220E+00	6.9								
93 Y	12729	6.180E+00	6.0								
94 Y	12729	5.870E+00	7.2								
95 ZR	12729	6.390E+00	4.4								
97 ZR	12729	5.920E+00	3.9								
99 MO	12729	5.450E+00	5.3								
103 RU	12729	3.570E+00	5.3								
105 RU	12729	1.420E+00	6.3								
109 PD	12729	1.600E-01	12.5								
111 AG	12729	1.400E-01	14.3								
112 PD	12729	1.200E-01	16.7								
115 CD	12729	1.000E-01	20.0								
121 SN	12729	8.200E-02	14.6								
125 SN	12729	8.800E-02	14.8								
127 SB	12729	3.900E-01	15.4								
129 SB	12729	1.410E+00	10.6								
132 TE	12729	5.100E+00	4.9								
133 I	12729	6.470E+00	4.3								
134 TE	12729	4.710E+00	5.1								
135 I	12729	6.420E+00	3.7								
138 XE	12729	6.100E+00	9.3								
139 BA	12729	6.420E+00	5.8								
140 BA	12729	5.820E+00	4.1								
141 CE	12729	6.030E+00	13.1								
142 LA	12729	5.160E+00	7.0								
143 CE	12729	4.660E+00	9.2								
144 CE	12729	4.190E+00	10.5								
147 ND	12729	2.220E+00	4.5								
149 PM	12729	1.150E+00	8.7								
151 PM	12729	5.200E-01	5.8								

TABLE 128 CHAIN AND CUMULATIVE YIELDS FROM 5.500E+06 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD.	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION			
85 KR(M)	12729	1.810E+00	5.5								
87 KR	12729	2.860E+00	5.6								
88 KR	12729	3.220E+00	5.0								
89 RB	12729	3.570E+00	15.4								
91 SR	12729	4.980E+00	4.0								
92 SR	12729	5.080E+00	8.9								
93 Y	12729	5.880E+00	8.5								
94 Y	12729	5.590E+00	8.4								
95 ZR	12729	6.410E+00	3.9								
97 ZR	12729	5.860E+00	4.1								
99 MO	12729	5.520E+00	5.6								
103 RU	12729	2.580E+00	5.4								
105 RU	12729	1.660E+00	6.0								
109 PD	12729	4.100E-01	14.6								
111 AG	12729	3.000E-01	16.7								
112 PD	12729	2.300E-01	17.4								
115 CD	12729	2.800E-01	14.3								
121 SN	12729	2.100E-01	14.3								
125 SN	12729	1.800E-01	16.7								
127 SB	12729	7.800E-01	15.4								
129 SB	12729	1.970E+00	7.1								
131 I	12729	4.750E+00	4.2								
132 TE	12729	5.170E+00	4.9								
133 I	12729	6.340E+00	4.3								
134 TE	12729	3.800E+00	7.1								
135 I	12729	6.230E+00	3.9								
138 XE	12729	5.410E+00	13.9								
139 BA	12729	5.530E+00	9.8								
140 BA	12729	5.660E+00	4.2								
141 CE	12729	6.450E+00	13.0								
142 LA	12729	4.630E+00	6.3								
143 CE	12729	4.830E+00	5.8								
147 ND	12729	2.610E+00	7.3								
149 PM	12729	1.310E+00	16.8								
151 PM	12729	6.400E-01	6.2								

TABLE 129 CHAIN AND CUMULATIVE YIELDS FROM 6.000E+06 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	YIELDS & SD.	COMPONENT	VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION			
84 BR	1099 1.160E+00	44.0					1.160E+00	4.0			
87 KR	1099 2.940E+00	16.0					2.940E+00	16.0			
89 SR	1099 3.820E+00	8.0					3.820E+00	8.0			
91 SR	1099 5.310E+00	9.0					5.310E+00	9.0			
95 ZR	1099 5.850E+00	8.0					5.850E+00	8.0			
97 ZR	1099 5.720E+00	10.0					5.720E+00	10.0			
99 MO	1099 6.170E+00	8.0					6.170E+00	8.0			
103 RU	1099 3.110E+00	5.0					3.110E+00	5.0			
104 TC	1099 2.810E+00	46.1					2.810E+00	46.1			
105 RE	1099 1.720E+00	10.0					1.720E+00	10.0			
111 AG	1099 2.410E-01	8.0					2.410E-01	8.0			
112 PD	1099 2.200E-01	8.0					2.200E-01	8.0			
115 CD(G)	1099 1.840E-01	8.0	1.840E-01								
CD(M)	1099 1.430E-02	44.0	1.430E-02								
127 SB	1099 8.210E-01	22.0					8.210E-01	22.0			
129 SN	1099 8.040E-01	19.0					8.040E-01	19.0			
130 SB	1099 1.020E+00	19.0					1.020E+00	19.0			
132 TE	1099 4.580E+00	8.0					4.580E+00	8.0			
133 I	1099 6.140E+00	13.0					6.140E+00	13.0			
137 CS	1099 6.090E+00	13.0					6.090E+00	13.0			
140 BA	1099 5.030E+00	8.0					5.030E+00	8.0			
141 CE	1099 4.930E+00	9.0					4.930E+00	9.0			
142 LA	1099 5.030E+00	9.0					5.030E+00	9.0			
143 CE	1099 4.690E+00	10.0					4.690E+00	10.0			
144 CE	1099 2.160E+00	9.0					2.160E+00	9.0			
147 ND	1099 2.090E+00	9.0					2.090E+00	9.0			
151 PM	1099 5.340E-01	102.0					5.340E-01	102.0			
156 EU	1099 4.640E-02	10.0					4.640E-02	10.0			

TABLE 130 CHAIN AND CUMULATIVE YIELDS FROM 6.300E+06 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	YIELDS & SD.	COMPONENT	VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION			
85 KR(M)	12729 1.840E+00	6.5					1.840E+00	6.5			
87 KR	12729 2.660E+00	7.9					2.660E+00	7.9			
88 KR	12729 3.270E+00	6.4					3.270E+00	6.4			
91 SR	12729 4.870E+00	3.9					4.870E+00	3.9			
92 SR	12729 4.730E+00	8.2					4.730E+00	8.2			
93 Y	12729 6.470E+00	6.8					6.470E+00	6.8			
95 ZR	12729 6.270E+00	5.3					6.270E+00	5.3			
97 ZR	12729 5.580E+00	4.1					5.580E+00	4.1			
99 MO	12729 5.050E+00	5.7					5.050E+00	5.7			
103 RU	12729 3.520E+00	5.4					3.520E+00	5.4			
105 RU	12729 1.600E+00	10.6					1.600E+00	10.6			
109 PD	12729 3.900E-01	15.4					3.900E-01	15.4			
111 AG	12729 3.000E-01	16.7					3.000E-01	16.7			
112 PD	12729 2.900E-01	13.8					2.900E-01	13.8			
115 CD	12729 3.200E-01	15.6					3.200E-01	15.6			
121 SN	12729 2.300E-01	13.0					2.300E-01	13.0			
125 SN	12729 2.100E-01	14.3					2.100E-01	14.3			
127 SB	12729 7.300E-01	15.1					7.300E-01	15.1			
129 SB	12729 1.720E+00	8.7					1.720E+00	8.7			
131 I	12729 4.980E+00	4.2					4.980E+00	4.2			
132 TE	12729 4.860E+00	4.3					4.860E+00	4.3			
133 I	12729 6.110E+00	4.3					6.110E+00	4.3			
134 TE	12729 5.600E+00	12.2					5.600E+00	12.2			
135 I	12729 5.660E+00	4.4					5.660E+00	4.4			
139 BA	12729 5.570E+00	7.7					5.570E+00	7.7			
140 BA	12729 5.600E+00	4.1					5.600E+00	4.1			
141 CE	12729 5.700E+00	8.6					5.700E+00	8.6			
142 LA	12729 4.850E+00	6.8					4.850E+00	6.8			
143 CE	12729 4.900E+00	6.1					4.900E+00	6.1			
147 ND	12729 2.270E+00	7.5					2.270E+00	7.5			
149 PM	12729 1.490E+00	12.8					1.490E+00	12.8			
151 PM	12729 5.800E-01	8.6					5.800E-01	8.6			

TABLE 131 CHAIN AND CUMULATIVE YIELDS FROM 7.100E+06 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION			
84 BR	1100	1.220E+00	40.3				1.220E+00	40.3			
85 KR(M)	12729	2.370E+00	5.9								
87 KR	1100	2.920E+00	14.3								
	12729	3.050E+00	6.6								
88 KR	12729	3.430E+00	5.5								
89 SR	1100	4.140E+00	7.7				4.140E+00	7.7			
91 SR	1100	5.190E+00	10.4				5.190E+00	10.4			
92 SR	12729	4.780E+00	9.4								
93 Y	12729	6.200E+00	7.1				6.200E+00	7.1			
95 ZR	12729	6.050E+00	5.0	-0.13		0.02	0.02	6.070E+00	(I)	4.2A	
	1100	6.120E+00	7.7	0.13					(E)	0.5	
97 ZR	12729	5.570E+00	4.0	-0.34		0.11	0.11	5.597E+00	(I)	3.7A	
	1100	5.770E+00	9.6	0.34					(E)	1.2	
99 MO	12729	5.210E+00	5.4	-0.40		0.16	0.16	5.272E+00	(I)	4.4A	
	1100	5.410E+00	7.7	0.40					(E)	1.8	
103 RU	1100	3.140E+00	8.2	-0.26		0.07	0.07	3.196E+00	(I)	4.4A	
	12729	3.220E+00	5.3	0.26					(E)	1.2	
104 TC	1100	2.740E+00	34.2				2.740E+00	34.2			
105 RU	12729	1.630E+00	5.5	1.62		2.62	2.62	1.546E+00	(I)	4.8 >2	
	1100	1.370E+00	9.7	-1.62					(E)	7.8A	
109 PD	12729	3.900E-01	15.4				3.900E-01	15.4			
111 AG	12729	2.180E-01	17.5	-1.75		3.07	3.07	2.269E-01	(I)	6.8 >2	
	1100	2.180E-01	17.5	1.75					(E)	1.2	
112 PD	1100	2.020E-01	7.4								
	12729	2.300E-01	17.4								
115 CD	12729	3.400E-01	14.7	3.400E-01	0.00	6.92	7.452	7.44	2.085E-01	(I)	6.3 >2
	1100	1.790E-01	7.5	1.790E-01	0.00	0.50				(E)	17.3A
CD(G)	1100	1.960E-02	14.7	1.960E-02	0.00	0.02					
CD(M)	1100	1.960E-02	14.7	1.960E-02	0.00						
121 SN	12729	2.300E-01	13.0				2.300E-01	13.0			
125 SN	12729	2.000E-01	15.0								
127 SB	12729	7.800E-01	15.4	-0.24		0.06	0.06	7.957E-01	(I)	12.6A	
	1100	8.320E-01	22.0	0.24					(E)	3.0	
129 SN	1100	7.080E-01	20.5				7.080E-01	20.5			
SB	12729	1.740E+00	8.1								
130 SB	1100	9.550E-01	19.1				9.550E-01	19.1			
131 I	12729	4.410E+00	7.3								
132 TE	12729	4.850E+00	3.9	-0.05		0.00	0.00	4.854E+00	(I)	3.5A	
	1100	4.870E+00	8.0	0.05					(E)	0.2	
133 I	1100	6.190E+00	12.7								
	12729	6.220E+00	4.3								
134 TE	12729	3.910E+00	14.8								
135 I	12729	5.830E+00	3.8								
137 CS	1100	7.240E+00	12.8				7.240E+00	12.8			
140 BA	1100	5.300E+00	7.7								
	12729	5.510E+00	4.0								
141 CE	1100	5.010E+00	9.2	-1.20		1.44	1.44	5.365E+00	(I)	6.6	
	12729	5.870E+00	9.4	1.20					(E)	7.9A	
142 LA	12729	4.900E+00	5.9	-0.24		0.06	0.06	4.922E+00	(I)	5.6A	
	1100	5.130E+00	17.6	0.24					(E)	1.4	
143 CE	1100	4.640E+00	9.6								
	12729	5.020E+00	5.8								

TABLE 131 CHAIN AND CUMULATIVE YIELDS FROM 7.100E+06 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION			
144 CE	12729	4.300E+00	11.9	-0.02		0.00	0.00	4.306E+00	(I)	7.3A	
	1100	4.310E+00	9.2	0.02					(E)	0.1	
147 ND	12729	2.130E+00	6.6	-0.28		0.08	0.08	2.153E+00	(I)	5.3A	
	1100	2.200E+00	9.2	0.28					(E)	1.5	
149 PM	12729	1.100E+00	12.7				1.100E+00	12.7			
151 PM	1100	3.590E-01	16.9								
	12729	5.300E-01	9.4								
156 EU	1100	3.880E-02	9.9				3.880E-02	9.9			

TABLE 132 CHAIN AND CUMULATIVE YIELDS FROM 8.100E+06 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	YIELDS & SD	COMPONENT	VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION			
84 BR	1101 1.580E+00	34.6					1.580E+00	34.6			
85 KR(M)	12729 2.070E+00	6.3									
87 KR	12729 2.830E+00	6.0	-0.53		0.28	0.28	2.859E+00	(I) 5.6A			
	1101 3.110E+00	16.0	0.53					(E) 3.0			
88 KR	12729 3.380E+00	5.3									
89 SR	1101 3.850E+00	9.8					3.850E+00	9.8			
91 SR	12729 5.150E+00	4.1	-0.05		0.00	0.00	5.153E+00	(I) 3.9A			
	1101 5.180E+00	12.2	0.05					(E) 0.2			
92 SR	12729 4.790E+00	8.1									
93 Y	12729 6.230E+00	5.8									
95 ZR	1101 5.900E+00	8.7	-0.40		0.16	0.16	6.073E+00	(I) 4.5A			
	12729 6.140E+00	5.2	0.40					(E) 1.8			
97 ZR	12729 5.470E+00	4.2	-0.08		0.01	0.01	5.476E+00	(I) 3.9A			
	1101 5.520E+00	10.8	0.08					(E) 0.3			
99 MO	12729 4.920E+00	5.5	-0.86		0.74	0.74	5.035E+00	(I) 4.7A			
	1101 5.390E+00	8.8	0.86					(E) 4.0			
103 RU	1101 2.960E+00	9.8	-0.36		0.13	0.13	3.049E+00	(I) 4.8A			
	12729 3.080E+00	5.5	0.36					(E) 1.7			
104 TC	1101 2.420E+00	31.2					2.420E+00	31.2			
105 RU	12729 1.530E+00	5.9	0.77		0.60	0.60	1.495E+00	(I) 5.2A			
RH	1101 1.390E+00	11.3	-0.77					(E) 4.0			
109 PD	12729 5.400E-01	14.8					5.400E-01	14.8			
111 AG	1101 2.970E-01	18	-3.23		10.40	10.40	2.443E-01	(I) 23.2A			
	12729 4.300E-01	14.0	3.23					(E) 23.2A			
112 PD	1101 2.170E-01	7.9									
	12729 4.400E-01	13.6									
115 CD	12729 3.600E-01	15.8	3.800E-01	0.00	8.20	8.72	8.71	2.080E-01	(I) 7.0	>2	
CD(G)	1101 1.820E-01	8.0	1.820E-01	0.00	0.48			(E) 20.6A			
CD(M)	1101 1.540E-02	21.3	1.540E-02	0.00	0.02						
121 SN	12729 3.000E-01	16.7					3.000E-01	16.7			
125 SN	12729 3.000E-01	16.7									
127 SB	1101 6.420E-01	22.0									
	12729 9.800E-01	15.3									
129 SN	1101 7.530E-01	19.9					7.530E-01	19.9			
SB	12729 1.750E+00	8.0									
130 SB	1101 8.880E-01	20.1					8.880E-01	20.1			
132	12729 4.360E+00	4.1									
132 TE	1101 4.450E+00	8.7									
	12729 4.750E+00	4.2									
133 I	1101 5.690E+00	14.9									
	12729 5.950E+00	4.4									
134 TE	12729 3.740E+00	13.6									
135 I	12729 5.680E+00	6.3									
135 CS	1101 4.180E+00	15.7					4.180E+00	15.7			
138 XB	12729 5.230E+00	5.7									
139 BA	12729 6.010E+00	6.5									
140 BA	12729 5.300E+00	9.8									
141 CE	1101 4.970E+00	10.4	-0.89		0.80	0.80	5.325E+00	(I) 6.2A			
	12729 5.570E+00	7.7	0.89					(E) 5.5			

TABLE 132 CHAIN AND CUMULATIVE YIELDS FROM 8.100E+06 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	YIELDS & SD	COMPONENT	VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION			
142 LA	12729 4.680E+00	5.8	-0.60		0.36	0.36	4.719E+00	(E) 3.3			
	1101 5.340E+00	20.1	0.60								
143 CE	1101 4.730E+00	11.0									
	12729 4.920E+00	5.7									
144 CE	12729 4.650E+00	11.8									
147 ND	1101 2.030E+00	11.1	-0.70		0.49	0.49	2.162E+00	(I) 5.8A			
	12729 2.220E+00	6.8	0.70					(E) 4.1			
149 PM	12729 1.120E+00	10.7					1.120E+00	10.7			
151 PM	1101 4.760E-01	16.1									
	12729 5.300E-01	5.7									
156 EU	1101 3.420E-02	12.1					3.420E-02	12.1			

TABLE 133 CHAIN AND CUMULATIVE YIELDS FROM 9.100E+06 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	INT. EXT./DF	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	VALUE	EXTERNAL	EXTERNAL	INT.	EXT.	INT. EXT./DF	MEAN	DEVIATION
84 BR	1102	1.140E+00	38.1								1.140E+00	38.1
87 KR	1102	2.910E+00	19.6								2.910E+00	19.6
89 SR	1102	3.250E+00	14.9								3.250E+00	14.9
91 SR	1102	4.880E+00	12.9								4.880E+00	12.9
95 ZR	1102	6.050E+00	10.5								6.050E+00	10.5
97 ZR	1102	5.350E+00	12.8								5.350E+00	12.8
99 MO	1102	5.360E+00	10.8								5.360E+00	10.8
103 RU	1102	2.700E+00	14.2								2.700E+00	14.2
104 TC	1102	2.670E+00	31.1								2.670E+00	31.1
105 RH	1102	1.020E+00	17.0								1.020E+00	17.0
111 AG	1102	3.060E-01	8.8								3.060E-01	8.8
112 PD	1102	2.920E-01	8.5								2.920E-01	8.5
115 CD(G)	1102	2.420E-01	8.3	2.420E-01				0.00	0.00	2.573E-01 (I)	8.1A	
CD(M)	1102	1.530E-02	33.1	1.530E-02							(E)	0.0
127 SB	1102	8.080E-01	12.2								8.080E-01	12.2
129 SN	1102	8.280E-01	22.0								8.280E-01	22.0
130 SB	1102	1.040E+00	20.7								1.040E+00	20.7
132 TE	1102	3.960E+00	11.1								3.960E+00	11.1
133 I	1102	5.640E+00	18.1								5.640E+00	18.1
137 CS	1102	5.400E+00	15.1								5.400E+00	15.1
140 BA	1102	4.710E+00	11.3								4.710E+00	11.3
141 CE	1102	4.570E+00	12.9								4.570E+00	12.9
142 LA	1102	5.500E+00	22.9								5.500E+00	22.9
143 CE	1102	4.390E+00	13.5								4.390E+00	13.5
144 CE	1102	3.620E+00	13.3								3.620E+00	13.3
147 ND	1102	1.870E+00	14.9								1.870E+00	14.9
151 PM	1102	3.700E-01	47.5								3.700E-01	47.5
156 EU	1102	3.810E-02	15.6								3.810E-02	15.6

TABLE 134 CHAIN AND CUMULATIVE YIELDS FROM 1.400E+07 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	INT. EXT./DF	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	VALUE	EXTERNAL	EXTERNAL	INT.	EXT.	INT. EXT./DF	MEAN	DEVIATION
4 HE FI	2050	1.456E-01	40.0								1.456E-01	40.0
											0.40	
											0.40	
											0.16	0.16 1.687E-01 (E)
											2.5	

TABLE 135 CHAIN AND CUMULATIVE YIELDS FROM 1.430E+07 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION	
85 KR(G)	13116	3.980E-01	50.0							
156 EU	13116	5.140E-02	50.0					5.140E-02	50.0	
161 TB	13116	4.090E-03	50.0					4.090E-03	50.0	

TABLE 136 CHAIN AND CUMULATIVE YIELDS FROM 1.470E+07 eV FISSION IN 235U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION	
85 KR(G)	13116	4.000E-01	50.0							
156 EU	13116	5.350E-02	50.0					5.350E-02	50.0	
161 TB	13116	4.380E-03	50.0					4.380E-03	50.0	

TABLE 137 CHAIN AND CUMULATIVE YIELDS FROM 4.500E+06 eV FISSION IN 236U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	INT. EXT./DF	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT VALUE	COMPONENT	EXTERNAL	EXTERNAL	INT.	EXT.	DEVIATION
4 HE PI	2079	6.135E-03	10.0					6.135E-03	10.0	

TABLE 138 CHAIN AND CUMULATIVE YIELDS FROM 4.850E+00 eV FISSION IN 238U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	INT. EXT./DF	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT VALUE	COMPONENT	EXTERNAL	EXTERNAL	INT.	EXT.	DEVIATION
99 MO	321	6.450E+00	10.0					6.450E+00	10.0	

TABLE 139 CHAIN AND CUMULATIVE YIELDS FROM 9.500E-01 eV FISSION IN 238U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT.	EXT./DF	INT.	DEVIATION
99 MO	321	6.190E+00	10.0					6.190E+00	10.0

TABLE 140 CHAIN AND CUMULATIVE YIELDS FROM 5.000E+05 eV FISSION IN 238U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT.	EXT./DF	INT.	DEVIATION
3 H PI	92043	1.907E-02	17.0						
4 HE PI	92043	1.025E-01	10.0						

TABLE 141 CHAIN AND CUMULATIVE YIELDS FROM 1.000E+06 eV FISSION IN 238U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.		NO.	YIELDS & SD	COMPONENT	VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION	
3 H	PI	92043	1.225E-02	16.0							
4 HE	PI	92043	1.106E-01	10.0							

TABLE 142 CHAIN AND CUMULATIVE YIELDS FROM 1.500E+06 eV FISSION IN 238U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.		NO.	YIELDS & SD	COMPONENT	VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION	
83 BR		1086	2.800E-01	11.0						2.800E-01	11.0
85 KR(G)		1086	7.900E-01	6.0							
87 KR		1086	1.600E+00	6.0						1.600E+00	6.0
88 KR		1086	1.710E+00	8.0						1.710E+00	8.0
89 RB		1086	2.340E+00	13.0						2.340E+00	13.0
91 SR		1086	3.930E+00	6.0						3.930E+00	6.0
92 SR		1086	4.180E+00	6.0						4.180E+00	6.0
93 Y		1086	4.360E+00	7.0						4.360E+00	7.0
94 Y		1086	4.450E+00	8.0						4.450E+00	8.0
95 ZR		1086	5.310E+00	4.0						5.310E+00	4.0
97 ZR		1086	5.360E+00	5.0						5.360E+00	5.0
99 MO		1086	6.290E+00	5.0						6.290E+00	5.0
101 TC		1086	6.410E+00	9.0						6.410E+00	9.0
103 RU		1086	6.960E+00	5.0						6.960E+00	5.0
104 TC		1086	5.170E+00	7.0						5.170E+00	7.0
105 RU		1086	4.680E+00	6.0						4.680E+00	6.0
107 RH		1086	5.400E-01	9.0						5.400E-01	9.0
109 PD		1086	7.500E-02	11.0						7.500E-02	11.0
112 PD		1086	2.800E-02	22.0						2.800E-02	22.0
113 AG		1086	2.500E-02	25.0						2.500E-02	25.0
115 CD(G)		1086	8.900E-03	10.0							
121 SN(G)		1086	1.360E-02	11.0							
125 SN(G)		1086	6.200E-03	25.0							
127 SB		1086	8.300E-02	5.0						8.300E-02	5.0
129 SB		1086	2.800E-01	15.0	-2.04		4.18	4.18	3.291E-01 (I)	10.5	>2
					2.04					21.4A	
131 I		1086	3.240E+00	5.0						3.240E+00	5.0
132 TE		1086	5.400E+00	5.0						5.400E+00	5.0
133 I		1086	7.150E+00	5.0							
134 TE		1086	8.120E+00	5.0						8.120E+00	5.0
135 I		1086	7.230E+00	5.0						7.230E+00	5.0
138 XE		1086	5.270E+00	5.0						5.270E+00	5.0
139 BA		1086	7.110E+00	10.0							
140 BA		1086	6.010E+00	5.0						6.010E+00	5.0
142 LA		1086	4.690E+00	6.0						4.690E+00	6.0
143 CE		1086	4.630E+00	7.0						4.630E+00	7.0
146 CE		1086	3.820E+00	9.0							
147 ND		1086	2.650E+00	14.0						2.650E+00	14.0
149 ND		1086	1.740E+00	22.0						1.740E+00	22.0

TABLE 143 CHAIN AND CUMULATIVE YIELDS FROM 1.720E+06 eV FISSION IN 238U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	YIELDS & SD	COMPONENT	VALUE	COMPONENT	EXT.	INT.	EXT./DF	MEAN	DEVIATION		
85 KR(M)	2000 7.410E+00	9.4									
87 KR	2000 1.200E+00	12.5						1.200E+00	12.5		
88 KR	2000 1.600E+00	10.6						1.600E+00	10.6		
89 RB	2000 3.260E+00	12.0						0.59	0.59	3.065E+00 (E)	8.3A
	2000 3.260E+00	11.0						0.77			
91 SR	2000 3.630E+00	10.2						0.30	0.15	3.782E+00 (I)	5.9A
	2000 3.920E+00	10.2						0.42			(E) 2.3
Y (M)	2000 3.820E+00	10.2						0.12			
92 SR	2000 4.380E+00	9.1						4.380E+00	9.1		
93 Y	2000 5.160E+00	10.5						5.160E+00	10.5		
94 Y	2000 4.370E+00	12.1						4.370E+00	12.1		
95 ZR	2000 5.370E+00	10.6						5.370E+00	10.6		
97 NB(G)	2000 5.480E+00	11.5	5.480E+00					0.00	0.00	5.480E+00 (I)	11.5A
NB(M)	2000 5.220E+00	10.9	5.220E+00								(E) 0.0
101 TC	2000 7.830E+00	11.9						7.830E+00	11.9		
103 RU	2000 6.680E+00	10.5						6.680E+00	10.5		
104 TC	2000 4.820E+00	10.8						4.820E+00	10.8		
105 RU	2000 4.650E+00	11.2						1.54	1.54	4.010E+00 (I)	7.2
	2000 4.370E+00	9.4						1.24			9.0A
107 RH	2000 6.700E+00	31.3						6.700E+00	31.3		
129 SB	2000 4.400E+00	15.9						4.400E+00	15.9		
131 I	2000 3.570E+00	10.4						3.570E+00	10.4		
132 I	2000 4.620E+00	12.6						1.10	0.37	4.986E+00 (I)	5.8A
	2000 4.900E+00	10.2						-0.73			
	2000 5.010E+00	14.2						-0.21			
	2000 5.470E+00	10.8						0.36			
	2000 5.470E+00	10.8						0.94			
133 I	2000 7.080E+00	10.0						7.080E+00	10.0		
134 TE	2000 6.640E+00	11.1						6.640E+00	11.1		
135 I	2000 7.320E+00	10.7						0.49	0.24	7.093E+00 (I)	6.0A
	2000 7.350E+00	10.5						0.40			(E) 3.0
140 BA	2000 5.670E+00	10.8						0.03	0.02	5.726E+00 (I)	6.2A
	2000 5.670E+00	10.8						-0.11			
LA	2000 5.820E+00	10.7						-0.07			(E) 0.8
	2000 5.820E+00	10.7						0.19			
141 BA	2000 4.980E+00	13.1						4.980E+00	13.1		
142 LA	2000 5.040E+00	11.7						5.040E+00	11.7		
143 CB	2000 4.600E+00	12.0						4.600E+00	12.0		
146 CE	2000 3.290E+00	11.8						3.290E+00	11.8		
147 ND	2000 2.640E+00	15.9						2.640E+00	15.9		
149 ND	2000 1.650E+00	5.2						1.650E+00	5.2		

TABLE 144 CHAIN AND CUMULATIVE YIELDS FROM 2.000E+06 eV FISSION IN 238U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	YIELDS & SD	COMPONENT	VALUE	COMPONENT	EXT.	INT.	EXT./DF	MEAN	DEVIATION		
3 H	PI 92043 9.160E-03	33.0									
4 HE	PI 92043 1.080E-01	10.0									
77 AS	366 4.000E-03	15.0						4.000E-03	15.0		
83 KR	1087 2.800E-01	11.0						0.16	0.16	2.723E-01 (E)	3.6A
	1087 2.800E-01	11.0						0.40			
85 KR(M)	935 7.500E-01	15.0									
	1087 7.700E-01	5.0									
87 KR	1087 1.570E+00	5.0						0.16			4.7A
	1087 1.570E+00	5.0						0.03	0.03	1.566E+00 (E)	0.8
88 KR	935 1.790E+00	15.0						0.56	0.31	0.31 1.931E+00 (I)	4.7A
	1087 1.950E+00	5.0						0.56			(E) 2.7
89 RB	1087 2.260E+00	14.0						0.45	0.20	0.20 2.352E+00 (I)	10.2A
	935 2.480E+00	15.0						0.45			(E) 4.6
91 SR	1087 3.940E+00	6.0						0.50	0.58	0.29 3.996E+00 (I)	5.2A
	935 3.970E+00	15.0						-0.05			(E) 2.8
Y	935 4.480E+00	15.0						0.76			
92 SR	1087 4.100E+00	6.0								4.100E+00	6.0
93 Y	935 4.580E+00	15.0						0.29	0.08	0.08 4.758E+00 (I)	6.3A
	1087 4.800E+00	7.0						0.29			(E) 1.8
94 Y	1087 4.400E+00	7.0								4.400E+00	7.0
95 ZR	935 5.110E+00	15.0						0.04	0.00	0.00 5.137E+00 (I)	4.7A
	1087 5.140E+00	5.0						0.04			(E) 0.2
97 ZR	1087 5.580E+00	15.0						0.23	0.05	0.05 5.600E+00 (I)	4.7A
	935 5.580E+00	15.0						-0.23			(E) 1.1
99 MO	1087 6.120E+00	5.0						1.14	1.72	0.86 6.252E+00 (I)	4.5A
	935 6.620E+00	15.0						0.39			(E) 4.2
	935 7.600E+00	15.0						1.22			
101 TC	1087 6.450E+00	7.0								6.450E+00	7.0
103 RU	935 4.760E+00	15.0M						2.38	6.32	3.16 6.610E+00 (I)	4.6 >2
	935 6.850E+00	15.0						0.25			(E) 8.1A
	1087 7.030E+00	5.0M						2.44			
104 TC	1087 4.860E+00	7.0								4.860E+00	7.0
105 RU	935 4.440E+00	15.0						0.11	0.01	0.01 4.509E+00 (I)	5.2A
	935 4.510E+00	15.0						0.00			(E) 0.4
	1087 4.520E+00	6.0						0.08			
106 RU	935 3.850E+00	15.0						1.06	1.13	1.13 3.027E+00 (I)	8.4
	935 3.850E+00	15.0						-1.06			(E) 8.9A
107 RH	1087 1.050E+00	26.0								1.050E+00	26.0
109 PD	935 6.200E-02	15.0						1.05	1.09	6.928E-02 (I)	8.9
	1087 7.500E-02	11.0						1.05			(E) 9.3A
111 AG	935 2.900E-02	15.0						0.33	0.14	0.07 3.025E-02 (I)	7.3A
	366 3.000E-02	15.0						0.36			(E) 2.0
	1087 3.000E-02	15.0						0.34			
112 PD	1087 2.600E-02	12.0						0.20	0.04	0.04 2.637E-02 (I)	9.4A
	935 2.700E-02	15.0						0.20			(E) 1.8
113 AG(G)	1087 9.000E-03	23.0								9.000E-03	23.0
115 CD(G)	1087 1.050E-02	15.0						0.66	1.05	0.53 1.131E-02 (I)	8.7A
	366 1.300E-02	15.0						1.00			(E) 6.3
CHAIN	935 1.100E-02	15.0						0.24			
121 SN(G)	1087 1.390E-02	10.0						0.04	0.00	0.00 1.393E-02 (I)	8.3A
	935 1.400E-02	15.0						0.04			(E) 0.3
125 SN(G)	1087 8.200E-03	25.0								2.000E-02	15.0
CHAIN	935 2.000E-02	15.0									
127 SB	935 5.600E-02	15.0						0.67	0.45	0.45 5.955E-02 (I)	11.0A
	1087 6.500E-02	16.0						0.67			(E) 7.4

TABLE 144 CHAIN AND CUMULATIVE YIELDS FROM 2.000E+06 eV FISSION IN 238U .

(CONT.)

A EL. NO.	REF.	EXPERIMENTAL YIELDS & SD	MEAN COMPONENT VALUE	R VALUE	CHI2/DF	CHI2 EXTERNAL	TOTAL CHI2 INT. EXT./DF	WEIGHTED MEAN DEVIATION
129 SB	935 3.300E-01	14.0	-1.05	2.83	0.94	3.738E-01	(I) 7.1A	(E) 6.9
	1087 3.500E-01	15.0	-0.58					
	1087 4.000E-01	13.0	0.59					
	935 4.600E-01	15.0	1.35					
131 I	1087 3.250E+00	15.0	-1.40	4.06	2.03	3.141E+00	(I) 4.5	>2
	1087 3.500E+00	15.0	-1.40				(E) 6.5A	
	935 3.370E+00	15.0	0.47					
132 TE	935 4.160E+00	15.0	-1.48	2.93	1.47	5.018E+00	(I) 4.5	
	935 4.590E+00	15.0	-0.66				(E) 5.5A	
	1087 5.230E+00	5.0	1.65					
133 I	935 6.600E+00	15.0	-0.49	0.24	0.12	7.060E+00	(I) 4.5A	
	935 7.050E+00	15.0	-0.01				(E) 1.6	
	1087 7.120E+00	5.0	0.38					
134 TE	1087 7.780E+00	5.0				7.780E+00	5.0	
135 I	935 5.340E+00	15.0	-2.00	4.91	2.46	6.815E+00	(I) 4.5	>2
	935 6.240E+00	15.0	-0.65				(E) 7.1A	
	1087 7.200E+00	5.0	2.09					
138 XE	1087 5.690E+00	5.0				5.690E+00	5.0	
139 BA	935 6.810E+00	5.0	-0.12	0.01	0.01	6.918E+00	(I) 7.1A	
	1087 6.950E+00	8.0	0.12				(E) 0.8	
140 BA	935 5.770E+00	15.0	-0.35	0.14	0.07	6.055E+00	(I) 4.5A	
	935 5.970E+00	15.0	-0.10				(E) 1.2	
	1087 6.100E+00	5.0	0.34					
141 BA	1087 5.730E+00	6.0	0.32	0.12	0.04	5.651E+00	(I) 4.2A	
CE	1087 5.550E+00	7.0	-0.33				(E) 0.9	
	935 5.610E+00	15.0	-0.05					
	935 5.690E+00	15.0	0.05					
142 LA	935 4.540E+00	7.0	-0.16	0.03	0.03	4.638E+00	(I) 6.3A	
	1087 4.660E+00	7.0	0.16				(E) 1.0	
143 CE	935 4.280E+00	15.0	-0.59					
	1087 4.620E+00	6.0	-0.11	0.51	0.17	4.641E+00	(I) 4.2A	
	1087 4.750E+00	6.0	0.39				(E) 1.7	
	935 4.920E+00	15.0	0.39					
144 CE	935 4.800E+00	15.0				4.800E+00	15.0	
146 CE	1087 3.720E+00	8.0				3.720E+00	8.0	
147 ND	935 2.250E+00	13.0	-2.28	6.98	3.49	2.880E+00	(I) 6.7	>2
	1087 2.820E+00	13.0	-0.19				(E) 12.6A	
	1087 3.460E+00	9.0	2.38					
149 ND	1087 1.720E+00	12.0	-1.12	1.26	1.26	1.845E+00	(I) 9.4	
PK	935 2.150E+00	15.0	1.12				(E) 10.6A	
151 PM	935 6.500E-01	15.0	-1.64	3.10	1.55	7.830E-01	(I) 6.9	
	1087 8.200E-01	9.0	0.74				(E) 8.6A	
	935 9.200E-01	15.0	1.08					
153 SM	935 3.800E-01	15.0	-0.33	0.11	0.11	3.869E-01	(I) 1A	
	1087 4.300E-01	33.0	0.33				(E) 4.5	
156 EU	935 9.100E-02	15.0				9.100E-02	15.0	

TABLE 145 CHAIN AND CUMULATIVE YIELDS FROM 2.160E+06 eV FISSION IN 238U .

A EL. NO.	REF.	EXPERIMENTAL YIELDS & SD	MEAN COMPONENT VALUE	R VALUE	CHI2/DF	CHI2 EXTERNAL	TOTAL CHI2 INT. EXT./DF	WEIGHTED MEAN DEVIATION
85 KR(M)	2000 8.657E-01	13.9						
87 KR	2000 1.060E+00	12.3					1.060E+00	12.3
88 KR	2000 1.480E+00	14.9					1.480E+00	14.9
89 RB	2000 3.030E+00	14.2	-0.02	0.00	0.00	3.025E+00	(I) 0.5A	
	2000 3.030E+00	14.2	0.02				(E) 0.5A	
91 SR	2000 3.570E+00	11.5	-1.19	1.41	1.41	3.886E+00	(I) 8.0	
	2000 4.320E+00	11.1	1.19				(E) 9.5A	
92 SR	2000 4.450E+00	10.6				4.450E+00	10.6	
93 Y	2000 4.550E+00	10.3				4.550E+00	10.3	
94 Y	2000 4.370E+00	12.1				4.370E+00	12.1	
95 ZR	2000 5.330E+00	10.7				5.330E+00	10.7	
97 NB(M)	2000 5.540E+00	10.5				5.540E+00	10.5	
99 Y (M)	2000 3.340E+00	12.0				3.340E+00	12.0	
101 TC	2000 6.990E+00	11.0				6.990E+00	11.0	
103 RU	2000 6.480E+00	10.3				6.480E+00	10.3	
104 TC	2000 4.730E+00	11.4				4.730E+00	11.4	
105 RU	2000 3.320E+00	11.4	-1.87	3.50	3.50	3.767E+00	(I) 7.8	>2
	2000 4.450E+00	10.6	1.87				(E) 14.7A	
107 RH	2000 8.200E-01	28.1				8.200E-01	28.1	
129 SB	2000 4.300E-01	11.6				4.300E-01	11.6	
131 I	2000 3.530E+00	10.5				3.530E+00	10.5	
132 I	2000 5.380E+00	11.0	-0.81	0.94	0.31	5.785E+00	(I) 5.3A	
	2000 5.690E+00	10.4	0.19				(E) 3.0	
	2000 6.050E+00	10.2	0.49					
	2000 6.140E+00	11.2	0.58					
133 I	2000 6.260E+00	10.3				6.260E+00	10.3	
134 TE	2000 6.540E+00	10.9				6.540E+00	10.9	
135 I	2000 6.950E+00	10.5	-0.33	0.28	0.14	7.141E+00	(I) 6.2A	
	2000 7.040E+00	10.8	-0.16				(E) 2.3	
	2000 7.510E+00	11.1	0.53					
138 CS	2000 5.290E+00	10.8				5.290E+00	10.8	
140 BA	2000 5.730E+00	11.0	-0.06	0.45	0.15	5.764E+00	(I) 5.4A	
LA	2000 5.840E+00	11.3	-0.35				(E) 2.1	
	2000 5.840E+00	11.3	-0.22					
	2000 6.130E+00	10.4	0.65					
141 BA	2000 4.670E+00	10.9				4.670E+00	10.9	
142 LA	2000 4.790E+00	10.9				4.790E+00	10.9	
143 CE	2000 4.490E+00	11.1				4.490E+00	11.1	
146 CE	2000 3.540E+00	13.0				3.540E+00	13.0	
147 ND	2000 2.730E+00	16.1				2.730E+00	16.1	
149 ND	2000 1.680E+00	15.5				1.680E+00	15.5	

TABLE 146 CHAIN AND CUMULATIVE YIELDS FROM 2.500E+06 eV FISSION IN 238U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
4HE PI	2051	1.66E-01	10.0W	2.30	8.52	2.84	7.25E-02 (I)	7.7 >2
	2057	4.82E-02	30.2	-2.26				(E) 13.0A
	2052	6.21E-02	10.6W	-0.89				
	2050	9.06E-02	40.0	0.52				

TABLE 147 CHAIN AND CUMULATIVE YIELDS FROM 3.000E+06 eV FISSION IN 238U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
77 AS	367	9.10E-03	15.0				9.10E-03	15.0
83 BR	911	1.170E-01	20.0				1.170E-01	20.0
84 BR	911	2.100E-01	10.0				2.100E-01	10.0
89 SR	911	3.730E+00	11.0				3.730E+00	11.0
91 SR	911	4.650E+00	11.0	1.54			2.36 3.972E+00 (I)	6.5 >2
CHAIN	405	3.740E+00	8.0	-1.54				(E) 10.0A
92 SR	911	5.210E+00	10.0				5.210E+00	10.0
93 Y	911	5.720E+00	9.0	0.96			0.92 0.92 5.332E+00 (I)	6.0A
CHAIN	405	5.090E+00	8.0	-0.96				(E) 5.7
95 ZR	911	6.670E+00	12.0				6.670E+00	12.0
97 ZR	911	6.920E+00	10.0				6.920E+00	10.0
99 MO	911	6.750E+00	11.0				6.750E+00	11.0
103 RU	911	5.240E+00	16.0				5.240E+00	16.0
105 RH	911	2.160E+00	15.0	-4.16			17.29 17.29 3.110E+00 (I)	7.4 >2
	405	4.070E+00	8.0	4.16			(E) 30.7A	
107 CHAIN	405	1.450E+00	10.0				1.450E+00	10.0
109 PD	911	1.020E-01	10.0				1.020E-01	10.0
111 AG	367	5.200E-02	15.0	-2.17			4.71 4.71 6.347E-02 (I)	9.0 >2
	911	7.700E-02	11.0	2.17			(E) 19.6A	
112 PD	911	6.900E-02	13.0				6.900E-02	13.0
113 AG	911	5.900E-02	12.0				5.900E-02	12.0
115 CD(G)	367	2.600E-02	15.0	-2.82			7.98 7.98 2.991E-02 (I)	12.2 >2
	911	5.700E-02	18.0	2.82			(E) 34.4A	
118 CD	911	5.400E-02	18.0				5.400E-02	18.0
121 SN	911	5.900E-02	15.0				5.900E-02	15.0
127 SB	911	1.310E-01	16.0				1.310E-01	16.0
129 CHAIN	405	4.400E-01	8.0				4.400E-01	8.0
131 TE(W)	911	1.680E+00	11.0				3.310E+00	8.0
CHAIN	405	3.310E+00	8.0					
132 TE	911	3.790E+00	9.0				3.790E+00	9.0
133 I	911	7.370E+00	12.0				7.370E+00	12.0
134 I	911	8.190E+00	10.0				8.190E+00	10.0
135 I	911	6.880E+00	13.0				6.880E+00	13.0
139 BA	911	5.10E+00	10.0				5.10E+00	10.0
140 BA	911	6.160E+00	7.0				6.160E+00	7.0
141 CE	911	5.760E+00	11.0				5.760E+00	11.0
143 CE	911	5.450E+00	10.0	-0.06			0.00 0.00 5.474E+00 (I)	6.2A
CHAIN	405	5.490E+00	8.0	0.06				(E) 0.4
145 PR	911	4.070E+00	10.0	-0.54			0.29 0.29 4.237E+00 (I)	6.3A
CHAIN	405	4.360E+00	8.0	0.54				(E) 3.4
147 ND	911	3.500E+00	14.0				3.500E+00	14.0
149 PM	911	1.830E+00	13.0				1.830E+00	13.0
151 PM	911	6.900E-01	12.0				6.900E-01	12.0

TABLE 148 CHAIN AND CUMULATIVE YIELDS FROM 3.600E+06 eV FISSION IN 238U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
3 H	PI	2000 1.770E-02	25.0				1.770E-02	25.0
4 HE	PI	2000 1.130E-01	10.0				1.130E-01	10.0

TABLE 149 CHAIN AND CUMULATIVE YIELDS FROM 3.730E+06 eV FISSION IN 238U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
85 KR	(M)	2000 8.344E-01	9.6					
87 KR		2000 1.390E+00	11.5				1.390E+00	11.5
88 KR		2000 1.770E+00	10.7				1.770E+00	10.7
89 RB		2000 2.950E+00	15.2	-0.03		0.00	0.00 2.950E+00 (I)	10.2A
91 SR		2000 3.360E+00	11.9	-0.72		1.67	0.84 3.599E+00 (I)	6.2A
		2000 4.040E+00	10.2	1.28				5.6
	Y (M)	2000 3.460E+00	10.1	-0.51				
92 SR		2000 4.900E+00	10.4				4.900E+00	10.4
93 Y		2000 5.230E+00	10.9				5.230E+00	10.9
94 Y		2000 4.570E+00	12.2				4.570E+00	12.2
95 ZR		2000 5.750E+00	11.0				5.750E+00	11.0
97 NB	(G)	2000 5.930E+00	10.3	5.930E+00		0.00	0.00 5.930E+00 (I)	10.3A
	NB (M)	2000 5.460E+00	10.3	5.460E+00				
101 TC		2000 7.490E+00	10.6				7.490E+00	10.6
103 RU		2000 6.270E+00	10.2				6.270E+00	10.2
104 TC		2000 4.130E+00	10.9				4.130E+00	10.9
105 RU		2000 3.330E+00	11.1	0.47		0.22	0.22 3.448E+00 (I)	7.8A
		2000 3.580E+00	10.9	0.47				3.6
107 RH		2000 8.100E-01	22.2				8.100E-01	22.2
129 SB		2000 6.200E-01	12.9				6.200E-01	12.9
131 I		2000 3.650E+00	10.1				3.650E+00	10.1
132 I		2000 4.590E+00	11.6	-1.01		3.88	1.94 5.017E+00 (I)	6.4
		2000 4.690E+00	11.3	-0.78				8.9A
		2000 6.080E+00	10.4	1.96				
133 I		2000 6.500E+00	10.3				6.500E+00	10.3
134 TE		2000 6.110E+00	12.3				6.110E+00	12.3
135 I		2000 7.050E+00	10.6	-0.06		0.00	0.00 7.077E+00 (I)	8.3A
		2000 7.120E+00	13.2	0.06				0.5
138 CS		2000 5.290E+00	11.0	-0.08		0.01	0.01 5.324E+00 (I)	7.8A
		2000 5.360E+00	11.2	0.08				0.7
140 BA		2000 5.730E+00	10.5	0.23		0.07	0.03 5.620E+00 (I)	6.4A
	LA	2000 5.510E+00	10.5	-0.24				(B) 1.2
		2000 5.630E+00	13.0	0.02				
141 BA		2000 4.990E+00	15.8				4.990E+00	15.8
142 LA		2000 5.110E+00	10.4				5.110E+00	10.4
143 CE		2000 4.390E+00	10.2				4.390E+00	10.2
146 CE		2000 3.340E+00	12.9	-0.18		0.03	0.03 3.392E+00 (I)	9.2A
		2000 3.450E+00	13.0	0.18				(B) 1.6
147 ND		2000 4.770E+00	15.5				4.770E+00	15.5
149 ND		2000 1.840E+00	15.2				1.840E+00	15.2

TABLE 150 CHAIN AND CUMULATIVE YIELDS FROM 3.900E+06 eV FISSION IN 238U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION	
85 KR(G)	1088 8.600E+00	5.0						
87 KR	1088 1.780E+00	5.0				1.780E+00	5.0	
88 KR	1088 2.090E+00	8.0				2.090E+00	8.0	
89 RB	1088 2.570E+00	12.0				2.570E+00	12.0	
91 SR	1088 3.960E+00	7.0				3.960E+00	7.0	
92 SR	1088 4.240E+00	6.0				4.240E+00	6.0	
93 Y	1088 4.03E+00	7.0	-1.31	1.72	1.72	4.571E+00 (I)	5.0	
	1088 4.03E+00	7.0				4.03E+00	7.0	
94 Y	1088 5.130E+00	8.0				5.130E+00	8.0	
95 ZR	1088 5.340E+00	5.0				5.340E+00	5.0	
ZR	1088 5.620E+00	5.0				5.620E+00	5.0	
99 MO	1088 6.000E+00	5.0				6.000E+00	5.0	
101 TC	1088 7.080E+00	8.0				7.080E+00	8.0	
103 RU	1088 6.120E+00	5.0				6.120E+00	5.0	
104 TC	1088 4.740E+00	7.0				4.740E+00	7.0	
105 RU	1088 4.400E+00	7.0				4.400E+00	7.0	
106 RU	1088 2.810E+00	11.0				2.810E+00	11.0	
107 RH	1088 1.050E+00	21.0				1.050E+00	21.0	
109 PD	1088 1.180E-01	11.0				1.180E-01	11.0	
111 AG	1088 1.040E-01	13.0				1.040E-01	13.0	
112 PD	1088 5.700E-02	30.0				5.700E-02	30.0	
113 AG(G)	1088 3.400E-02	24.0				3.400E-02	24.0	
115 CD(G)	1088 2.900E-02	11.0						
121 SN(G)	1088 2.900E-02	11.0				2.900E-02	11.0	
125 SN(G)	1088 2.600E-02	27.0				2.600E-02	27.0	
127 SB	1088 1.600E-01	13.0	-1.02	1.04	1.04	1.749E-01 (I)	8.4	
	1088 1.900E-01	11.0				1.90E-01 (E)	8.6A	
129 SB	1088 6.100E-01	15.0	-1.47	2.17	2.17	7.170E-01 (I)	7.8	>2
	1088 7.800E-01	9.0	1.47			7.80E-01 (E)	11.5A	
131 I	1088 3.360E+00	5.0				3.360E+00	5.0	
132 TE	1088 4.890E+00	5.0				4.890E+00	5.0	
133 I	1088 6.950E+00	5.0				6.950E+00	5.0	
134 TE	1088 7.760E+00	6.0				7.760E+00	6.0	
135	1088 6.450E+00	5.0				6.45E+00	5.0	
138 XE	1088 5.820E+00	5.0				5.820E+00	5.0	
139 BA	1088 5.430E+00	11.0				5.430E+00	11.0	
140 BA	1088 6.170E+00	8.0				6.170E+00	8.0	
141 BA	1088 5.850E+00	10.0	0.31	0.10	0.10	5.693E+00 (I)	5.1A	
CE	1088 5.640E+00	6.0	-0.31				(E)	1.6
142 LA	1088 4.850E+00	6.0				4.850E+00	6.0	
143 CE	1088 4.600E+00	6.0	-0.35	0.12	0.12	4.568E+00 (I)	4.2A	
	1088 4.740E+00	6.0	0.35			4.74E+00 (E)	1.5	
146 CE	1088 3.440E+00	9.0				3.440E+00	9.0	
147 ND	1088 2.700E+00	8.0	-1.57	2.48	2.48	2.918E+00 (I)	5.7	>2
	1088 3.230E+00	8.0	1.57			3.23E+00 (E)	8.9A	
149 ND	1088 1.940E+00	13.0	-0.03	0.00	0.00	1.945E+00 (I)	9.2A	
	1088 1.950E+00	13.0	0.03			1.95E+00 (E)	0.3	

TABLE 150 CHAIN AND CUMULATIVE YIELDS FROM 3.900E+06 eV FISSION IN 238U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION	
151 PM	1088 9.000E-01	7.0				9.000E-01	7.0	
153 SM	1088 4.300E-01	19.0				4.300E-01	19.0	

TABLE 151 CHAIN AND CUMULATIVE YIELDS FROM 4.200E+06 eV FISSION IN 238U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT.	EXT./DF	INT.	DEVIATION
3 H	PI	2000	2.370E-02	25.0					25.0
4 HE	PI	2000	1.150E-01	12.0					12.0

TABLE 152 CHAIN AND CUMULATIVE YIELDS FROM 4.500E+06 eV FISSION IN 238U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT.	EXT./DF	INT.	DEVIATION
4 HE	PI	2079	2.041E-02	10.0					10.0
									2.041E-02

TABLE 153 CHAIN AND CUMULATIVE YIELDS FROM 4.780E+06 eV FISSION IN 238U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION		
85 KR(M)	2000	1.033E+00	9.7							
85 KR	2000	1.520E+00	10.5				1.520E+00	10.5		
87 KR	2000	2.000E+00	10.5				2.000E+00	10.5		
88 KR	2000	3.660E+00	13.7				3.660E+00	13.7		
89 RB	2000	3.620E+00	10.5				3.620E+00	10.5		
91 SR	2000	3.480E+00	10.9				3.480E+00	10.9		
92 SR	2000	4.110E+00	10.5				4.110E+00	10.5		
93 Y	2000	4.770E+00	10.9				4.770E+00	10.9		
94 Y	2000	6.560E+00	10.4				6.560E+00	10.4		
101 TC	2000	5.820E+00	10.7				5.820E+00	10.7		
103 RU	2000	5.000E+00	10.6				5.000E+00	10.6		
104 TC	2000	3.710E+00	10.8				3.710E+00	10.8		
105 RU	2000	9.200E-01	21.7				9.200E-01	21.7		
107 RH	2000	2.400E-01	20.8				2.400E-01	20.8		
127 SB	2000	5.49	5.49	3.314E-01	(I)	9.4	>2			
129 SB	2000	7.500E-01	12.0				7.500E-01	12.0		
131 I	2000	3.860E+00	10.1				3.860E+00	10.1		
132 I	2000	4.310E+00	10.7	-0.84			4.310E+00	10.7		
133 I	2000	4.350E+00	10.6	-0.74			4.350E+00	10.6		
134 TE	2000	4.890E+00	10.4	0.56			4.890E+00	10.4		
135 I	2000	5.180E+00	10.2	1.15			5.180E+00	10.2		
136 XE	2000	6.170E+00	10.2				6.170E+00	10.2		
137 BA	2000	6.280E+00	11.5				6.280E+00	11.5		
138 XE	2000	6.590E+00	10.4	-0.15			6.590E+00	10.4		
139 BA	2000	6.590E+00	10.4	-0.08			6.590E+00	10.4		
140 BA	2000	6.590E+00	10.4	0.23			6.590E+00	10.4		
141 BA	2000	6.590E+00	10.4				6.590E+00	10.4		
142 LA	2000	6.590E+00	10.4				6.590E+00	10.4		
143 CE	2000	6.590E+00	10.4				6.590E+00	10.4		
144 CE	2000	6.590E+00	10.4				6.590E+00	10.4		
145 CE	2000	6.590E+00	10.4				6.590E+00	10.4		
146 CE	2000	6.590E+00	10.4				6.590E+00	10.4		
147 ND	2000	6.590E+00	10.4				6.590E+00	10.4		
148 ND	2000	6.590E+00	10.4				6.590E+00	10.4		
149 ND	2000	6.590E+00	10.4				6.590E+00	10.4		

TABLE 154 CHAIN AND CUMULATIVE YIELDS FROM 5.500E+06 eV FISSION IN 238U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION		
83 RB	1089	3.900E-01	11.0				3.900E-01	11.0		
85 KR(G)	1089	1.030E+00	6.0				1.030E+00	6.0		
87 KR	1089	1.900E+00	6.0				1.900E+00	6.0		
88 KR	1089	2.050E+00	8.0				2.050E+00	8.0		
89 RB	1089	2.860E+00	13.0				2.860E+00	13.0		
91 SR	1089	3.630E+00	6.0				3.630E+00	6.0		
92 SR	1089	3.960E+00	7.0				3.960E+00	7.0		
93 Y	1089	4.930E+00	7.0				4.930E+00	7.0		
94 Y	1089	5.110E+00	8.0				5.110E+00	8.0		
95 ZR	1089	5.590E+00	5.0				5.590E+00	5.0		
97 ZR	1089	5.440E+00	5.0				5.440E+00	5.0		
99 MO	1089	5.460E+00	6.0				5.460E+00	6.0		
101 TC	1089	6.530E+00	9.0				6.530E+00	9.0		
103 RU	1089	6.000E+00	5.0				6.000E+00	5.0		
104 TC	1089	4.490E+00	7.0				4.490E+00	7.0		
105 RU	1089	3.870E+00	8.0				3.870E+00	8.0		
106 RU	1089	3.050E+00	11.0				3.050E+00	11.0		
107 RH	1089	1.400E+00	42.0				1.400E+00	42.0		
111 AG	1089	1.670E-01	11.0				1.670E-01	11.0		
113 AG(G)	1089	8.300E-02	25.0				8.300E-02	25.0		
115 CD(G)	1089	6.700E-02	11.0				6.700E-02	11.0		
121 SN(G)	1089	9.100E-02	10.0				9.100E-02	10.0		
123 SN(G)	1089	1.300E-02	24.0				1.300E-02	24.0		
127 SB	1089	2.800E-01	15.0	-1.64			2.800E-01	15.0		
129 SB	1089	1.100E+00	7.0	2.66			1.100E+00	7.0		
131 I	1089	3.720E+00	5.0	-2.66			3.720E+00	5.0		
132 TE	1089	5.050E+00	5.0				5.050E+00	5.0		
133 I	1089	6.770E+00	5.0				6.770E+00	5.0		
134 TE	1089	7.000E+00	8.0				7.000E+00	8.0		
135 I	1089	6.490E+00	5.0				6.490E+00	5.0		
136 XE	1089	5.800E+00	5.0				5.800E+00	5.0		
137 BA	1089	6.500E+00	8.0				6.500E+00	8.0		
140 BA	1089	5.610E+00	5.0				5.610E+00	5.0		
141 BA	1089	5.300E+00	7.0				5.300E+00	7.0		
142 LA	1089	4.580E+00	7.0				4.580E+00	7.0		
143 CE	1089	4.750E+00	7.0				4.750E+00	7.0		
146 CE	1089	3.640E+00	9.0				3.640E+00	9.0		
147 ND	1089	2.960E+00	10.0				2.960E+00	10.0		
149 ND	1089	1.510E+00	6.0				1.510E+00	6.0		

TABLE 157 CHAIN AND CUMULATIVE YIELDS FROM 6.900E+06 eV FISSION IN 238U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL	CHI2	EXT.	DF	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION				
85 KR(G)	1090	8.300E+00	6.0									
87 KR	1090	1.470E+00	8.0				1.470E+00	8.0				
91 SR	1090	3.990E+00	6.0				3.990E+00	6.0				
92 SR	1090	3.680E+00	7.0				3.680E+00	7.0				
95 ZR	1090	5.580E+00	5.0				5.580E+00	5.0				
97 ZR	1090	5.430E+00	8.0				5.430E+00	8.0				
99 MO	1090	6.060E+00	5.0				6.060E+00	5.0				
103 RU	1090	5.980E+00	5.0				5.980E+00	5.0				
105 RU	1090	3.880E+00	6.0				3.880E+00	6.0				
109 PD	1090	3.600E-01	11.0				3.600E-01	11.0				
111 AG	1090	2.500E-01	12.0				2.500E-01	12.0				
112 PD	1090	2.000E-01	20.0				2.000E-01	20.0				
115 CD(G)	1090	1.160E-01	11.0				1.160E-01	11.0				
121 SN(G)	1090	1.220E-01	10.0				1.220E-01	10.0				
125 SN(G)	1090	6.700E-02	26.0				6.700E-02	26.0				
127 SB	1090	3.900E-01	16.0	-0.86		0.74	4.378E-01	(I) 6.4A				
	1090	4.500E-01	7.0	0.86				(E) 5.5				
129 SB	1090	8.900E-01	7.0	-0.19		0.04	0.04 8.945E-01	(I) 6.4A				
	1090	9.200E-01	16.0	0.19				(E) 1.2				
131 I	1090	3.480E+00	5.0				3.480E+00	5.0				
132 TE	1090	5.100E+00	5.0				5.100E+00	5.0				
133 I	1090	7.100E+00	5.0				7.100E+00	5.0				
134 TE	1090	7.240E+00	12.0				7.240E+00	12.0				
135 I	1090	6.660E+00	5.0				6.660E+00	5.0				
139 BA	1090	6.100E+00	8.0				6.100E+00	8.0				
140 BA	1090	5.400E+00	5.0				5.400E+00	5.0				
141 CE	1090	5.070E+00	8.0				5.070E+00	8.0				
142 LA	1090	4.250E+00	6.0	-0.33		0.11	0.11 4.308E+00	(I) 4.2A				
	1090	4.370E+00	6.0	0.33				(E) 1.4				
143 CE	1090	4.170E+00	6.0	-0.31		0.09	0.09 4.224E+00	(I) 4.2A				
	1090	4.280E+00	6.0	0.31				(E) 1.3				
144 CE	1090	4.750E+00	13.0				4.750E+00	13.0				
147 ND	1090	2.900E+00	9.0				2.900E+00	9.0				
149 ND	1090	1.750E+00	16.0				1.750E+00	16.0				
151 PM	1090	8.500E-01	6.0				8.500E-01	6.0				
153 SM	1090	4.600E-01	11.0				4.600E-01	11.0				

TABLE 158 CHAIN AND CUMULATIVE YIELDS FROM 7.100E+06 eV FISSION IN 238U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL	CHI2	EXT.	DF	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION				
84 BR	1104	1.070E+00	40.3				1.070E+00	40.3				
87 KR	1104	1.840E+00	15.7				1.840E+00	15.7				
89 SR	1104	2.570E+00	7.5				2.570E+00	7.5				
91 SR	1104	4.140E+00	9.3				4.140E+00	9.3				
95 ZR	1104	5.190E+00	7.5				5.190E+00	7.5				
97 ZR	1104	5.540E+00	9.4				5.540E+00	9.4				
99 MO	1104	6.080E+00	7.5				6.080E+00	7.5				
103 RU	1104	5.590E+00	8.5				5.590E+00	8.5				
104 TC	1104	4.510E+00	25.9				4.510E+00	25.9				
105 RH	1104	3.490E+00	10.2				3.490E+00	10.2				
111 AG	1104	1.730E-01	7.4				1.730E-01	7.4				
112 PD	1104	1.390E-01	7.6				1.390E-01	7.6				
115 CD(G)	1104	9.810E-02	7.7				9.810E-02	7.7				
CD(M)	1104	2.260E-02	32.1				2.260E-02	32.1	0.00	0.00	1.207E-01	(I) 8.7A
127 SB	1104	1.010E+00	50.8				1.010E+00	50.8				
129 SN	1104	4.920E-01	19.5				4.920E-01	19.5				
130 SB	1104	6.160E-01	20.8				6.160E-01	20.8				
132 TE	1104	4.690E+00	7.6				4.690E+00	7.6				
133 I	1104	6.840E+00	13.4				6.840E+00	13.4				
137 CS	1104	2.60E+00	45.2				2.60E+00	45.2				
140 BA	1104	5.350E+00	7.5				5.350E+00	7.5				
141 CE	1104	4.740E+00	9.0				4.740E+00	9.0				
142 A	1104	4.60E+00	18.0				4.60E+00	18.0				
143 CE	1104	4.690E+00	9.1				4.690E+00	9.1				
144 CE	1104	5.080E+00	9.1				5.080E+00	9.1				
147 ND	1104	2.560E+00	9.0				2.560E+00	9.0				
151 PM	1104	7.020E-01	29.7				7.020E-01	29.7				
156 EU	1104	7.730E-02	9.8				7.730E-02	9.8				

TABLE 159 CHAIN AND CUMULATIVE YIELDS FROM 7.700E+06 eV FISSION IN 238U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	YIELDS & SD	COMPONENT	VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION		
85 KR(G)	1091 2.400E+00	6.0								
87 KR	1091 1.820E+00	5.0					1.820E+00	5.0		
88 KR	1091 2.320E+00	7.0					2.320E+00	7.0		
89 RB	1091 2.680E+00	13.0					2.680E+00	13.0		
91 SR	1091 4.040E+00	6.0					4.040E+00	6.0		
92 SR	1091 4.230E+00	7.0					4.230E+00	7.0		
93 Y	1091 5.050E+00	7.0					5.050E+00	7.0		
94 Y	1091 4.510E+00	9.0					4.510E+00	9.0		
95 ZR	1091 5.360E+00	5.0					5.360E+00	5.0		
97 ZR	1091 5.620E+00	5.0					5.620E+00	5.0		
99 MO	1091 5.960E+00	5.0					5.960E+00	5.0		
101 TC	1091 6.780E+00	7.0					6.780E+00	7.0		
103 RU	1091 6.220E+00	5.0					6.220E+00	5.0		
104 TC	1091 4.440E+00	7.0					4.440E+00	7.0		
105 RU	1091 3.750E+00	6.0					3.750E+00	6.0		
106 RU	1091 3.020E+00	10.0					3.020E+00	10.0		
107 RH	1091 7.100E-01	26.0					7.100E-01	26.0		
109 PD	1091 3.200E-01	10.0					3.200E-01	10.0		
111 AG	1091 2.600E-01	12.0					2.600E-01	12.0		
113 PD	1091 2.000E-01	20.0					2.000E-01	20.0		
115 CD(G)	1091 1.650E-01	14.0					1.650E-01	14.0		
121 SN(G)	1091 1.500E-01	10.0					1.500E-01	10.0		
125 SN(G)	1091 5.100E-02	55.0					5.100E-02	55.0		
127 SB	1091 4.100E-01	15.0	-1.36	1.84	1.84	4.680E-01	(I) 9.4	(E) 12.8A		
129 SB	1091 1.230E+00	7.0	1.82	3.30	3.30	1.151E+00	(I) 6.5	(E) 11.7A	>2	
131 I	1091 3.890E+00	5.0					3.890E+00	5.0		
132 TE	1091 5.220E+00	5.0					5.220E+00	5.0		
133 I	1091 7.040E+00	5.0					7.040E+00	5.0		
134 TE	1091 7.020E+00	7.0					7.020E+00	7.0		
135 I	1091 6.790E+00	5.0	3.82	14.61	14.61	5.757E+00	(I) 3.6	(E) 13.6A	>2	
XE			-3.82							
139 BA	1091 4.540E+00	8.0					4.540E+00	8.0		
140 BA	1091 5.690E+00	5.0					5.690E+00	5.0		
141 BA	1091 5.510E+00	6.0					5.510E+00	6.0		
142 LA	1091 4.350E+00	6.0					4.350E+00	6.0		
143 CE	1091 4.580E+00	6.0					4.580E+00	6.0		
146 CE	1091 3.190E+00	8.0					3.190E+00	8.0		
147 ND	1091 2.660E+00	9.0					2.660E+00	9.0		
149 ND	1091 1.910E+00	10.0					1.910E+00	10.0		

TABLE 160 CHAIN AND CUMULATIVE YIELDS FROM 8.000E+06 eV FISSION IN 238U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	YIELDS & SD	COMPONENT	VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION		
83 BR	936 6.200E-01	15.0					6.200E-01	15.0		
85 KR(M)	936 8.800E-01	15.0								
87 KR	936 2.000E+00	15.0					2.000E+00	15.0		
88 KR	936 2.260E+00	15.0					2.260E+00	15.0		
89 RB	936 2.640E+00	15.0	0.28				0.08	0.08	2.561E+00	(I) 10.6A
SR	936 2.490E+00	15.0	-0.28							(E) 2.9
91 SR	936 4.400E+00	15.0	0.81				0.66	0.66	3.990E+00	(I) 10.6A
Y	936 3.700E+00	15.0	-0.81							(E) 8.6
92 SR	936 4.810E+00	15.0							4.810E+00	15.0
93 Y	936 5.330E+00	15.0							5.330E+00	15.0
94 Y	936 5.010E+00	15.0							5.010E+00	15.0
95 ZR	936 5.910E+00	15.0	-0.04				0.00	0.00	5.935E+00	(I) 10.6A
	936 5.960E+00	15.0	0.04							(E) 0.4
97 ZR	936 6.260E+00	15.0							6.260E+00	15.0
99 MO	936 6.520E+00	15.0	-0.77				0.59	0.59	7.006E+00	(I) 10.6A
	936 7.680E+00	15.0	0.77							(E) 8.2
101 MO	936 7.340E+00	15.0							7.340E+00	15.0
103 RU	936 5.120E+00	15.0	1.08				1.16	1.16	5.634E+00	(I) 10.7
	936 6.450E+00	15.0	1.08							(E) 11.5A
105 RU	936 3.960E+00	15.0							3.960E+00	15.0
106 RU	936 3.110E+00	15.0							3.110E+00	15.0
107 RH	936 2.360E+00	15.0							2.360E+00	15.0
109 PD	936 3.200E-01	15.0							3.200E-01	15.0
111 AG	936 2.400E-01	15.0							2.400E-01	15.0
112 PD	936 2.000E-01	15.0							2.000E-01	15.0
121 SN	936 1.600E-01	15.0							1.600E-01	15.0
125 SN	936 2.000E-01	15.0							2.000E-01	15.0
127 SB	936 3.700E-01	15.0	-1.96	3.85	3.85	4.293E-01	(I) 10.8	(E) 21.3A	>2	
129 SB	936 1.290E+00	15.0	2.20	4.86	4.86	9.264E-01	(I) 10.9	(E) 24.0A	>2	
	936 7.900E-01	15.0	-2.20							
131 I	936 2.300E+00	15.0	2.76	7.62	7.62	2.747E+00	(I) 11.1	(E) 30.6A	>2	
	936 4.330E+00	15.0	2.76							
132 TE	936 4.350E+00	15.0	-0.71	0.50	0.50	4.652E+00	(I) 10.6A			
	936 5.060E+00	15.0	0.71							(E) 7.5
133 I	936 7.330E+00	15.0	0.45	0.20	0.20	7.605E+00	(I) 10.6A			
	936 8.070E+00	15.0	0.45							(E) 4.8
135 I	936 6.280E+00	15.0	-0.90	0.82	0.82	6.822E+00	(I) 10.7A			
	936 7.620E+00	15.0	0.90							(E) 9.6
139 BA	936 4.910E+00	15.0							4.910E+00	15.0
140 BA	936 5.710E+00	15.0	-0.09	0.01	0.01	5.764E+00	(I) 10.6A			
	936 5.820E+00	15.0	0.09							(E) 1.0
141 CE	936 5.390E+00	15.0	0.44	0.19	0.19	5.630E+00	(I) 10.6A			
	936 5.920E+00	15.0	0.44							(E) 4.7
142 LA	936 4.430E+00	15.0							4.430E+00	15.0
143 CE	936 4.350E+00	15.0	-0.57	0.07	0.07	4.472E+00	(I) 10.6A			
	936 4.30E+00	15.0	0.57							(E) 1.0
146 ND	936 3.400E+00	15.0							3.400E+00	15.0
147 ND	936 2.850E+00	15.0							2.850E+00	15.0

TABLE 160 CHAIN AND CUMULATIVE YIELDS FROM 8.000E+06 eV FISSION IN 238U .

(cont)

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
149 ND	936	2.030E+00	15.0	4.17	17.36	17.36	8.288E-01	(I) 11.8 >2
PM	936	6.900E-01	15.0	-4.17				(E) 49.3A
151 PM	936	5.400E-01	15.0	-1.21	1.46	1.46	5.997E-01	(I) 10.7
	936	7.000E-01	15.0	1.21				(E) 12.9A
153 SM	936	1.900E-01	15.0				1.900E-01	15.0

TABLE 161 CHAIN AND CUMULATIVE YIELDS FROM 8.100E+06 eV FISSION IN 238U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
84 BR	1105	1.110E+00	39.8				1.110E+00	39.8
87 KR	1105	1.740E+00	18.5				1.740E+00	18.5
89 SR	1105	2.610E+00	8.4				2.610E+00	8.4
91 SR	1105	3.770E+00	10.0				3.770E+00	10.0
95 ZR	1105	4.90E+00	9.8				4.90E+00	9.8
97 ZR	1105	5.400E+00	10.1				5.400E+00	10.1
99 MO	1105	6.060E+00	8.0				6.060E+00	8.0
103 RU	1105	5.220E+00	9.2				5.220E+00	9.2
104 TC	1105	4.560E+00	27.4				4.560E+00	27.4
105 RH	1105	3.560E+00	10.9				3.560E+00	10.9
111 AG	1105	1.950E-01	8.6				1.950E-01	8.6
112 PD	1105	1.690E-01	8.6				1.690E-01	8.6
115 CD(G)	1105	1.230E-01	7.9	1.230E-01				
CD(M)	1105	1.230E-02	33.8	1.230E-02				
127 SB	1105	5.390E-01	51.6				5.390E-01	51.6
129 SN	1105	4.600E-01	20.9				4.600E-01	20.9
130 SB	1105	7.330E-01	19.3				7.330E-01	19.3
132 TE	1105	4.660E+00	5.9				4.660E+00	5.9
133 I	1105	6.710E+00	14.6				6.710E+00	14.6
137 CS	1105	3.820E+00	20.2				3.820E+00	20.2
140 BA	1105	5.150E+00	8.2				5.150E+00	8.2
141 CE	1105	4.620E+00	9.7				4.620E+00	9.7
142 BA	1105	4.670E+00	37.6				4.670E+00	37.6
143 CE	1105	4.780E+00	10.1				4.780E+00	10.1
144 CE	1105	4.340E+00	9.7				4.340E+00	9.7
147 ND	1105	2.630E+00	9.9				2.630E+00	9.9
151 PM	1105	8.210E-01	17.3				8.210E-01	17.3
156 EU	1105	7.700E-02	14.3				7.700E-02	14.3

TABLE 162 CHAIN AND CUMULATIVE YIELDS FROM 8.270E+06 eV FISSION IN 238U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED	STANDARD
NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION		
83 CHAIN	30751 5.100E+01	7.8				5.100E+01	7.8		
84 CHAIN	30751 9.800E-01	6.1				9.800E-01	6.1		
85 CHAIN	30751 7.900E-01	6.3				7.900E-01	6.3		
87 CHAIN	30751 1.600E+00	5.0				1.600E+00	5.0		
88 CHAIN	30751 2.080E+00	5.3				2.080E+00	5.3		
89 CHAIN	30751 2.770E+00	5.0	-2.59			6.69	6.69 2.999E+00 (I)	3.6	>2
	30751 3.330E+00	5.0	2.59					(E)	9.2A
91 CHAIN	30751 4.140E+00	5.0	1.30			1.70	1.70 4.322E+00 (I)	4.6A	
	30751 4.540E+00	5.0						(E)	
92 CHAIN	30751 4.200E+00	5.0					4.200E+00	5.0	
93 CHAIN	30751 5.410E+00	5.0					5.410E+00	5.0	
94 CHAIN	30751 4.290E+00	5.0					4.290E+00	5.0	
95 CHAIN	30751 5.420E+00	5.0	-0.66			0.44	0.44 5.544E+00 (I)	3.5A	
	30751 5.680E+00	5.0	0.66					(E)	2.3
97 CHAIN	30751 6.010E+00	5.0	-0.67			0.45	0.45 5.863E+00 (I)	3.5A	
	30751 6.010E+00	5.0	0.67					(E)	2
99 CHAIN	30751 6.220E+00	5.0	-0.02			0.00	0.00 6.225E+00 (I)	3.5A	
	30751 6.230E+00	5.0	0.02					(E)	0.1
101 CHAIN	30751 6.130E+00	5.0					6.130E+00	5.0	
103 CHAIN	30751 5.190E+00	6.5	-1.81			3.27	3.27 5.650E+00 (I)	4.0	>2
	30751 6.010E+00	5.0	1.81					(E)	7.2A
104 CHAIN	30751 3.740E+00	5.0					3.740E+00	5.0	
105 CHAIN	30751 3.710E+00	5.0					3.710E+00	5.0	
106 CHAIN	30751 2.680E+00	6.7					2.680E+00	6.7	
107 CHAIN	30751 1.830E+00	5.0					1.830E+00	5.0	
109 CHAIN	30751 5.230E+00	5.3					5.230E+00	5.3	
111 CHAIN	30751 3.460E-01	8.7					3.460E-01	8.7	
112 CHAIN	30751 2.570E-01	5.0					2.570E-01	5.0	
113 CHAIN	30751 2.500E-01	5.0					2.500E-01	5.0	
115 CHAIN	30751 2.270E-01	5.0					2.270E-01	5.0	
121 CHAIN	30751 2.630E-01	9.5					2.630E-01	9.5	
125 SN (G)	30751 7.600E-02	5.0							
127 CHAIN	30751 5.600E-01	5.0	-3.66			13.38	13.38 6.225E-01 (I)	3.6	>2
	30751 7.280E-01	5.0	3.66					(E)	13.0A
128 CHAIN	30751 7.000E-01	5.0					7.000E-01	5.0	
129 CHAIN	30751 1.220E+00	5.0					1.220E+00	5.0	
130 SB (G)	30751 6.600E-01	6.1							
131 CHAIN	30751 3.160E+00	5.0	-0.57			0.32	0.32 3.222E+00 (I)	3.5A	
	30751 3.290E+00	5.0	0.57					(E)	2.0
132 CHAIN	30751 4.610E+00	5.0	-1.51			2.27	2.27 4.842E+00 (I)	3.5	>2
	30751 5.130E+00	5.0	1.51					(E)	5.3A
133 CHAIN	30751 7.210E+00	5.0					7.210E+00	5.0	
134 CHAIN	30751 6.550E+00	5.0					6.550E+00	5.0	
135 CHAIN	30751 6.750E+00	5.0					6.750E+00	5.0	
138 CHAIN	30751 5.870E+00	5.0					5.870E+00	5.0	
139 CHAIN	30751 4.490E+00	6.1					4.490E+00	6.1	
140 CHAIN	30751 5.640E+00	5.0	-0.17			0.03	0.03 5.675E+00 (I)	3.5A	
	30751 5.710E+00	5.0	0.17					(E)	0.6
141 CHAIN	30751 4.680E+00	5.1	-2.22			4.93	4.93 5.031E+00 (I)	3.6	>2

TABLE 162 CHAIN AND CUMULATIVE YIELDS FROM 8.270E+06 eV FISSION IN 238U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED	STANDARD
NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION		
142 CHAIN	30751 5.490E+00	5.0	2.22					(E)	8.0A
143 CHAIN	30751 4.210E+00	5.0					4.210E+00	5.0	
144 CHAIN	30751 4.660E+00	5.0					4.660E+00	5.0	
146 CHAIN	30751 3.620E+00	5.0					3.620E+00	5.0	
147 CHAIN	30751 2.580E+00	5.0	-0.64			0.41	0.41 2.637E+00 (I)	3.5A	
	30751 2.700E+00	5.0	0.64					(E)	2.3
151 CHAIN	30751 7.070E-01	5.0					7.070E-01	5.0	
153 CHAIN	30751 4.340E-01	5.0					4.340E-01	5.0	
156 CHAIN	30751 9.050E-02	7.3					9.050E-02	7.3	
161 CHAIN	30751 4.000E-03	7.5					4.000E-03	7.5	

TABLE 163 CHAIN AND CUMULATIVE YIELDS FROM 9.100E+06 eV FISSION IN 238U .

A EL.	REF.	EXPERIMENTAL	NO.	YIELDS & SD	MEAN	R	CHI2/DF	CHI2	EXTERNAL	INT.	EXT./DF	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	NO.	YIELDS & SD	MEAN	R	CHI2/DF	CHI2	EXTERNAL	INT.	EXT./DF	TOTAL	CHI2	WEIGHTED	STANDARD
84 BR	1106	8.940E+01	39.9											8.940E+01	39.9
87 KR	1106	1.910E+00	21.7											1.910E+00	21.7
89 SR	1106	2.420E+00	10.9											2.420E+00	10.9
91 SR	1106	4.020E+00	11.2											4.020E+00	11.2
95 ZR	1106	4.990E+00	9.4											4.990E+00	9.4
97 ZR	1106	5.280E+00	11.5											5.280E+00	11.5
99 MO	1106	5.980E+00	9.3											5.980E+00	9.3
103 RU	1106	4.870E+00	12.1											4.870E+00	12.1
104 TC	1106	4.510E+00	27.3											4.510E+00	27.3
105 RH	1106	2.660E+00	14.9											2.660E+00	14.9
111 AG	1106	2.690E+01	9.9											2.690E+01	9.9
112 PD	1106	2.230E+01	10.0											2.230E+01	10.0
115 CD(G)	1106	1.690E+01	8.5	1.690E-01						0.00	0.00	1.911E-01	(I)	8.4A	
CD(M)	1106	2.210E-02	33.1	2.210E-02											
127 SB	1106	5.110E+01	18.5											5.110E+01	18.5
129 SN	1106	5.670E+01	23.0											5.670E+01	23.0
130 SB	1106	7.520E+01	22.2											7.520E+01	22.2
132 TE	1106	4.300E+00	9.5											4.300E+00	9.5
133 I	1106	6.310E+00	16.0											6.310E+00	16.0
137 CS	1106	5.340E+00	18.9											5.340E+00	18.9
140 BA	1106	4.980E+00	9.7											4.980E+00	9.7
141 CE	1106	4.410E+00	11.2											4.410E+00	11.2
142 LA	1106	4.110E+00	22.0											4.110E+00	22.0
143 CE	1106	4.370E+00	11.6											4.370E+00	11.6
144 CE	1106	4.270E+00	11.1											4.270E+00	11.1
147 ND	1106	2.440E+00	12.2											2.440E+00	12.2
151 PM	1106	1.040E+00	56.2											1.040E+00	56.2
156 EU	1106	8.340E+02	16.5											8.340E+02	16.5

TABLE 164 CHAIN AND CUMULATIVE YIELDS FROM 1.400E+07 eV FISSION IN 238U .

A EL.	REF.	EXPERIMENTAL	NO.	YIELDS & SD	MEAN	R	CHI2/DF	CHI2	EXTERNAL	INT.	EXT./DF	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	NO.	YIELDS & SD	MEAN	R	CHI2/DF	CHI2	EXTERNAL	INT.	EXT./DF	TOTAL	CHI2	WEIGHTED	STANDARD
4 HE FI	2050	1.258E-01	40.0											1.03	0.52
														7.513E-02	(E)
														8.5A	
	2053	7.407E-02	15.0											-0.12	
	2052	7.442E-02	10.6											-0.15	

TABLE 165 CHAIN AND CUMULATIVE YIELDS FROM 1.440E+07 eV FISSION IN 238U .

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
85 KR(G)	13116	2.500E-01	50.0						
156 EU	13116	1.040E-01	50.0					1.040E-01	50.0
161 TB	13116	6.890E-03	50.0					6.890E-03	50.0

TABLE 166 CHAIN AND CUMULATIVE YIELDS FROM 3.000E-01 eV FISSION IN 239PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
91 SR	1107	2.400E+00	8.0					2.400E+00	8.0
111 AG	1107	2.800E-01	14.0					2.800E-01	14.0
112 AG	1107	1.300E-01	15.0					1.300E-01	15.0
113 AG(G)	1107	7.600E-02	13.0					7.600E-02	13.0
115 CD(G)	1107	2.400E-02	25.0					2.400E-02	25.0
117 CD	1107	1.800E-02	22.0					1.800E-02	22.0
118 CD	1107	3.000E-02	60.0					3.000E-02	60.0

TABLE 167 CHAIN AND CUMULATIVE YIELDS FROM 1.300E+05 eV FISSION IN 239PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION	
99 NO	1053	5.240E+00	6.0				5.240E+00	6.0	
111 AG	1053	2.900E-01	7.0				2.900E-01	7.0	
140 BA	1053	4.960E+00	7.0				4.960E+00	7.0	
147 ND	1053	2.190E+00	7.0				2.190E+00	7.0	
153 SM	1053	3.000E-01	12.0				3.000E-01	12.0	

TABLE 168 CHAIN AND CUMULATIVE YIELDS FROM 1.400E+05 eV FISSION IN 239PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION	
3 H	PI 30498	3.461E-03	80.2				3.461E-03	80.2	
4 HE	PI 30498	2.059E-01	4.5				2.059E-01	4.5	

TABLE 169 CHAIN AND CUMULATIVE YIELDS FROM 1.700E+05 eV FISSION IN 239PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT VALUE	EXT.	INT.	EXT./DF	INT.	DEVIATION
87 KR	12817	7.600E-01	13.2						13.2
88 KR	12817	1.130E+00	8.8						8.8
91 SR	12817	2.720E+00	5.9						5.9
92 SR	12817	3.050E+00	12.5						12.5
93 Y	12817	4.160E+00	9.6						9.6
97 ZR	12817	5.670E+00	5.6						5.6
99 MO	12817	6.290E+00	6.7						6.7
103 RU	12817	7.570E+00	6.6						6.6
105 RU	12817	6.030E+00	9.1						9.1
109 PD	12817	1.140E+00	14.9						14.9
111 AG	12817	2.500E-01	16.0						16.0
112 PD	12817	1.400E-01	14.3						14.3
115 CD	12817	2.700E-02	14.8						14.8
121 SN	12817	3.200E-02	15.6						15.6
125 SN	12817	3.900E-02	15.4						15.4
127 SB	12817	3.400E-01	14.7						14.7
129 SB	12817	1.180E+00	20.3						20.3
132 TE	12817	5.520E+00	6.9						6.9
133 I	12817	7.640E+00	5.9						5.9
135 I	12817	6.890E+00	5.4						5.4
140 BA	12817	5.490E+00	6.0						6.0
142 LA	12817	4.680E+00	6.4						6.4
143 CE	12817	4.570E+00	7.9						7.9

TABLE 170 CHAIN AND CUMULATIVE YIELDS FROM 1.750E+05 eV FISSION IN 239PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT VALUE	EXT.	INT.	EXT./DF	INT.	DEVIATION
3 H	PI 30498	3.605E-02	80.2						80.2
4 H	PI 30498	2.080E-01	4.5						4.5

TABLE 171 CHAIN AND CUMULATIVE YIELDS FROM 2.000E+05 eV FISSION IN 239PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	INT. EXT./DF	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT VALUE	COMPONENT	EXTERNAL	EXTERNAL	INT.	EXT.	DEVIATION
3 H	PI	30498±1.716E-02	80.2							80.2
4 HE	PI	30498±2.163E-01	5.1							5.1

TABLE 172 CHAIN AND CUMULATIVE YIELDS FROM 2.650E+05 eV FISSION IN 239PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	INT. EXT./DF	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT VALUE	COMPONENT	EXTERNAL	EXTERNAL	INT.	EXT.	DEVIATION
3 H	PI	30498±5.047E-02	90.2							90.2
4 HE	PI	30498±2.226E-01	5.0							5.0

TABLE 173 CHAIN AND CUMULATIVE YIELDS FROM 3.00E+05 eV FISSION IN 239PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	INT. EXT./DF	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INTERNAL	EXTERNAL	INTERNAL	EXT./DF	DEVIATION
3 H	PI	30498±2.684E-02	80.2							80.2
4 HE	PI	30498±1.934E-01	4.6							4.6

TABLE 174 CHAIN AND CUMULATIVE YIELDS FROM 3.30E+05 eV FISSION IN 239PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	INT. EXT./DF	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INTERNAL	EXTERNAL	INTERNAL	EXT./DF	DEVIATION
4 HE	PI	2057±2.184E-01	10.5							10.5
										2.184E-01

TABLE 175 CHAIN AND CUMULATIVE YIELDS FROM 5.000E+05 eV FISSION IN 239PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	INT. EXT./DF	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT VALUE	COMPONENT	EXTERNAL	EXTERNAL	EXTERNAL	INT. EXT./DF	DEVIATION
3 H	PI	2043r1.410E-02	21.7						21.7	21.7
4 HE	PI	2043r2.028E-01	7.7						7.7	7.7

TABLE 176 CHAIN AND CUMULATIVE YIELDS FROM 5.750E+05 eV FISSION IN 239PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	INT. EXT./DF	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT VALUE	COMPONENT	EXTERNAL	EXTERNAL	EXTERNAL	INT. EXT./DF	DEVIATION
3 H	PI	30498r4.182E-03	80.2						80.2	80.2
4 HE	PI	30498r2.246E-01	4.3						4.3	4.3

TABLE 177 CHAIN AND CUMULATIVE YIELDS FROM 6.900E+05 eV FISSION IN 239PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
4 HE PI	2057	1.872E-01	15.4					1.872E-01	15.4

TABLE 178 CHAIN AND CUMULATIVE YIELDS FROM 7.000E+05 eV FISSION IN 239PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION
99 MO	1055	5.650E+00	8.0					5.650E+00	8.0
111 AG	1055	3.200E-01	7.0					3.200E-01	7.0
140 BA	1055	5.960E+00	13.0					5.960E+00	13.0
147 ND	1055	2.460E+00	7.0					2.460E+00	7.0
153 SM	1055	3.600E-01	16.0					3.600E-01	16.0

TABLE 179 CHAIN AND CUMULATIVE YIELDS FROM 7.680E+05 eV FISSION IN 239PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	INT. EXT./DF	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT VALUE	COMPONENT	EXTERNAL	EXTERNAL	EXTERNAL	INT. EXT./DF	DEVIATION
3 H	PI	2043r1.159E-02	32.4							32.4
4 HE	PI	2043r2.259E-01	6.8							6.8

TABLE 180 CHAIN AND CUMULATIVE YIELDS FROM 7.900E+05 eV FISSION IN 239PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	INT. EXT./DF	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT VALUE	COMPONENT	EXTERNAL	EXTERNAL	EXTERNAL	INT. EXT./DF	DEVIATION
3 H	PI	30498r1.009E-03	80.2							80.2
4 HE	PI	30498r2.101E-01	4.4							4.4

TABLE 181 CHAIN AND CUMULATIVE YIELDS FROM 9.000E+05 eV FISSION IN 239PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	INT. EXT./DF	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	MEAN	COMPONENT	EXTERNAL	INTERNAL	EXTERNAL	INTERNAL	DEVIATION
99 NO	1056	5.580E+00	9.0							9.0
111 AG	1056	3.300E-01	9.0							5.580E+00
140 BA	1056	5.340E+00	10.0							3.300E-01
147 ND	1056	2.380E+00	6.0							5.340E+00
153 SM	1056	3.500E-01	10.0							2.380E+00

TABLE 182 CHAIN AND CUMULATIVE YIELDS FROM 9.900E+05 eV FISSION IN 239PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	INT. EXT./DF	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	MEAN	COMPONENT	EXTERNAL	INTERNAL	EXTERNAL	INTERNAL	DEVIATION
3 H PI	30498	4.470E-03	80.2							80.2
4 HE PI	30498	2.226E-01	5.0							4.470E-03

TABLE 183 CHAIN AND CUMULATIVE YIELDS FROM 1.000E+06 eV FISSION IN 239PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	INT.	EXT./DF	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	COMPONENT	VALUE	COMPONENT	EXTERNAL	EXTERNAL	INTERNAL	INTERNAL	EXT.	EXT.	MEAN	DEVIATION
3 H	PI	2043r1.661E-02	18.8									1.661E-02	18.8
4 HE	PI	2043r2.330E-01	6.0	-0.53				0.28	0.28	2.366E-01	(I)	5.1A	
		856 2.481E-01	10.0	0.53							(E)	2.7	
87 KE		12817 8.300E-01	10.8							8.300E-01		10.8	
88 KE		12817 1.160E+00	7.8							1.160E+00		7.8	
91 SR		12817 2.710E+00	5.5							2.710E+00		5.5	
92 SR		12817 3.000E+00	12.7							3.000E+00		12.7	
93 Y		12817 4.430E+00	9.5							4.430E+00		9.5	
97 ZR		12817 5.370E+00	6.2							5.370E+00		6.2	
99 MO		12817 6.030E+00	6.6							6.030E+00		6.6	
100 RU		12817 5.610E+00	5.6							5.610E+00		5.6	
105 RU		12817 5.440E+00	7.9							5.440E+00		7.9	
109 PD		12817 9.400E-01	14.9							9.400E-01		14.9	
111 AG		12817 2.400E-01	16.7							2.400E-01		16.7	
115 CD		12817 3.600E-02	13.9							3.600E-02		13.9	
121 SN		12817 4.400E-02	15.9							4.400E-02		15.9	
125 SN		12817 5.200E-02	15.4							5.200E-02		15.4	
127 SB		12817 3.700E-01	16.2							3.700E-01		16.2	
129 SB		12817 1.200E+00	20.0							1.200E+00		20.0	
132 TE		12817 5.110E+00	6.8							5.110E+00		6.8	
133 I		12817 7.020E+00	5.8							7.020E+00		5.8	
134 TE		12817 4.140E+00	7.5							4.140E+00		7.5	
135 I		12817 6.290E+00	5.4							6.290E+00		5.4	
140 BA		12817 5.120E+00	5.9							5.120E+00		5.9	
142 LA		12817 4.490E+00	8.2							4.490E+00		8.2	
143 CE		12817 4.400E+00	8.0							4.400E+00		8.0	

TABLE 184 CHAIN AND CUMULATIVE YIELDS FROM 1.300E+06 eV FISSION IN 239PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	INT.	EXT./DF	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	COMPONENT	VALUE	COMPONENT	EXTERNAL	EXTERNAL	INTERNAL	INTERNAL	EXT.	EXT.	MEAN	DEVIATION
99 MO		1057 5.360E+00	8.0									5.360E+00	8.0
111 AG		1057 3.600E-01	8.0									3.600E-01	8.0
140 BA		1057 5.220E+00	7.0									5.220E+00	7.0
147 ND		1057 2.250E+00	10.0									2.250E+00	10.0
153 SM		1057 3.600E-01	15.0									3.600E-01	15.0

TABLE 185 CHAIN AND CUMULATIVE YIELDS FROM 1.700E+06 eV FISSION IN 239PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXT.	INT.	EXT./DF	INT.	DEVIATION
99 NO	1058	5.610E+00	6.0						6.0
111 AG	1058	3.800E-01	6.0						6.0
140 BA	1058	5.420E+00	9.0						9.0
147 ND	1058	2.600E+00	8.0						8.0
153 SM	1058	3.600E-01	6.0						6.0
156 EU	1058	8.700E-02	6.0						6.0

TABLE 186 CHAIN AND CUMULATIVE YIELDS FROM 1.990E+06 eV FISSION IN 239PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2	WEIGHTED STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	COMPONENT	EXT.	INT.	EXT./DF	INT.	DEVIATION
4 HE FI	2057	2.236E-01	30.2						30.2

TABLE 187 CHAIN AND CUMULATIVE YIELDS FROM 2.000E+06 eV FISSION IN 239PU.

A EL. NO.	REF.	EXPERIMENTAL YIELDS & SD.	MEAN COMPONENT VALUE	R TOTAL	CHI2/DF	CHI2	EXT.	DF	WEIGHTED MEAN	STANDARD DEVIATION
3 H	PI	2043r1.330E-02	23.6						1.330E-02	23.6
4 HE	PI	2043r2.001E-01	6.0						2.001E-01	6.0
87 RB		12817 9.300E-01	9.7						9.300E-01	9.7
88 RB		12817 1.420E+00	7.0						1.420E+00	7.0
91 SR		12817 2.940E+00	5.8						2.940E+00	5.8
92 SR		12817 3.360E+00	12.5						3.360E+00	12.5
93 Y		12817 4.860E+00	9.5						4.860E+00	9.5
97 ZR		12817 5.830E+00	5.7						5.830E+00	5.7
99 MO		12817 6.300E+00	7.0						6.300E+00	7.0
103 RU		12817 6.970E+00	6.7						6.970E+00	6.7
105 RU		12817 5.490E+00	6.9						5.490E+00	6.9
109 PD		12817 1.100E+00	15.5						1.100E+00	15.5
111 AG		12817 2.800E-01	14.3						2.800E-01	14.3
112 PD		12817 1.600E-01	12.5						1.600E-01	12.5
115 CD		12817 5.000E-02	16.0						5.000E-02	16.0
121 SN		12817 4.800E-02	14.6						4.800E-02	14.6
125 SN		12817 5.800E-02	15.5						5.800E-02	15.5
127 SB		12817 3.500E-01	14.3						3.500E-01	14.3
129 SB		12817 1.270E+00	19.7						1.270E+00	19.7
132 TE		12817 5.320E+00	9.6						5.320E+00	9.6
133 I		12817 7.320E+00	5.9						7.320E+00	5.9
134 TE		12817 4.360E+00	8.5						4.360E+00	8.5
139 I		12817 6.670E+00	5.1						6.670E+00	5.1
140 BA		12817 5.370E+00	6.0						5.370E+00	6.0
142 LA		12817 4.920E+00	8.9						4.920E+00	8.9
143 CB		12817 4.440E+00	7.7						4.440E+00	7.7

TABLE 188 CHAIN AND CUMULATIVE YIELDS FROM 3.000E+06 eV FISSION IN 239PU.

A EL. NO.	REF.	EXPERIMENTAL YIELDS & SD.	MEAN COMPONENT VALUE	R TOTAL	CHI2/DF	CHI2	EXT.	DF	WEIGHTED MEAN	STANDARD DEVIATION
91 SR		2046 2.180E+00	13.0						2.180E+00	13.0
92 SR		2046 2.850E+00	11.0						2.850E+00	11.0
99 MO		1054 5.420E+00	8.0						5.420E+00	8.0
105 RU		2046 5.460E+00	11.0						5.460E+00	11.0
111 AG		1054 2.800E-01	16.0						2.800E-01	16.0
127 SN		2046 7.800E-01	24.0						7.800E-01	24.0
129 SB		2046 2.730E+00	15.0						2.730E+00	15.0
130 SB		2046 1.010E+00	11.0						1.010E+00	11.0
131 TE(M)		2046 1.100E+00	13.0						1.100E+00	13.0
133 I		2046 6.590E+00	11.0						6.590E+00	11.0
134 TE		2046 3.330E+00	17.0						3.330E+00	17.0
I		2046 7.310E+00	14.0						7.310E+00	14.0
135 I		2046 5.740E+00	11.0						5.740E+00	11.0
138 LA		2046 7.050E+00	11.0						7.050E+00	11.0
140 BA		1054 5.220E+00	6.0						5.220E+00	6.0
LA		2046 6.200E+00	11.0						6.200E+00	11.0
147 ND		1054 2.220E+00	6.0						2.220E+00	6.0
153 SM		1054 3.300E-01	16.0						3.300E-01	16.0

TABLE 189 CHAIN AND CUMULATIVE YIELDS FROM 3.400E+06 eV FISSION IN 239PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION	
87 KR	12817	1.040E+00	10.6				1.040E+00	10.6	
88 KR	12817	1.590E+00	6.9				1.590E+00	6.9	
91 SR	12817	3.180E+00	5.7				3.180E+00	5.7	
92 SR	12817	3.480E+00	12.4				3.480E+00	12.4	
93 Y	12817	4.670E+00	8.3				4.670E+00	8.3	
97 ZR	12817	5.840E+00	6.7				5.840E+00	6.7	
99 MO	12817	6.210E+00	6.8				6.210E+00	6.8	
103 RU	12817	6.680E+00	7.2				6.680E+00	7.2	
105 RU	12817	5.470E+00	8.6				5.470E+00	8.6	
109 PD	12817	1.120E+00	15.2				1.120E+00	15.2	
111 AG	12817	4.500E-01	15.6				4.500E-01	15.6	
112 PD	12817	2.600E-01	15.4				2.600E-01	15.4	
115 CD	12817	1.100E-01	18.2				1.100E-01	18.2	
121 SN	12817	8.500E-02	15.3				8.500E-02	15.3	
125 SN	12817	1.200E-01	16.7				1.200E-01	16.7	
127 SB	12817	7.600E-01	14.5				7.600E-01	14.5	
129 SB	12817	1.770E+00	19.8				1.770E+00	19.8	
132 TE	12817	4.990E+00	5.6				4.990E+00	5.6	
133 I	12817	7.060E+00	5.8				7.060E+00	5.8	
135 I	12817	3.280E+00	9.8				3.280E+00	9.8	
135 I	12817	6.430E+00	5.8				6.430E+00	5.8	
140 BA	12817	5.100E+00	5.9				5.100E+00	5.9	
142 LA	12817	4.500E+00	8.0				4.500E+00	8.0	
143 CE	12817	4.220E+00	7.8				4.220E+00	7.8	

TABLE 190 CHAIN AND CUMULATIVE YIELDS FROM 4.500E+06 eV FISSION IN 239PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	TOTAL CHI2	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION	
87 KR	12817	1.380E+00	8.0				1.380E+00	8.0	
88 KR	12817	1.610E+00	7.5				1.610E+00	7.5	
91 SR	12817	3.240E+00	5.6				3.240E+00	5.6	
92 SR	12817	3.700E+00	12.4				3.700E+00	12.4	
93 Y	12817	5.410E+00	10.4				5.410E+00	10.4	
97 ZR	12817	5.930E+00	5.9				5.930E+00	5.9	
99 MO	12817	6.360E+00	6.9				6.360E+00	6.9	
103 RU	12817	5.830E+00	16.3				5.830E+00	16.3	
105 RU	12817	5.530E+00	7.4				5.530E+00	7.4	
109 PD	12817	1.410E+00	14.9				1.410E+00	14.9	
111 AG	12817	6.300E-01	14.3				6.300E-01	14.3	
112 PD	12817	3.600E-01	13.9				3.600E-01	13.9	
121 SN	12817	1.300E-01	15.4				1.300E-01	15.4	
125 SN	12817	1.700E-01	17.6				1.700E-01	17.6	
127 SB	12817	7.700E-01	15.6				7.700E-01	15.6	
129 SB	12817	1.650E+00	20.0				1.650E+00	20.0	
132 TE	12817	5.370E+00	10.4				5.370E+00	10.4	
133 I	12817	7.090E+00	5.9				7.090E+00	5.9	
134 TE	12817	3.570E+00	8.4				3.570E+00	8.4	
135 I	12817	6.380E+00	11.1				6.380E+00	11.1	
140 BA	12817	5.620E+00	6.0				5.620E+00	6.0	
142 LA	12817	5.000E+00	8.0				5.000E+00	8.0	
143 CE	12817	4.150E+00	8.0				4.150E+00	8.0	

TABLE 191 CHAIN AND CUMULATIVE YIELDS FROM 6.100E+06 eV FISSION IN 239PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD.	COMPONENT	VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION		
87 KR	12817	8.100E+01	18.5					6.100E+01	18.5		
88 KR	12817	1.650E+00	12.7					1.650E+00	12.7		
91 SR	12817	3.070E+00	7.2					3.070E+00	7.2		
92 SR	12817	3.530E+00	12.5					3.530E+00	12.5		
93 Y	12817	4.960E+00	17.3					4.960E+00	17.3		
97 ZR	12817	5.990E+00	10.9					5.990E+00	10.9		
105 RU	12817	4.710E+00	9.6					4.710E+00	9.6		
109 PD	12817	1.210E+00	14.9					1.210E+00	14.9		
111 AG	12817	3.800E-01	26.3					3.800E-01	26.3		
112 PD	12817	4.700E-01	14.9					4.700E-01	14.9		
115 CD	12817	2.700E-01	14.8					2.700E-01	14.8		
121 SN	12817	2.200E-01	13.6					2.200E-01	13.6		
125 SN	12817	1.600E-01	12.5					1.600E-01	12.5		
127 SB	12817	8.200E-01	14.6					8.200E-01	14.6		
129 SB	12817	1.580E+00	20.3					1.580E+00	20.3		
132 TE	12817	5.070E+00	10.3					5.070E+00	10.3		
133 I	12817	6.300E+00	5.9					6.300E+00	5.9		
134 TE	12817	2.450E+00	11.0					2.450E+00	11.0		
135 I	12817	5.400E+00	5.7					5.400E+00	5.7		
140 BA	12817	5.620E+00	6.2					5.620E+00	6.2		

TABLE 192 CHAIN AND CUMULATIVE YIELDS FROM 7.900E+06 eV FISSION IN 239PU.

A EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	CHI2	CHI2	TOTAL	CHI2	WEIGHTED	STANDARD
NO.	NO.	YIELDS & SD.	COMPONENT	VALUE	EXTERNAL	INT.	EXT./DF	MEAN	DEVIATION		
87 KR	12817	9.300E-01	17.2					9.300E-01	17.2		
88 KR	12817	1.730E+00	11.6					1.730E+00	11.6		
91 SR	12817	3.030E+00	6.3					3.030E+00	6.3		
92 SR	12817	3.510E+00	12.5					3.510E+00	12.5		
93 Y	12817	4.030E+00	12.4					4.030E+00	12.4		
97 ZR	12817	5.130E+00	10.1					5.130E+00	10.1		
99 MO	12817	5.490E+00	7.1					5.490E+00	7.1		
103 RU	12817	5.660E+00	6.9					5.660E+00	6.9		
105 RU	12817	4.740E+00	8.7					4.740E+00	8.7		
109 PD	12817	1.160E+00	14.7					1.160E+00	14.7		
111 AG	12817	6.600E-01	15.2					6.600E-01	15.2		
112 PD	12817	5.900E-01	15.3					5.900E-01	15.3		
125 SN	12817	3.100E-01	16.1					3.100E-01	16.1		
127 SB	12817	1.080E+00	14.8					1.080E+00	14.8		
129 SB	12817	1.670E+00	19.8					1.670E+00	19.8		
132 TE	12817	4.920E+00	7.9					4.920E+00	7.9		
133 I	12817	6.240E+00	5.8					6.240E+00	5.8		
134 TE	12817	2.860E+00	8.4					2.860E+00	8.4		
135 I	12817	5.210E+00	5.6					5.210E+00	5.6		
140 BA	12817	5.480E+00	6.2					5.480E+00	6.2		

TABLE 193 CHAIN AND CUMULATIVE YIELDS FROM 1.480E+07 eV FISSION IN 239PU.

A	EL.	REF.	EXPERIMENTAL	MEAN	R	CHI2/DF	DCHI2	CHI2	TOTAL CHI2
NO.	YIELDS & SD	COMPONENT VALUE	EXTERNAL	INT.	EXT./DF	MEAN	STANDARD		
85	KR(G)	13116	2.320E-01	50.0					
156	EU	13116	1.940E-01	50.0					
161	TB	13116	2.290E-02	50.0					

TABLE 12 LIST OF DISCREPANT CHAIN YIELDS

FISSILE NUCLEUS: 95-AM-242, NEUTRON ENERGY: THERMAL.

MASS NUMBER	NUMBER OF MEASUREMENTS	MAX.DCH2 CONTRIBUTING MEASUREMENT & DCH2	TOTAL CH2 YIELD IN DATABASE	PROBABILITY PC.
160	NO		
161	1	568	ONE MEASUREMENT ONLY	
162	NO		

FISSILE NUCLEUS: 96-CM-243 , NEUTRON ENERGY: THERMAL.

[illegible]

TABLE 14 LIST OF DISCREPANT CHAIN YIELDS

FISSILE NUCLEUS: 96-CM-245, NEUTRON ENERGY: THERMAL.

MASS	NUMBER	NUMBER OF MEASUREMENTS	MAX DCH12 CONTRIBUTING MEASUREMENT	DCH12	TOTAL	PROBABILITY PC.
71	72	1NONO	YIELD IN DATABASENO
72	73	1NONO	YIELD IN DATABASENO
73	74	1NONO	YIELD IN DATABASENO
74	75	1NONO	YIELD IN DATABASENO
75	76	1NONO	YIELD IN DATABASENO
76	77	1NONO	YIELD IN DATABASENO
77	78	1NONO	YIELD IN DATABASENO
78	79	1NONO	YIELD IN DATABASENO
79	80	1NONO	YIELD IN DATABASENO
80	81	1NONO	YIELD IN DATABASENO
81	82	1NONO	YIELD IN DATABASENO
82	83	1NONO	YIELD IN DATABASENO
83	84	1NONO	YIELD IN DATABASENO
84	85	1NONO	YIELD IN DATABASENO
85	86	1NONO	YIELD IN DATABASENO
86	87	1NONO	YIELD IN DATABASENO
87	88	1NONO	YIELD IN DATABASENO
88	89	1NONO	YIELD IN DATABASENO
89	90	1NONO	YIELD IN DATABASENO
90	91	1NONO	YIELD IN DATABASENO
91	92	1NONO	YIELD IN DATABASENO
92	93	1NONO	YIELD IN DATABASENO
93	94	1NONO	YIELD IN DATABASENO
94	95	1NONO	YIELD IN DATABASENO
95	96	1NONO	YIELD IN DATABASENO
96	97	1NONO	YIELD IN DATABASENO
97	98	1NONO	YIELD IN DATABASENO
98	99	1NONO	YIELD IN DATABASENO
99	100	1NONO	YIELD IN DATABASENO
100	101	1NONO	YIELD IN DATABASENO
101	102	1NONO	YIELD IN DATABASENO
102	103	1NONO	YIELD IN DATABASENO
103	104	1NONO	YIELD IN DATABASENO
104	105	1NONO	YIELD IN DATABASENO
105	106	1NONO	YIELD IN DATABASENO
106	107	1NONO	YIELD IN DATABASENO
107	108	1NONO	YIELD IN DATABASENO
108	109	1NONO	YIELD IN DATABASENO
109	110	1NONO	YIELD IN DATABASENO
110	111	1NONO	YIELD IN DATABASENO
111	112	1NONO	YIELD IN DATABASENO
112	113	1NONO	YIELD IN DATABASENO
113	114	1NONO	YIELD IN DATABASENO
114	115	1NONO	YIELD IN DATABASENO
115	116	1NONO	YIELD IN DATABASENO
116	117	1NONO	YIELD IN DATABASENO
117	118	1NONO	YIELD IN DATABASENO
118	119	1NONO	YIELD IN DATABASENO
119	120	1NONO	YIELD IN DATABASENO
120	121	1NONO	YIELD IN DATABASENO
121	122	1NONO	YIELD IN DATABASENO
122	123	1NONO	YIELD IN DATABASENO
123	124	1NONO	YIELD IN DATABASENO
124	125	1NONO	YIELD IN DATABASENO
125	126	1NONO	YIELD IN DATABASENO
126	127	1NONO	YIELD IN DATABASENO
127	128	1NONO	YIELD IN DATABASENO
128	129	1NONO	YIELD IN DATABASENO
129	130	1NONO	YIELD IN DATABASENO
130	131	1NONO	YIELD IN DATABASENO
131	132	1NONO	YIELD IN DATABASENO
132	133	1NONO	YIELD IN DATABASENO
133	134	1NONO	YIELD IN DATABASENO
134	135	1NONO	YIELD IN DATABASENO
135	136	1NONO	YIELD IN DATABASENO
136	137	1NONO	YIELD IN DATABASENO
137	138	1NONO	YIELD IN DATABASENO
138	139	1NONO	YIELD IN DATABASENO
139	140	1NONO	YIELD IN DATABASENO
140	141	1NONO	YIELD IN DATABASENO
141	142	1NONO	YIELD IN DATABASENO
142	143	1NONO	YIELD IN DATABASENO
143	144	1NONO	YIELD IN DATABASENO

TABLE 47 LIST OF DISCREPANT CHAIN YIELDS
FABLE NUCLEUS: 91-PA-231, NEUTRON ENERGY: HIGH.

MASS NUMBER	NUMBER OF MEASUREMENTS	MAX DCH12 MEASUREMENT	CONTRIBUTING MEASUREMENT & DCH12	TOTAL CH12	PC PROBABILITY
71	YIELD IN DATABASE
72	YIELD IN DATABASE
73	YIELD IN DATABASE
74	YIELD IN DATABASE
75	YIELD IN DATABASE
76	YIELD IN DATABASE
77	YIELD IN DATABASE
78	YIELD IN DATABASE
79	YIELD IN DATABASE
80	YIELD IN DATABASE
81	YIELD IN DATABASE
82	YIELD IN DATABASE
83	YIELD IN DATABASE
84	1	645	ONE MEASUREMENT ONLY	YIELD IN DATABASE
85	YIELD IN DATABASE
86	YIELD IN DATABASE
87	YIELD IN DATABASE
88	YIELD IN DATABASE
89	YIELD IN DATABASE
90	YIELD IN DATABASE
91	1	645	ONE MEASUREMENT ONLY	YIELD IN DATABASE
92	YIELD IN DATABASE
93	1	645	ONE MEASUREMENT ONLY	YIELD IN DATABASE
94	YIELD IN DATABASE
95	YIELD IN DATABASE
96	YIELD IN DATABASE
97	1	645	ONE MEASUREMENT ONLY	YIELD IN DATABASE
98	YIELD IN DATABASE
99	YIELD IN DATABASE
100	YIELD IN DATABASE
101	YIELD IN DATABASE
102	YIELD IN DATABASE
103	YIELD IN DATABASE
104	YIELD IN DATABASE
105	1	645	ONE MEASUREMENT ONLY	YIELD IN DATABASE
106	YIELD IN DATABASE
107	YIELD IN DATABASE
108	YIELD IN DATABASE
109	YIELD IN DATABASE
110	YIELD IN DATABASE
111	YIELD IN DATABASE
112	1	645	ONE MEASUREMENT ONLY	YIELD IN DATABASE
113	1	645	ONE MEASUREMENT ONLY	YIELD IN DATABASE
114	YIELD IN DATABASE
115	YIELD IN DATABASE
116	YIELD IN DATABASE
117	YIELD IN DATABASE
118	YIELD IN DATABASE
119	YIELD IN DATABASE
120	YIELD IN DATABASE
121	YIELD IN DATABASE
122	YIELD IN DATABASE
123	YIELD IN DATABASE
124	YIELD IN DATABASE
125	YIELD IN DATABASE
126	YIELD IN DATABASE
127	YIELD IN DATABASE
128	YIELD IN DATABASE
129	1	645	ONE MEASUREMENT ONLY	YIELD IN DATABASE
130	YIELD IN DATABASE
131	1	645	ONE MEASUREMENT ONLY	YIELD IN DATABASE
132	1	169	ONE MEASUREMENT ONLY	YIELD IN DATABASE
133	1	169	ONE MEASUREMENT ONLY	YIELD IN DATABASE
134	YIELD IN DATABASE
135	YIELD IN DATABASE
136	YIELD IN DATABASE
137	YIELD IN DATABASE
138	YIELD IN DATABASE
139	YIELD IN DATABASE
140	YIELD IN DATABASE
141	YIELD IN DATABASE
142	YIELD IN DATABASE
143	1	645	ONE MEASUREMENT ONLY	YIELD IN DATABASE
144	YIELD IN DATABASE
145	YIELD IN DATABASE
146	YIELD IN DATABASE
147	YIELD IN DATABASE
148	YIELD IN DATABASE
149	YIELD IN DATABASE
150	YIELD IN DATABASE
151	YIELD IN DATABASE
152	YIELD IN DATABASE
153	YIELD IN DATABASE
154	YIELD IN DATABASE
155	YIELD IN DATABASE
156	YIELD IN DATABASE
157	YIELD IN DATABASE
158	YIELD IN DATABASE
159	YIELD IN DATABASE

TABLE 48 LIST OF DISCREPANT CHAIN YIELDS

[illegible]

TABLE 48 LIST OF DISCREPANT CHAIN YIELDS (cont)

MASS NUMBER	NUMBER OF MEASUREMENTS	MAX. DCH12 CONTRIBUTING TO MEASUREMENT	TOTAL PROBABILITY
170	NO YIELD IN DATABASE	CH12
171	NO YIELD IN DATABASE	PC
172	NO YIELD IN DATABASE	
173	1	565 ONE MEASUREMENT ONLY	
174	NO YIELD IN DATABASE	
175	1	565 ONE MEASUREMENT ONLY	

TABLE 49 LIST OF DISCREPANT CHAIN YIELDS

FISSILE NUCLEUS: 92-U -235, NEUTRON ENERGY:HIGH.									
MASS NUMBER	NUMBER OF MEASUREMENTS	MAX.DCH12 CONTRIBUTING MEASUREMENTS	TOTAL CH12 PC.	PROBABILITY					
			ONE CH12 MEASUREMENT ONLY	ONE MEASUREMENT ONLY					
3	1	2065	4.1	6.0	1.3983 < 1.5%				
66	2	403							
67	1	349							
71	1								
72	3	13091	4.3	5.3					
74	1	403							
75									
76									
77	1	403							
78									
79									
80									
81									
82									
83	1	987							
84									
85									
86									
87									
88	1	943							
92	1	943							
93	1	349							
94									
97	5	280	4.6	8.6	7.1890				
98									
100									
101									
102									
103									
104									
105	3	162	5.7	9.8					
106	2	162	4.8	5.2	2.3085 < 1.5%				
107									
108									
110									
111	3	13091	3.5						
112	1	280							
113									
114									
116									
117									
118									
119									
120									
121									
122									
123									
124									
125									
126									
127									
128									
129									
130									
132	7	395	4.8	15.1	1.9148				
133	1	21708							
134	1	1111							
135									
136	1	1111							
137	2	162	2.5	3.8	4.9750				
138									
139	1	987							
142									
143	1	985							
144									
145									
146									
148	4	1183	5.4	9.9	1.9507				
149									
150									
151									
152									
153									
154									
155									
157									
158									
159	1	349							
160									
161	4	13091	2.6	8.4	3.8650				
162									
163									
164									
165									
166									
167	1	349							
168									
169	1	349							
170									

TABLE 49 LIST OF DISCREPANT CHAIN YIELDS (cont.)

FISSILE NUCLEUS: 92-U -235, NEUTRON ENERGY:HIGH.									
MASS NUMBER	NUMBER OF MEASUREMENTS	MAX.DCH12 CONTRIBUTING MEASUREMENTS	TOTAL CH12 PC.	PROBABILITY					
			ONE CH12 MEASUREMENT ONLY	ONE MEASUREMENT ONLY					
172	1	349							
173									
174									
175									
176									
177									
178									
179									
180									
181									
182									
183									
184									
185									
186									
187									
188									
189									
190									
191									
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232									
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255									
256									
257									
258									
259									
260									
261									
262									
263									
264									
265									
266									
267									
268									
269									
270									

TABLE 53 LIST OF DISCREPANT CHAIN YIELDS

FISSILE NUCLEUS: 94-PU-240 , NEUTRON ENERGY: HIGH.

[illegible]

FISSILE NUCLEUS: 94-PU-242 , NEUTRON ENERGY: HIGH.

[illegible]

TABLE 55 LIST OF DISCREPANT CHAIN YIELDS

FISSILE NUCLEUS: 95-AM-241, NEUTRON ENERGY: HIGH.

[illegible]

TABLE 55 LIST OF DISCREPANT CHAIN YIELDS

(CONT.)

FISSILE NUCLEUS: 95-AM-241, NEUTRON ENERGY:HIGH.

MASS NUMBER	NUMBER OF MEASUREMENTS	MAX.DCH12 CONTRIBUTING MEASUREMENT & DCH12 YIELD IN DATABASE	TOTAL YIELD IN DATABASE	PROBABILITY PC
161	1	1154	1154	ONE MEASUREMENT ONLY
162				YIELD IN DATABASE

TABLE 56 LIST OF DISCREPANT CHAIN YIELDS

FISSILE NUCLEUS: 90-TH-232, NEUTRON ENERGY:SPONTANEOUS

MASS NUMBER	NUMBER OF MEASUREMENTS	MAX.DCH12 CONTRIBUTING MEASUREMENT & DCH12 YIELD IN DATABASE	TOTAL YIELD IN DATABASE	PROBABILITY PC
72				YIELD IN DATABASE
73				YIELD IN DATABASE
74				YIELD IN DATABASE
75				YIELD IN DATABASE
76				YIELD IN DATABASE
77				YIELD IN DATABASE
78				YIELD IN DATABASE
79				YIELD IN DATABASE
80				YIELD IN DATABASE
81				YIELD IN DATABASE
82				YIELD IN DATABASE
83	1	326	326	ONE MEASUREMENT ONLY
84	1	326	326	ONE MEASUREMENT ONLY
85				YIELD IN DATABASE
86	1	326	326	ONE MEASUREMENT ONLY
87				YIELD IN DATABASE
88				YIELD IN DATABASE
89				YIELD IN DATABASE
90				YIELD IN DATABASE
91				YIELD IN DATABASE
92				YIELD IN DATABASE
93				YIELD IN DATABASE
94				YIELD IN DATABASE
95				YIELD IN DATABASE
96				YIELD IN DATABASE
97				YIELD IN DATABASE
98				YIELD IN DATABASE
99				YIELD IN DATABASE
100				YIELD IN DATABASE
101				YIELD IN DATABASE
102				YIELD IN DATABASE
103				YIELD IN DATABASE
104				YIELD IN DATABASE
105				YIELD IN DATABASE
106				YIELD IN DATABASE
107				YIELD IN DATABASE
108				YIELD IN DATABASE
109				YIELD IN DATABASE
110				YIELD IN DATABASE
111				YIELD IN DATABASE
112				YIELD IN DATABASE
113				YIELD IN DATABASE
114				YIELD IN DATABASE
115				YIELD IN DATABASE
116				YIELD IN DATABASE
117				YIELD IN DATABASE
118				YIELD IN DATABASE
119				YIELD IN DATABASE
120				YIELD IN DATABASE
121				YIELD IN DATABASE
122				YIELD IN DATABASE
123				YIELD IN DATABASE
124				YIELD IN DATABASE
125				YIELD IN DATABASE
126				YIELD IN DATABASE
127				YIELD IN DATABASE
128				YIELD IN DATABASE
129				YIELD IN DATABASE
130				YIELD IN DATABASE
131				YIELD IN DATABASE
132				YIELD IN DATABASE
133				YIELD IN DATABASE
134				YIELD IN DATABASE
135				YIELD IN DATABASE
136				YIELD IN DATABASE
137				YIELD IN DATABASE
138				YIELD IN DATABASE
139				YIELD IN DATABASE
140				YIELD IN DATABASE
141				YIELD IN DATABASE
142				YIELD IN DATABASE
143				YIELD IN DATABASE
144				YIELD IN DATABASE
145				YIELD IN DATABASE
146				YIELD IN DATABASE
147				YIELD IN DATABASE
148				YIELD IN DATABASE
149				YIELD IN DATABASE
150				YIELD IN DATABASE
151				YIELD IN DATABASE
152				YIELD IN DATABASE
153				YIELD IN DATABASE
154				YIELD IN DATABASE
155				YIELD IN DATABASE
156				YIELD IN DATABASE
157				YIELD IN DATABASE

TABLE 57 LIST OF DISCREPANT CHAIN YIELDS

FISSILE NUCLEUS: 92-U -238, NEUTRON ENERGY:SPONTANEOUS

MASS NUMBER	NUMBER OF MEASUREMENTS	MAX.DCH12 CONTRIBUTING MEASUREMENT & DCH12 YIELD IN DATABASE	TOTAL YIELD IN DATABASE	PROBABILITY PC
72				YIELD IN DATABASE
73				YIELD IN DATABASE
74				YIELD IN DATABASE
75				YIELD IN DATABASE
76				YIELD IN DATABASE
77				YIELD IN DATABASE
78				YIELD IN DATABASE
79				YIELD IN DATABASE
80				YIELD IN DATABASE
81				YIELD IN DATABASE
82				YIELD IN DATABASE
83				YIELD IN DATABASE
84				YIELD IN DATABASE
85				YIELD IN DATABASE
86				YIELD IN DATABASE
87				YIELD IN DATABASE
88				YIELD IN DATABASE
89				YIELD IN DATABASE
90				YIELD IN DATABASE
91	1	616	616	ONE MEASUREMENT ONLY
92	1	589	589	ONE MEASUREMENT ONLY
93	1	616	616	ONE MEASUREMENT ONLY
94				YIELD IN DATABASE
95				YIELD IN DATABASE
96				YIELD IN DATABASE
97				YIELD IN DATABASE
98				YIELD IN DATABASE
99				YIELD IN DATABASE
100				YIELD IN DATABASE
101				YIELD IN DATABASE
102				YIELD IN DATABASE
103				YIELD IN DATABASE
104	1	588	588	ONE MEASUREMENT ONLY
105	1	229	229	ONE MEASUREMENT ONLY
106	1	588	588	ONE MEASUREMENT ONLY
107				YIELD IN DATABASE
108				YIELD IN DATABASE
109				YIELD IN DATABASE
110				YIELD IN DATABASE
111				YIELD IN DATABASE
112				YIELD IN DATABASE
113				YIELD IN DATABASE
114				YIELD IN DATABASE
115				YIELD IN DATABASE
116				YIELD IN DATABASE
117				YIELD IN DATABASE
118				YIELD IN DATABASE
119				YIELD IN DATABASE
120				YIELD IN DATABASE
121				YIELD IN DATABASE
122				YIELD IN DATABASE
123				YIELD IN DATABASE
124				YIELD IN DATABASE
125				YIELD IN DATABASE
126				YIELD IN DATABASE
127				YIELD IN DATABASE
128				YIELD IN DATABASE
129				YIELD IN DATABASE
130				YIELD IN DATABASE
131				YIELD IN DATABASE
132				YIELD IN DATABASE
133				YIELD IN DATABASE
134				YIELD IN DATABASE
135				YIELD IN DATABASE
136				YIELD IN DATABASE
137				YIELD IN DATABASE
138				YIELD IN DATABASE
139				YIELD IN DATABASE
140				YIELD IN DATABASE
141				YIELD IN DATABASE
142				YIELD IN DATABASE
143				YIELD IN DATABASE
144				YIELD IN DATABASE
145				YIELD IN DATABASE
146				YIELD IN DATABASE
147				YIELD IN DATABASE
148				YIELD IN DATABASE
149				YIELD IN DATABASE
150				YIELD IN DATABASE
151				YIELD IN DATABASE
152				YIELD IN DATABASE
153				YIELD IN DATABASE
154				YIELD IN DATABASE
155				YIELD IN DATABASE
156				YIELD IN DATABASE
157				YIELD IN DATABASE
158				YIELD IN DATABASE
159				YIELD IN DATABASE
160				YIELD IN DATABASE
161				YIELD IN DATABASE
162				YIELD IN DATABASE

TABLE 1 ENERGY-THERMAL NUCLEI-TH-229									
Mass Elem.	Ref.	Yield	Error	N-Res	Type	wt. mean	Chi/df Estimates of Error		

RB	22143	2.1000E-01	12.4	0.00	FractInd	2.1000E-01	0.00	12.4(I)	0.0(E) 12.4(A)
SR	22143	6.0000E-03	166.7	0.00	FractInd	6.0000E-03	0.00	166.7(I)	0.0(E)166.7(A)
91 BR	22143	2.2000E-02	54.5	0.00	FractInd	2.2000E-02	0.00	54.5(I)	0.0(E) 54.5(A)
KR	22143	4.2400E-01	3.8	0.00	FractInd	4.2400E-01	0.00	3.8(I)	0.0(E) 3.8(A)
RB	22143	4.5600E-01	5.0	0.00	FractInd	4.5600E-01	0.00	5.0(I)	0.0(E) 5.0(A)
SR	22143	9.7000E-02	11.3	0.00	FractInd	9.7000E-02	0.00	11.3(I)	0.0(E) 11.3(A)
92 KR	22143	1.9500E-01	6.2	0.00	FractInd	1.9500E-01	0.00	6.2(I)	0.0(E) 6.2(A)
RB	22143	3.7300E-01	6.7	0.00	FractInd	3.7300E-01	0.00	6.7(I)	0.0(E) 6.7(A)
SR	22143	4.3100E-01	5.3	0.00	FractInd	4.3100E-01	0.00	5.3(I)	0.0(E) 5.3(A)
93 KR	22143	3.7000E-02	116.2	0.00	FractInd	3.7000E-02	0.00	116.2(I)	0.0(E)116.2(A)
RB	22143	2.5100E-01	7.2	0.00	FractInd	2.5100E-01	0.00	7.2(I)	0.0(E) 7.2(A)
SR	22143	6.6500E-01	4.2	0.00	FractInd	6.6500E-01	0.00	4.2(I)	0.0(E) 4.2(A)
Y	22143	4.7000E-02	48.9	0.00	FractInd	4.7000E-02	0.00	48.9(I)	0.0(E) 48.9(A)
94 KR	22143	1.3000E-02	76.9	0.00	FractInd	1.3000E-02	0.00	76.9(I)	0.0(E) 76.9(A)
RB	22143	8.5000E-02	16.5	0.00	FractInd	8.5000E-02	0.00	16.5(I)	0.0(E) 16.5(A)
SR	22143	7.7700E-01	4.2	0.00	FractInd	7.7700E-01	0.00	4.2(I)	0.0(E) 4.2(A)
Y	22143	1.2500E-01	42.4	0.00	FractInd	1.2500E-01	0.00	42.4(I)	0.0(E) 42.4(A)
95 RB	22143	2.9000E-02	62.1	0.00	FractInd	2.9000E-02	0.00	62.1(I)	0.0(E) 62.1(A)
SR	22143	6.0100E-01	5.7	0.00	FractInd	6.0100E-01	0.00	5.7(I)	0.0(E) 5.7(A)
Y	22143	3.3800E-01	10.7	0.00	FractInd	3.3800E-01	0.00	10.7(I)	0.0(E) 10.7(A)
ZR	22143	3.2000E-02	59.4	0.00	FractInd	3.2000E-02	0.00	59.4(I)	0.0(E) 59.4(A)
96 RB	22143	1.1000E-02	90.9	0.00	FractInd	1.1000E-02	0.00	90.9(I)	0.0(E) 90.9(A)
SR	22143	4.4700E-01	5.1	0.00	FractInd	4.4700E-01	0.00	5.1(I)	0.0(E) 5.1(A)
Y	22143	3.9800E-01	5.3	0.00	FractInd	3.9800E-01	0.00	5.3(I)	0.0(E) 5.3(A)
ZR	22143	1.4400E-01	11.8	0.00	FractInd	1.4400E-01	0.00	11.8(I)	0.0(E) 11.8(A)
97 SR	22143	1.6000E-01	8.8	0.00	FractInd	1.6000E-01	0.00	8.8(I)	0.0(E) 8.8(A)
Y	22143	4.3100E-01	7.4	0.00	FractInd	4.3100E-01	0.00	7.4(I)	0.0(E) 7.4(A)
ZR	22143	3.3500E-01	7.5	0.00	FractInd	3.3500E-01	0.00	7.5(I)	0.0(E) 7.5(A)
136 CS	300	1.4400E-02	57.0	0.00	Ind/Y(A)	1.4400E-02	0.00	57.0(I)	0.0(E) 57.0(A)

TABLE 1 ENERGY-THERMAL NUCLEI-TH-229									
Mass Elem.	Ref.	Yield	Error	N-Res	Type	wt. mean	Chi/df Estimates of Error		

78 GA	22143	2.7100E-01	20.7	0.00	FractInd	2.7100E-01	0.00	20.7(I)	0.0(E) 20.7(A)

GE	22143	7.2900E-01	12.3	0.00	FractInd	7.2900E-01	0.00	12.3(I)	0.0(E) 12.3(A)
79 GA	22143	1.7600E-01	22.2	0.00	FractInd	1.7600E-01	0.00	22.2(I)	0.0(E) 22.2(A)

GE	22143	7.8600E-01	10.9	0.00	FractInd	7.8600E-01	0.00	10.9(I)	0.0(E) 10.9(A)
AS	22143	3.7000E-02	32.4	0.00	FractInd	3.7000E-02	0.00	32.4(I)	0.0(E) 32.4(A)
80 GA	22143	2.1000E-02	47.6	0.00	FractInd	2.1000E-02	0.00	47.6(I)	0.0(E) 47.6(A)

GE	22143	9.4800E-01	3.9	0.00	FractInd	9.4800E-01	0.00	3.9(I)	0.0(E) 3.9(A)
AS	22143	3.1000E-02	51.6	0.00	FractInd	3.1000E-02	0.00	51.6(I)	0.0(E) 51.6(A)
81 GA	22143	1.2000E-02	83.3	0.00	FractInd	1.2000E-02	0.00	83.3(I)	0.0(E) 83.3(A)

GE	22143	7.1400E-01	3.6	0.00	FractInd	7.1400E-01	0.00	3.6(I)	0.0(E) 3.6(A)
AS	22143	2.4800E-01	6.9	0.00	FractInd	2.4800E-01	0.00	6.9(I)	0.0(E) 6.9(A)
SE	22143	2.6000E-02	42.3	0.00	FractInd	2.6000E-02	0.00	42.3(I)	0.0(E) 42.3(A)
82 GE	22143	3.3600E-01	4.8	0.00	FractInd	3.3600E-01	0.00	4.8(I)	0.0(E) 4.8(A)

AS	22143	4.0000E-01	5.0	0.00	FractInd	4.0000E-01	0.00	5.0(I)	0.0(E) 5.0(A)
SE	22143	2.3800E-01	7.1	0.00	FractInd	2.3800E-01	0.00	7.1(I)	0.0(E) 7.1(A)
BR	22143	2.5000E-02	40.0	0.00	FractInd	2.5000E-02	0.00	40.0(I)	0.0(E) 40.0(A)
83 GE	22143	3.0000E-02	33.3	0.00	FractInd	3.0000E-02	0.00	33.3(I)	0.0(E) 33.3(A)

AS	22143	3.2600E-01	4.9	0.00	FractInd	3.2600E-01	0.00	4.9(I)	0.0(E) 4.9(A)
SE	22143	6.2600E-01	3.4	0.00	FractInd	6.2600E-01	0.00	3.4(I)	0.0(E) 3.4(A)
BR	22143	1.8000E-02	61.1	0.00	FractInd	1.8000E-02	0.00	61.1(I)	0.0(E) 61.1(A)
84 GE	22143	5.0000E-03	200.0	0.00	FractInd	5.0000E-03	0.00	200.0(I)	0.0(E)200.0(A)

AS	22143	7.7000E-02	13.0	0.00	FractInd	7.7000E-02	0.00	13.0(I)	0.0(E) 13.0(A)
SE	22143	8.8300E-01	2.2	0.00	FractInd	8.8300E-01	0.00	2.2(I)	0.0(E) 2.2(A)
BR	22143	3.6000E-02	30.6	0.00	FractInd	3.6000E-02	0.00	30.6(I)	0.0(E) 30.6(A)
85 AS	22143	3.0000E-02	43.3	0.00	FractInd	3.0000E-02	0.00	43.3(I)	0.0(E) 43.3(A)

SE	22143	7.8900E-01	2.2	0.00	FractInd	7.8900E-01	0.00	2.2(I)	0.0(E) 2.2(A)
BR	22143	1.8200E-01	10.4	0.00	FractInd	1.8200E-01	0.00	10.4(I)	0.0(E) 10.4(A)
86 AS	22143	6.0000E-03	166.7	0.00	FractInd	6.0000E-03	0.00	166.7(I)	0.0(E)166.7(A)

SE	22143	6.1500E-01	2.8	0.00	FractInd	6.1500E-01	0.00	2.8(I)	0.0(E) 2.8(A)
BR	22143	3.1000E-01	5.2	0.00	FractInd	3.1000E-01	0.00	5.2(I)	0.0(E) 5.2(A)
KR	22143	6.9000E-02	15.9	0.00	FractInd	6.9000E-02	0.00	15.9(I)	0.0(E) 15.9(A)
87 SE	22143	1.9400E-01	5.7	0.00	FractInd	1.9400E-01	0.00	5.7(I)	0.0(E) 5.7(A)

BR	22143	4.8000E-01	4.0	0.00	FractInd	4.8000E-01	0.00	4.0(I)	0.0(E) 4.0(A)
KR	22143	3.2600E-01	5.8	0.00	FractInd	3.2600E-01	0.00	5.8(I)	0.0(E) 5.8(A)
88 SE	22143	3.2000E-02	31.2	0.00	FractInd	3.2000E-02	0.00	31.2(I)	0.0(E) 31.2(A)

BR	22143	2.9200E-01	6.2	0.00	FractInd	2.9200E-01	0.00	6.2(I)	0.0(E) 6.2(A)
KR	22143	6.3300E-01	3.3	0.00	FractInd	6.3300E-01	0.00	3.3(I)	0.0(E) 3.3(A)
RB	22143	4.4000E-02	50.0	0.00	FractInd	4.4000E-02	0.00	50.0(I)	0.0(E) 50.0(A)
89 SE	22143	1.1000E-02	90.9	0.00	FractInd	1.1000E-02	0.00	90.9(I)	0.0(E) 90.9(A)

BR	22143	1.3400E-01	9.7	0.00	FractInd	1.3400E-01	0.00	9.7(I)	0.0(E) 9.7(A)
KR	22143	7.9600E-01	3.0	0.00	FractInd	7.9600E-01	0.00	3.0(I)	0.0(E) 3.0(A)
RB	22143	5.9000E-02	20.3	0.00	FractInd	5.9000E-02	0.00	20.3(I)	0.0(E) 20.3(A)
90 BR	22143	3.7000E-02	86.5	0.00	FractInd	3.7000E-02	0.00	86.5(I)	0.0(E) 86.5(A)

KR	22143	7.4700E-01	2.4	0.00	FractInd	7.4700E-01	0.00	2.4(I)	0.0(E) 2.4(A)

TABLE 2 ENERGY-THERMAL NUCLEI-U -233									
Mass Elem	Ref.	Yield	Error	N-Res	Type	wt. mean	Chi/df	Estimates of Error	
90 BR	10918 2.4700E-02	11.3	-2.13	FractInd	2.5721E-02	4.52	10.7(I)	22.7(E)	22.7(A)
91 BR	10918 2.9600E-01	13.5	0.00	FractInd	2.9600E-01	0.00	13.5(I)	0.0(E)	13.5(A)
AS	10918 5.4500E-01	7.9	0.00	FractInd	5.4500E-01	0.00	7.9(I)	0.0(E)	7.9(A)
SE	10918 7.6000E-02	34.2	0.00	FractInd	7.6000E-02	0.00	34.2(I)	0.0(E)	34.2(A)
82 GA	10918 4.5900E-02	23.1	0.00	FractInd	4.5900E-02	0.00	23.1(I)	0.0(E)	23.1(A)
GE	10918 1.4400E-01	9.2	0.00	FractInd	1.4400E-01	0.00	9.2(I)	0.0(E)	9.2(A)
AS	10918 5.3000E-01	5.0	0.00	FractInd	5.3000E-01	0.00	5.0(I)	0.0(E)	5.0(A)
SE	10918 2.8100E-01	5.3	0.00	FractInd	2.8100E-01	0.00	5.3(I)	0.0(E)	5.3(A)
BR(G)	416 2.0400E-03	13.9	2.59	Ind/Y(A)	1.3402E-03	6.70	6.4(I)	16.5(E)	16.5(A)
305 1.2700E-03	7.1	-2.59	Ind/Y(A)						
83 GE	10918 4.7500E-02	13.7	0.00	FractInd	4.7500E-02	0.00	13.7(I)	0.0(E)	13.7(A)
AS	10918 3.4900E-01	5.0	0.00	FractInd	3.4900E-01	0.00	5.0(I)	0.0(E)	5.0(A)
SE	10918 5.8900E-01	5.0	0.00	FractInd	5.8900E-01	0.00	5.0(I)	0.0(E)	5.0(A)
BR	10918 1.4000E-02	43.6	0.00	FractInd	1.4000E-02	0.00	43.6(I)	0.0(E)	43.6(A)
84 GE	10918 1.2700E-02	36.2	0.00	FractInd	1.2700E-02	0.00	36.2(I)	0.0(E)	36.2(A)
AS	10918 1.0300E-01	8.2	0.00	FractInd	1.0300E-01	0.00	8.2(I)	0.0(E)	8.2(A)
SE	10918 7.5500E-01	5.0	0.00	FractInd	7.5500E-01	0.00	5.0(I)	0.0(E)	5.0(A)
BR	10918 1.2900E-01	5.6	0.00	FractInd	1.2900E-01	0.00	5.6(I)	0.0(E)	5.6(A)
RB(G)	895 3.9200E-08	10.2	0.00	Ind/Y(A)	3.9200E-08	0.00	10.2(I)	0.0(E)	10.2(A)
85 AS	10918 4.9000E-02	10.2	0.00	FractInd	4.9000E-02	0.00	10.2(I)	0.0(E)	10.2(A)
SE	10918 5.2000E-01	5.0	0.00	FractInd	5.2000E-01	0.00	5.0(I)	0.0(E)	5.0(A)
BR	10918 3.7700E-01	5.0	0.00	FractInd	3.7700E-01	0.00	5.0(I)	0.0(E)	5.0(A)
KR	10918 5.3600E-02	17.9	0.00	FractInd	5.3600E-02	0.00	17.9(I)	0.0(E)	17.9(A)
86 AS	10918 1.7700E-02	18.1	0.00	FractInd	1.7700E-02	0.00	18.1(I)	0.0(E)	18.1(A)
SE	10918 2.8800E-01	2.6	0.00	FractInd	2.8800E-01	0.00	2.6(I)	0.0(E)	2.6(A)
BR	10918 4.9300E-01	1.6	0.00	FractInd	4.9300E-01	0.00	1.6(I)	0.0(E)	1.6(A)
KR	10918 2.0200E-01	3.1	0.00	FractInd	2.0200E-01	0.00	3.1(I)	0.0(E)	3.1(A)
RB(G)	865 3.0200E-04	10.0	0.00	Ind/Y(A)	3.0200E-04	0.00	10.0(I)	0.0(E)	10.0(A)
87 SE	10918 9.1700E-02	6.4	0.00	FractInd	9.1700E-02	0.00	6.4(I)	0.0(E)	6.4(A)
BR	10918 4.3600E-01	1.6	0.61	FractInd	4.3479E-01	3.15	1.6(I)	2.8(E)	2.8(A)
919 4.4200E-01	6.0	0.28	FractInd						
810 2.5100E-01	5.2w	-2.50	Ind/Y(A)						
KR	10918 4.5500E-01	1.6	-0.69	FractInd	4.5641E-01	0.48	1.5(I)	1.0(E)	1.5(A)
919 4.7200E-01	5.0	0.69	FractInd						
RB	10918 1.7800E-02	19.1	0.00	FractInd	1.7800E-02	0.00	19.1(I)	0.0(E)	19.1(A)
88 SE	10918 2.2800E-02	11.8	0.00	FractInd	2.2800E-02	0.00	11.8(I)	0.0(E)	11.8(A)
BR	10918 2.1500E-01	2.8	-0.87	FractInd	2.1666E-01	0.76	2.7(I)	2.3(E)	2.7(A)
919 2.3200E-01	8.0	0.87	FractInd						
KR	10918 7.0400E-01	1.0	-0.19	FractInd	7.0426E-01	0.04	1.0(I)	0.2(E)	1.0(A)
919 1.1100E-01	5.0	0.19	FractInd						
RB	10918 5.7900E-02	6.9	0.00	FractInd	5.7900E-02	0.00	6.9(I)	0.0(E)	6.9(A)
89 BR	919 1.1600E-01	20.0	0.27	FractInd	1.1025E-01	3.61	8.9(I)	16.9(E)	16.9(A)
1807 2.1200E-01	20.0	2.47	FractInd						
810 1.7000E-01	20.1	1.83	FractInd						
KR	10918 7.3800E-01	5.0	-0.85	FractInd	7.5961E-01	0.73	3.5(I)	3.0(E)	3.5(A)
919 7.8400E-01	5.0	0.85	FractInd						
RB	10918 1.5300E-01	5.0	0.00	FractInd	1.5300E-01	0.00	5.0(I)	0.0(E)	5.0(A)
SR	10918 1.5600E-02	14.1	0.00	FractInd	1.5600E-02	0.00	14.1(I)	0.0(E)	14.1(A)

TABLE 2 ENERGY-THERMAL NUCLEIDS-U -233

Mass Elem	Ref.	Yield	Error	N Res	Type	wt. mean	Chi/df	Estimates of Error
SB(M)	930	6.3600E-02	20.2	0.00	Ind/Y(A)	6.3600E-02	0.00	20.2(I) 0.0(E) 20.2(A)
TE	682	5.4400E-01	7.0	-2.41	FractInd	7.2564E-01	5.78	4.1(I) 9.8(E) 9.8(A)
	22016	7.4800E-01	5.0	2.41	FractInd			
I (G)	408	6.0000E-02	50.0	1.23	FractInd	2.3294E-02	1.50	9.3(I) 11.4(E) 11.4(A)
	20848	2.3100E-02	9.4	-1.23	Ind/Y(A)			
I (M)	20641	1.1500E-02	30.8	-1.45	Ind/Y(A)	1.6385E-02	2.10	8.3(I) 12.0(E) 12.0(A)
	20848	1.7200E-02	8.6	1.45	Ind/Y(A)			
I (T)	20848	3.9900E-02	6.8	0.00	Ind/Y(A)	3.9900E-02	0.00	6.8(I) 0.0(E) 6.8(A)
133 SB	22016	1.7900E-01	6.7	0.00	FractInd	1.7900E-01	0.00	6.7(I) 0.0(E) 6.7(A)
TE(G)	780	2.1000E-01	10.0	1.56	FractInd	2.3014E-01	2.42	7.2(I) 11.2(E) 11.2(A)
	930	2.6300E-01	10.2	1.56	Ind/Y(A)			
TE(M)	780	5.5000E-01	5.0	5.16	FractInd	4.5164E-01	26.66	4.4(I) 22.7(E) 22.7(A)
	930	3.4500E-01	8.3	-5.16	Ind/Y(A)			
TE(T)	22016	8.2100E-01	5.6	0.00	FractInd	8.2100E-01	0.00	5.6(I) 0.0(E) 5.6(A)
I (G)	566	1.3700E-01	10.0	-0.29	FractInd	1.4057E-01	3.83	4.5(I) 8.8(E) 8.8(A)
	780	1.5500E-01	7.0	1.64	FractInd			
	408	2.1000E-01	13.0w	2.50	FractInd			
	20848	1.2100E-01	7.3w	-2.46	Ind/Y(A)			
XE(G)	864	1.6000E-03	50.0	-1.33	FractInd	2.6429E-03	1.78	6.3(I) 8.4(E) 8.4(A)
	12895	2.6900E-03	6.3	1.33	FractInd			
XE(M)	12895	6.4800E-03	10.6	0.00	FractInd	6.4800E-03	0.00	10.6(I) 0.0(E) 10.6(A)
XE(T)	12895	9.2000E-03	7.9	0.00	FractInd	9.2000E-03	0.00	7.9(I) 0.0(E) 7.9(A)
134 TE	22016	3.9800E-01	5.0	0.00	FractInd	3.9800E-01	0.00	5.0(I) 0.0(E) 5.0(A)
I (G)	20848	1.6400E-01	6.5	0.00	Ind/Y(A)	1.6400E-01	0.00	6.5(I) 0.0(E) 6.5(A)
I (M)	20848	1.2400E-01	5.9	-0.71	Ind/Y(A)	1.2604E-01	0.50	5.3(I) 3.8(E) 5.3(A)
	20841	1.3700E-01	12.3	0.71	Ind/Y(A)			
I (T)	22016	2.3180E-01	9.2w	-2.50	FractInd	2.7563E-01	5.26	4.6(I) 10.5(E) 10.5(A)
	566	3.9820E-01	6.0w	2.50	FractInd			
	20848	2.8800E-01	5.7	1.19	Ind/Y(A)			
XE(G)	408	3.7000E-01	16.0	0.00	FractInd	3.7000E-01	0.00	16.0(I) 0.0(E) 16.0(A)
135 I	566	6.0600E-01	15.0	0.00	FractInd	6.0600E-01	0.00	15.0(I) 0.0(E) 15.0(A)
XE	604	2.7900E-01	5.0	0.00	FractInd	2.7900E-01	0.00	5.0(I) 0.0(E) 5.0(A)
XE(G)	807	7000E-01	12.0	2.46	FractInd	1.2341E-01	4.70	6.2(I) 13.4(E) 13.4(A)
	265	1.4200E-01	10.0w	-3.31	FractInd			
	12895	9.9400E-02	9.3w	-2.50	FractInd			
	20848	1.1800E-01	10.4	-0.56	Ind/Y(A)			
XE(M)	12895	1.2800E-01	13.3	-2.79	FractInd	1.6494E-01	7.77	6.5(I) 18.1(E) 18.1(A)
	20848	1.6900E-01	7.3	2.79	Ind/Y(A)			
XE(T)	777	1.7000E-01	12.0	-0.24	FractInd	1.7340E-01	4.74	8.5(I) 18.5(E) 18.5(A)
	12895	2.3200E-01	12.0	2.48	FractInd			
	864	9.9000E-02	14.0w	-2.50	FractInd			
136 TE	22016	4.4050E-02	5.7	0.00	FractInd	4.4050E-02	0.00	5.7(I) 0.0(E) 5.7(A)
I	22016	5.0200E-01	5.0	0.00	FractInd	5.0200E-01	0.00	5.0(I) 0.0(E) 5.0(A)
CS	42	1.4600E-02	22.1	0.41	Ind/Y(A)	1.3351E-02	0.73	7.2(I) 6.2(E) 7.2(A)
	885	1.4900E-02	13.7	0.86	Ind/Y(A)			
	215	1.5300E-02	17.6	0.77	Ind/Y(A)			
	305	1.2100E-02	0.16	-	Ind/Y(A)			
137 TE	22016	1.3000E-02	50.0	0.00	FractInd	1.3000E-02	0.00	50.0(I) 0.0(E) 50.0(A)
I	22016	1.5500E-01	23.9	-1.79	FractInd	2.1581E-01	3.19	6.8(I) 12.1(E) 12.1(A)
	919	2.2700E-01	7.0	1.79	FractInd			
XE	919	6.5300E-01	5.0	-3.35	FractInd	7.1973E-01	11.21	3.6(I) 12.0(E) 12.0(A)
	22016	8.3200E-01	5.1	3.35	FractInd			
138 I	919	1.1600E-01	20.0	0.00	FractInd	1.1600E-01	0.00	20.0(I) 0.0(E) 20.0(A)
CS(G)	20848	5.8100E-02	9.5	0.00	Ind/Y(A)	5.8100E-02	0.00	9.5(I) 0.0(E) 9.5(A)
CS(M)	20848	1.4200E-01	8.7	0.00	Ind/Y(A)	1.4200E-01	0.00	8.7(I) 0.0(E) 8.7(A)

TABLE 2 ENERGY-THERMAL NUCLEIDS-U -233

Mass Elem	Ref.	Yield	Error	N Res	Type	wt. mean	Chi/df	Estimates of Error
ZR	10918	6.5800E-01	5.0	0.00	FractInd	6.5800E-01	0.00	5.0(I) 0.0(E) 5.0(A)
NB	10918	4.4100E-02	10.4	6.97	FractInd	1.7404E-02	48.53	14.4(I)100.6(E)100.6(A)
	21218	6.0000E-03	50.0	-6.97	FractInd			
99 SR	10918	1.3400E-02	16.4	0.00	FractInd	1.3400E-02	0.00	16.4(I) 0.0(E) 16.4(A)
Y	22016	1.3400E-01	5.0	-6.83	FractInd	1.5496E-01	46.69	3.8(I) 26.3(E) 26.3(A)
	22016	2.3400E-01	5.6	6.83	FractInd			
ZR	10918	7.1100E-01	5.0	-0.70	FractInd	7.2811E-01	0.49	3.5(I) 2.5(E) 3.5(A)
	22016	7.4700E-01	5.0	0.70	FractInd			
NB	10918	1.4100E-01	5.0	16.39	FractInd	3.1613E-02	268.50	7.2(I)117.5(E)117.5(A)
	22016	1.9000E-02	12.6	-16.39	FractInd			
100 Y	10918	3.6600E-02	11.2	0.00	FractInd	3.6600E-02	0.00	11.2(I) 0.0(E) 11.2(A)
ZR	10918	7.1500E-01	5.0	0.00	FractInd	7.1500E-01	0.00	5.0(I) 0.0(E) 5.0(A)
NB	10918	1.9800E-01	5.0	0.00	FractInd	1.9800E-01	0.00	5.0(I) 0.0(E) 5.0(A)
MO	10918	4.9800E-02	10.4	0.00	FractInd	4.9800E-02	0.00	10.4(I) 0.0(E) 10.4(A)
101 Y	10918	2.3900E-02	15.1	0.00	FractInd	2.3900E-02	0.00	15.1(I) 0.0(E) 15.1(A)
ZR	10918	4.4400E-01	5.0	0.00	FractInd	4.4400E-01	0.00	5.0(I) 0.0(E) 5.0(A)
NB	10918	4.5500E-01	5.0	0.00	FractInd	4.5500E-01	0.00	5.0(I) 0.0(E) 5.0(A)
MO	10918	7.7200E-02	8.2	0.00	FractInd	7.7200E-02	0.00	8.2(I) 0.0(E) 8.2(A)
102 ZR	10918	2.7000E-01	3.1	0.00	FractInd	2.7000E-01	0.00	3.1(I) 0.0(E) 3.1(A)
NB	10918	4.1500E-01	2.5	0.00	FractInd	4.1500E-01	0.00	2.5(I) 0.0(E) 2.5(A)
MO	10918	2.8500E-01	3.6	0.00	FractInd	2.8500E-01	0.00	3.6(I) 0.0(E) 3.6(A)
TC	10918	2.9800E-02	24.2	0.00	FractInd	2.9800E-02	0.00	24.2(I) 0.0(E) 24.2(A)
103 ZR	10918	1.0100E-01	7.8	0.00	FractInd	1.0100E-01	0.00	7.8(I) 0.0(E) 7.8(A)
NB	10918	3.6200E-01	3.3	0.00	FractInd	3.6200E-01	0.00	3.3(I) 0.0(E) 3.3(A)
MO	10918	5.0800E-01	2.5	0.00	FractInd	5.0800E-01	0.00	2.5(I) 0.0(E) 2.5(A)
TC	10918	2.0400E-02	27.6	0.00	FractInd	2.0400E-02	0.00	27.6(I) 0.0(E) 27.6(A)
104 ZR	10918	7.1100E-02	11.7	0.00	FractInd	7.1100E-02	0.00	11.7(I) 0.0(E) 11.7(A)
NB	10918	1.7900E-01	7.8	0.00	FractInd	1.7900E-01	0.00	7.8(I) 0.0(E) 7.8(A)
MO	10918	7.0400E-01	2.3	0.00	FractInd	7.0400E-01	0.00	2.3(I) 0.0(E) 2.3(A)
TC	10918	4.5900E-02	20.9	0.00	FractInd	4.5900E-02	0.00	20.9(I) 0.0(E) 20.9(A)
105 NB	10918	1.4800E-01	11.6	0.00	FractInd	1.4800E-01	0.00	11.6(I) 0.0(E) 11.6(A)
MO	10918	7.2300E-01	4.3	0.00	FractInd	7.2300E-01	0.00	4.3(I) 0.0(E) 4.3(A)
TC	10918	9.9800E-02	27.7	0.00	FractInd	9.9800E-02	0.00	27.7(I) 0.0(E) 27.7(A)
RU	10918	2.9200E-02	76.4	0.00	FractInd	2.9200E-02	0.00	76.4(I) 0.0(E) 76.4(A)
112 AG	336	2.0000E-04	15.0	-0.30	FractInd	2.7505E-04	0.09	13.4(I) 4.1(E) 13.4(A)
	930	1.4200E-01	10.3	0.28	Ind/Y(A)			
130 SN	22016	5.3320E-01	5.0	0.00	FractInd	5.3320E-01	0.00	5.0(I) 0.0(E) 5.0(A)
SB(T)	22016	7.7640E-01	5.0	0.00	FractInd	7.7640E-01	0.00	5.0(I) 0.0(E) 5.0(A)
131 TE(G)	930	1.4200E-01	10.3	0.28	Ind/Y(A)	1.3960E-01	0.08	8.5(I) 2.4(E) 8.5(A)
TE(M)	780	3.3400E-01	6.0	2.53	FractInd	2.9571E-01	6.39	4.4(I) 11.2(E) 11.2(A)
	930	2.6700E-01	6.5	-2.53	Ind/Y(A)			
I	780	1.4000E-02	22.2	2.73	FractInd	6.1179E-03	7.43	17.3(I) 47.2(E) 47.2(A)
	20848	5.0600E-03	22.3	-2.73	FractInd			
132 SN	22016	1.3000E-02	15.4	-2.23	FractInd	1.4658E-02	4.96	12.7(I) 28.3(E) 28.3(A)
	682	2.5000E-02	20.0	2.23	FractInd			
SB(G)	22016	2.7100E-01	10.0	-2.48	FractInd	2.1021E-01	3.28	5.5(I) 10.0(E) 10.0(A)
	930	1.7400E-01	18.2	-1.06	Ind/Y(A)			

TABLE 3		ENERGY-THERMAL		NUCLIDE-U -235		wt. mean	Chi/df	Estimates of Error
Mass Elem.	Ref.	Yield	Error	N.Res Type				
=====								
	21939	2.000E-01	5.0	0.39	FractInd			
PM	21532	1.5100E-10	100.0	0.00	Ind/Y(A)	1.5100E-10	0.00	100.0(I) 0.0(E)100.0(A)
147	LA	21939	4.1000E-01	2.4	0.00	FractInd	4.1000E-01	0.00 2.4(I) 0.0(E) 2.4(A)
CE	21939	4.1000E-01	19.5	0.00	FractInd	4.1000E-01	0.00	19.5(I) 0.0(E) 19.5(A)
PR	21939	1.8000E-01	44.4	0.00	FractInd	1.8000E-01	0.00	44.4(I) 0.0(E) 44.4(A)
148	PM(G)	554	5.000E-06	100.0	2.99	FractInd	8.6130E-06	8.96 56.3(I)168.6(E)168.6(A)
PM(M)	21532	1.6700E-09	25.0w	-2.36	Ind/Y(A)	4.1493E-09	5.16	7.3(I) 16.6(E) 16.6(A)
	21532	3.900E-09	9.0	-0.84	Ind/Y(A)			
	21532	5.6500E-09	9.5w	2.50	Ind/Y(A)			
150	PM	21552	4.6100E-05	33.3	-0.04	Ind/Y(A)	4.6497E-05	0.00 23.4(I) 0.9(E) 23.4(A)
	873	4.6900E-05	33.0	0.04	Ind/Y(A)			
160	TB	485	1.3000E-03	15.0	0.00	FractInd	1.3000E-03	0.00 15.0(I) 0.0(E) 15.0(A)

TABLE 4		ENERGY-THERMAL		NUCLIDES-NP-237		wt. mean	Chi/df	Estimates of Error
Mass Elem.	Ref.	Yield	Error	N Res	Type			
134	I	21651	3.2600E-01	22.7	-1.23	FractInd	3.5936E-01	1.51 19.2(I) 23.5(E) 23.5(A)
		10967	5.7400E-01	32.7	1.23	Ind/Y(A)		
135	XE	21651	1.0200E-01	17.6	0.00	FractInd	1.0200E-01	0.00 17.6(I) 0.0(E) 17.6(A)

TABLE 5		ENERGY-THERMAL		NUCLIDES-NP-238			
Mass Elem	Ref.	Yield	Error	N-Res Type	wt. mean	Chi/df	Estimates of Error
Y	2110	5.0100E-01	5.0	0.00	FractInd 5.0100E-01	0.00	5.0(I) 0.0(E) 5.0(A)
ZR	2110	3.1000E-01	5.0	0.00	FractInd 3.0000E-01	0.00	5.0(I) 0.0(E) 5.0(A)
NB	2110	3.9000E-02	5.0	0.00	FractInd 3.9000E-02	0.00	5.0(I) 0.0(E) 5.0(A)
99	SR	2110	3.4000E-02	5.0	0.00	FractInd 3.4000E-02	0.00 5.0(I) 0.0(E) 5.0(A)
Y	2110	4.4100E-01	5.0	0.00	FractInd 4.4100E-01	0.00	5.0(I) 0.0(E) 5.0(A)
ZR	2110	3.8900E-01	5.0	0.00	FractInd 3.8900E-01	0.00	5.0(I) 0.0(E) 5.0(A)
NB	2110	8.6000E-02	5.0	0.00	FractInd 8.6000E-02	0.00	5.0(I) 0.0(E) 5.0(A)
100	Y	2110	1.9100E-01	5.0	0.00	FractInd 1.9100E-01	0.00 5.0(I) 0.0(E) 5.0(A)
ZR	2110	6.9000E-01	5.0	0.00	FractInd 6.9000E-01	0.00	5.0(I) 0.0(E) 5.0(A)
NB	2110	1.1900E-01	5.0	0.00	FractInd 1.1900E-01	0.00	5.0(I) 0.0(E) 5.0(A)
101	Y	2110	8.1000E-02	5.0	0.00	FractInd 8.1000E-02	0.00 5.0(I) 0.0(E) 5.0(A)
ZR	2110	5.2400E-01	5.0	0.00	FractInd 5.2400E-01	0.00	5.0(I) 0.0(E) 5.0(A)
NB	2110	3.4700E-01	5.0	0.00	FractInd 3.4700E-01	0.00	5.0(I) 0.0(E) 5.0(A)
MO	2110	4.8000E-02	5.0	0.00	FractInd 4.8000E-02	0.00	5.0(I) 0.0(E) 5.0(A)
102	Y	2110	1.9000E-02	5.0	0.00	FractInd 1.9000E-02	0.00 5.0(I) 0.0(E) 5.0(A)
ZR	2110	4.4700E-01	5.0	0.00	FractInd 4.4700E-01	0.00	5.0(I) 0.0(E) 5.0(A)
NB	2110	4.6600E-01	5.0	0.00	FractInd 4.6600E-01	0.00	5.0(I) 0.0(E) 5.0(A)
MO	2110	8.8000E-02	5.0	0.00	FractInd 8.8000E-02	0.00	5.0(I) 0.0(E) 5.0(A)
103	ZR	2110	1.3300E-01	10.0	0.00	FractInd 1.3300E-01	0.00 10.0(I) 0.0(E) 10.0(A)
NB	2110	5.9900E-01	5.0	0.00	FractInd 5.9900E-01	0.00	5.0(I) 0.0(E) 5.0(A)
MO	2110	2.1000E-01	5.0	0.00	FractInd 2.1000E-01	0.00	5.0(I) 0.0(E) 5.0(A)
TC	2110	5.8000E-02	10.0	0.00	FractInd 5.8000E-02	0.00	10.0(I) 0.0(E) 10.0(A)
104	ZR	2110	5.4000E-02	10.0	0.00	FractInd 5.4000E-02	0.00 10.0(I) 0.0(E) 10.0(A)
NB	2110	4.0300E-01	5.0	0.00	FractInd 4.0300E-01	0.00	5.0(I) 0.0(E) 5.0(A)
MO	2110	4.7000E-01	5.0	0.00	FractInd 4.7000E-01	0.00	5.0(I) 0.0(E) 5.0(A)
TC	2110	7.3000E-02	10.0	0.00	FractInd 7.3000E-02	0.00	10.0(I) 0.0(E) 10.0(A)
105	ZR	2110	5.4000E-02	10.0	0.00	FractInd 5.4000E-02	0.00 10.0(I) 0.0(E) 10.0(A)
NB	2110	2.4700E-01	5.0	0.00	FractInd 2.4700E-01	0.00	5.0(I) 0.0(E) 5.0(A)
MO	2110	5.0600E-01	5.0	0.00	FractInd 5.0600E-01	0.00	5.0(I) 0.0(E) 5.0(A)
TC	2110	1.9300E-01	5.0	0.00	FractInd 1.9300E-01	0.00	5.0(I) 0.0(E) 5.0(A)
106	NB	2110	6.5000E-02	10.0	0.00	FractInd 6.5000E-02	0.00 10.0(I) 0.0(E) 10.0(A)
MO	2110	5.4500E-01	5.0	0.00	FractInd 5.4500E-01	0.00	5.0(I) 0.0(E) 5.0(A)
TC	2110	3.2700E-01	5.0	0.00	FractInd 3.2700E-01	0.00	5.0(I) 0.0(E) 5.0(A)
RU	2110	6.3000E-02	10.0	0.00	FractInd 6.3000E-02	0.00	10.0(I) 0.0(E) 10.0(A)

TABLE 5		ENERGY-THERMAL		NUCLIDES-NP-238			
Mass Elem	Ref.	Yield	Error	N-Res Type	wt. mean	Chi/df	Estimates of Error
86	AS	2110	5.4000E-02	5.0	0.00	FractInd 5.4000E-02	0.00 5.0(I) 0.0(E) 5.0(A)
SE	2110	7.6600E-01	5.0	0.00	FractInd 7.6600E-01	0.00	5.0(I) 0.0(E) 5.0(A)
BR	2110	1.8000E-01	5.0	0.00	FractInd 1.8000E-01	0.00	5.0(I) 0.0(E) 5.0(A)
87	AS	2110	4.2000E-02	5.0	0.00	FractInd 4.2000E-02	0.00 5.0(I) 0.0(E) 5.0(A)
SE	2110	2.9900E-01	5.0	0.00	FractInd 2.9900E-01	0.00	5.0(I) 0.0(E) 5.0(A)
BR	2110	5.4600E-01	5.0	0.00	FractInd 5.4600E-01	0.00	5.0(I) 0.0(E) 5.0(A)
KR	2110	1.1300E-01	5.0	0.00	FractInd 1.1300E-01	0.00	5.0(I) 0.0(E) 5.0(A)
88	SE	2110	1.2000E-01	5.0	0.00	FractInd 1.2000E-01	0.00 5.0(I) 0.0(E) 5.0(A)
BR	2110	5.3800E-01	5.0	0.00	FractInd 5.3800E-01	0.00	5.0(I) 0.0(E) 5.0(A)
KR	2110	3.0400E-01	5.0	0.00	FractInd 3.0400E-01	0.00	5.0(I) 0.0(E) 5.0(A)
RB	2110	3.8000E-02	5.0	0.00	FractInd 3.8000E-02	0.00	5.0(I) 0.0(E) 5.0(A)
89	SE	2110	2.9000E-02	5.0	0.00	FractInd 2.9000E-02	0.00 5.0(I) 0.0(E) 5.0(A)
BR	2110	3.7400E-01	5.0	0.00	FractInd 3.7400E-01	0.00	5.0(I) 0.0(E) 5.0(A)
KR	2110	5.3200E-01	5.0	0.00	FractInd 5.3200E-01	0.00	5.0(I) 0.0(E) 5.0(A)
RB	2110	6.5000E-02	5.0	0.00	FractInd 6.5000E-02	0.00	5.0(I) 0.0(E) 5.0(A)
90	BR	2110	8.4000E-02	5.0	0.00	FractInd 8.4000E-02	0.00 5.0(I) 0.0(E) 5.0(A)
KR	2110	7.4000E-01	5.0	0.00	FractInd 7.4000E-01	0.00	5.0(I) 0.0(E) 5.0(A)
RB	2110	1.7600E-01	5.0	0.00	FractInd 1.7600E-01	0.00	5.0(I) 0.0(E) 5.0(A)
91	BR	2110	4.1000E-02	5.0	0.00	FractInd 4.1000E-02	0.00 5.0(I) 0.0(E) 5.0(A)
KR	2110	4.7000E-01	5.0	0.00	FractInd 4.7000E-01	0.00	5.0(I) 0.0(E) 5.0(A)
RB	2110	4.3800E-01	5.0	0.00	FractInd 4.3800E-01	0.00	5.0(I) 0.0(E) 5.0(A)
SR	2110	5.2000E-02	5.0	0.00	FractInd 5.2000E-02	0.00	5.0(I) 0.0(E) 5.0(A)
92	KR	2110	2.6800E-01	5.0	0.00	FractInd 2.6800E-01	0.00 5.0(I) 0.0(E) 5.0(A)
RB	2110	6.2100E-01	5.0	0.00	FractInd 6.2100E-01	0.00	5.0(I) 0.0(E) 5.0(A)
SR	2110	1.1100E-01	5.0	0.00	FractInd 1.1100E-01	0.00	5.0(I) 0.0(E) 5.0(A)
93	KR	2110	7.4000E-02	5.0	0.00	FractInd 7.4000E-02	0.00 5.0(I) 0.0(E) 5.0(A)
RB	2110	6.6200E-01	5.0	0.00	FractInd 6.6200E-01	0.00	5.0(I) 0.0(E) 5.0(A)
SR	2110	2.6400E-01	5.0	0.00	FractInd 2.6400E-01	0.00	5.0(I) 0.0(E) 5.0(A)
94	KR	2110	2.6000E-02	5.0	0.00	FractInd 2.6000E-02	0.00 5.0(I) 0.0(E) 5.0(A)
RB	2110	3.8700E-01	5.0	0.00	FractInd 3.8700E-01	0.00	5.0(I) 0.0(E) 5.0(A)
SR	2110	5.2300E-01	5.0	0.00	FractInd 5.2300E-01	0.00	5.0(I) 0.0(E) 5.0(A)
Y	2110	6.4000E-02	5.0	0.00	FractInd 6.4000E-02	0.00	5.0(I) 0.0(E) 5.0(A)
95	RB	2110	1.8300E-01	5.0	0.00	FractInd 1.8300E-01	0.00 5.0(I) 0.0(E) 5.0(A)
SR	2110	6.2700E-01	5.0	0.00	FractInd 6.2700E-01	0.00	5.0(I) 0.0(E) 5.0(A)
Y	2110	1.9000E-01	5.0	0.00	FractInd 1.9000E-01	0.00	5.0(I) 0.0(E) 5.0(A)
96	RB	2110	4.3000E-02	5.0	0.00	FractInd 4.3000E-02	0.00 5.0(I) 0.0(E) 5.0(A)
SR	2110	5.5300E-01	5.0	0.00	FractInd 5.5300E-01	0.00	5.0(I) 0.0(E) 5.0(A)
Y	2110	3.4100E-01	5.0	0.00	FractInd 3.4100E-01	0.00	5.0(I) 0.0(E) 5.0(A)
ZR	2110	5.2950E-02	5.0	0.00	FractInd 5.2950E-02	0.00	5.0(I) 0.0(E) 5.0(A)
97	RB	2110	1.9000E-02	5.0	0.00	FractInd 1.9000E-02	0.00 5.0(I) 0.0(E) 5.0(A)
SR	2110	2.8500E-01	5.0	0.00	FractInd 2.8500E-01	0.00	5.0(I) 0.0(E) 5.0(A)
Y	2110	5.7800E-01	5.0	0.00	FractInd 5.7800E-01	0.00	5.0(I) 0.0(E) 5.0(A)
ZR	2110	1.1800E-01	5.0	0.00	FractInd 1.1800E-01	0.00	5.0(I) 0.0(E) 5.0(A)
98	SR	2110	1.6000E-01	5.0	0.00	FractInd 1.6000E-01	0.00 5.0(I) 0.0(E) 5.0(A)

TABLE 6 ENERGY-THERMAL NUCLEI DS-PU-238						
Mass Elem.	Ref.	Yield	Error	N Res Type	wt. mean	Chi/df Estimates of Error
133 TE(M)	22087	3.4600E-01	6.3	0.00 Ind/Y(A)	3.4600E-01	0.00 6.3(I) 0.0(E) 6.3(A)
134 I (G)	22087	4.2400E-01	6.8	0.00 Ind/Y(A)	4.2400E-01	0.00 6.8(I) 0.0(E) 6.8(A)
I (M)	22087	1.8000E-01	8.7	0.00 Ind/Y(A)	1.8000E-01	0.00 8.7(I) 0.0(E) 8.7(A)
135 XE(G)	22087	1.2300E-01	11.9	0.00 Ind/Y(A)	1.2300E-01	0.00 11.9(I) 0.0(E) 11.9(A)
XE(M)	22087	1.4600E-01	18.9	0.00 Ind/Y(A)	1.4600E-01	0.00 18.9(I) 0.0(E) 18.9(A)

TABLE 7 ENERGY-THERMAL NUCLEI DS-PU-239						
Mass Elem.	Ref.	Yield	Error	N Res Type	wt. mean	Chi/df Estimates of Error
84 RB(G)	887	8.4000E-08	10.8	0.00 Ind/Y(A)	8.4000E-08	0.00 10.8(I) 0.0(E) 10.8(A)
86 AS	21928	8.0000E-03	12.5	0.00 FractInd	8.0000E-03	0.00 12.5(I) 0.0(E) 12.5(A)
SE	21928	3.9100E-01	4.4	0.00 FractInd	3.9100E-01	0.00 4.4(I) 0.0(E) 4.4(A)
BR	21928	5.0400E-01	17.1	0.00 FractInd	5.0400E-01	0.00 17.1(I) 0.0(E) 17.1(A)
KR	21928	9.4000E-02	6.4	0.00 FractInd	9.4000E-02	0.00 6.4(I) 0.0(E) 6.4(A)
PI(G)	887	2.5100E-04	10.2	0.00 Ind/Y(A)	2.5100E-04	0.00 10.2(I) 0.0(E) 10.2(A)
RB(T)	21928	3.0000E-03	33.3	0.00 FractInd	3.0000E-03	0.00 33.3(I) 0.0(E) 33.3(A)
87 AS	21928	1.0000E-03	100.0	0.00 FractInd	1.0000E-03	0.00 100.0(I) 0.0(E) 100.0(A)
SE	21928	1.4000E-01	7.1	0.00 FractInd	1.4000E-01	0.00 7.1(I) 0.0(E) 7.1(A)
BR	21928	5.5900E-01	4.1	0.00 FractInd	5.5900E-01	0.00 4.1(I) 0.0(E) 4.1(A)
KR	21928	2.8500E-01	4.6	-1.13 FractInd	2.9191E-01	1.27 3.9(I) 4.4(E) 4.4(A)
	21549	3.1600E-01	7.7	1.13 Ind/Y(A)		
RB	21928	1.5000E-02	6.7	0.00 FractInd	1.5000E-02	0.00 6.7(I) 0.0(E) 6.7(A)
88 SE	21928	3.3000E-02	3.0	0.00 FractInd	3.3000E-02	0.00 3.0(I) 0.0(E) 3.0(A)
BR	21928	3.5400E-01	3.7	0.00 FractInd	3.5400E-01	0.00 3.7(I) 0.0(E) 3.7(A)
KR	21928	5.6800E-01	4.6	0.18 FractInd	5.6577E-01	0.03 4.1(I) 0.7(E) 4.1(A)
	21549	5.5800E-01	8.7	-0.18 Ind/Y(A)		
RB	21928	4.5000E-02	4.4	0.00 FractInd	4.5000E-02	0.00 4.4(I) 0.0(E) 4.4(A)
89 SE	21928	3.0000E-03	33.3	0.00 FractInd	3.0000E-03	0.00 33.3(I) 0.0(E) 33.3(A)
BR	21928	1.5300E-01	2.6	0.00 FractInd	1.5300E-01	0.00 2.6(I) 0.0(E) 2.6(A)
KR	21928	6.8300E-01	3.8	0.39 FractInd	6.7647E-01	0.15 3.0(I) 1.2(E) 3.0(A)
	21549	6.6700E-01	4.7	-0.39 Ind/Y(A)		
RB	21928	1.5100E-01	3.3	0.16 FractInd	1.5107E-01	0.02 3.3(I) 0.5(E) 3.3(A)
	910	1.6000E-01	36.0	0.16 Ind/Y(A)		
SR	21928	9.0000E-03	11.1	0.00 FractInd	9.0000E-03	0.00 11.1(I) 0.0(E) 11.1(A)
90 BR	21928	2.8000E-02	14.3	0.00 FractInd	2.8000E-02	0.00 14.3(I) 0.0(E) 14.3(A)
KR	21928	5.5500E-01	2.7	0.27 FractInd	5.5348E-01	0.07 2.5(I) 0.7(E) 2.5(A)
	21549	5.4400E-01	6.9	-0.27 Ind/Y(A)		
RB	21928	3.6900E-01	3.5	0.00 FractInd	3.6900E-01	0.00 3.5(I) 0.0(E) 3.5(A)
SR	21928	4.8000E-02	8.3	0.00 FractInd	4.8000E-02	0.00 8.3(I) 0.0(E) 8.3(A)
91 BR	21928	8.0000E-03	1.2	0.00 FractInd	8.0000E-03	0.00 1.2(I) 0.0(E) 1.2(A)
KR	21928	2.7900E-01	2.5	-0.18 FractInd	2.7978E-01	0.03 2.0(I) 0.3(E) 2.0(A)
	21549	2.8100E-01	3.1	0.18 Ind/Y(A)		
RB	21928	5.5600E-01	2.5	0.00 FractInd	5.5600E-01	0.00 2.5(I) 0.0(E) 2.5(A)
	910	5.5600E-01	15.0	0.00 Ind/Y(A)		
SR	21928	1.5600E-01	13.5	0.00 FractInd	1.5600E-01	0.00 13.5(I) 0.0(E) 13.5(A)
Y	21928	1.0000E-03	100.0	0.00 FractInd	1.0000E-03	0.00 100.0(I) 0.0(E) 100.0(A)
92 BR	21928	1.0000E-03	100.0	0.00 FractInd	1.0000E-03	0.00 100.0(I) 0.0(E) 100.0(A)
KR	21928	1.0800E-01	2.8	1.13 FractInd	1.0636E-01	1.28 2.5(I) 2.8(E) 2.8(A)
	21549	1.0100E-01	5.4	-1.13 Ind/Y(A)		
RB	21928	5.3300E-01	2.8	-0.15 FractInd	5.3335E-01	0.02 2.8(I) 0.4(E) 2.8(A)
	910	5.4700E-01	17.1	0.15 Ind/Y(A)		
SR	21928	3.4400E-01	2.6	0.00 FractInd	3.4400E-01	0.00 2.6(I) 0.0(E) 2.6(A)
Y	21928	1.5000E-02	6.7	0.00 FractInd	1.5000E-02	0.00 6.7(I) 0.0(E) 6.7(A)
NB(M)	21711	3.6700E-08	49.0	0.00 Ind/Y(A)	3.6700E-08	0.00 49.0(I) 0.0(E) 49.0(A)
NB(T)	21711	8.6800E-08	70.0	0.00 Ind/Y(A)	8.6800E-08	0.00 70.0(I) 0.0(E) 70.0(A)
93 KR	21928	2.2000E-02	5.0	2.86 FractInd	2.0055E-02	8.20 4.3(I) 12.4(E) 12.4(A)
	21549	1.6900E-02	8.3	-2.86 Ind/Y(A)		
RB	21928	3.4200E-01	5.0	-2.07 FractInd	3.4963E-01	4.28 4.8(I) 9.9(E) 9.9(A)

TABLE 8		ENERGY-THERMAL		NUCLIDES-PU-241			
Mass Elem	Ref.	Yield	Error	N-Res	Type	wt. mean	Chi/df Estimates of Error
87 KR	21549	1.4400E-01	10.1	0.00	Ind/Y(A)	1.4400E-01	0.00 10.1(I) 0.0(E) 10.1(A)
88 KR	21549	4.2700E-01	10.3	0.00	Ind/Y(A)	4.2700E-01	0.00 10.3(I) 0.0(E) 10.3(A)
89 KR	21549	5.9500E-01	9.1	0.00	Ind/Y(A)	5.9500E-01	0.00 9.1(I) 0.0(E) 9.1(A)
90 KR	21549	6.2300E-01	7.9	0.00	Ind/Y(A)	6.2300E-01	0.00 7.9(I) 0.0(E) 7.9(A)
91 KR	21549	5.1000E-01	7.1	0.00	Ind/Y(A)	5.1000E-01	0.00 7.1(I) 0.0(E) 7.1(A)
92 KR	21549	2.5000E-01	11.3	0.00	Ind/Y(A)	2.5000E-01	0.00 11.3(I) 0.0(E) 11.3(A)
93 KR	21549	6.7200E-02	11.3	0.00	Ind/Y(A)	6.7200E-02	0.00 11.3(I) 0.0(E) 11.3(A)
96 NB	101F3	3.0200E-03	9.8	0.00	Ind/Y(A)	3.0200E-03	0.00 9.8(I) 0.0(E) 9.8(A)
135 XE	607	3.3200E-02	5.0	0.47	FractInd	3.3232E-02	0.22 5.0(I) 2.3(E) 5.0(A)
268	5.2000E-02	77.0	0.47	FractInd			
136 CS	771F2	6.300E-03	12.9	0.00	Ind/Y(A)	2.6300E-03	0.00 12.9(I) 0.0(E) 12.9(A)
137 XE	21549	3.8600E-01	8.2	0.00	Ind/Y(A)	3.8600E-01	0.00 8.2(I) 0.0(E) 8.2(A)
138 XE	21549	5.9800E-01	8.4	0.00	Ind/Y(A)	5.9800E-01	0.00 8.4(I) 0.0(E) 8.4(A)
139 XE	21549	6.1600E-01	21.1	0.00	Ind/Y(A)	6.1600E-01	0.00 21.1(I) 0.0(E) 21.1(A)
140 XE	21549	5.2400E-01	10.2	0.00	Ind/Y(A)	5.2400E-01	0.00 10.2(I) 0.0(E) 10.2(A)
141 XE	21549	2.8700E-01	10.3	0.00	Ind/Y(A)	2.8700E-01	0.00 10.3(I) 0.0(E) 10.3(A)
142 XE	21549	1.1800E-01	9.3	0.00	Ind/Y(A)	1.1800E-01	0.00 9.3(I) 0.0(E) 9.3(A)

TABLE 9		ENERGY-THERMAL		NUCLIDES-M-241			
Mass Elem	Ref.	Yield	Error	N-Res	Type	wt. mean	Chi/df Estimates of Error
136 CS	769F4	0.0700E-02	22.1	0.00	Ind/Y(A)	4.0700E-02	0.00 22.1(I) 0.0(E) 22.1(A)

TABLE 10 ENERGY-THERMAL NUCLEIDE-AM-242m									
Mass Elem	Ref	Yield	Error	N Res Type	wt.mean	Chi/df Estimates of Error			
133	XE(G)	1.6400E-03	7.9	0.00	FractInd 1.6400E-03	0.00	7.9(I)	0.0(E)	7.9(A)

XE(M)	12895	4.7100E-03	10.4	0.00	FractInd 4.7100E-03	0.00	10.4(I)	0.0(E)	10.4(A)

XE(T)	12895	6.4000E-03	6.4	0.00	FractInd 6.4000E-03	0.00	6.4(I)	0.0(E)	6.4(A)

135	XE(G)	5.0000E-02	15.0	0.00	FractInd 5.0000E-02	0.00	15.0(I)	0.0(E)	15.0(A)

XE(M)	12895	8.6900E-02	6.2	0.00	FractInd 8.6900E-02	0.00	6.2(I)	0.0(E)	6.2(A)

XE(T)	12895	1.3900E-01	3.4	0.00	FractInd 1.3900E-01	0.00	3.4(I)	0.0(E)	3.4(A)
=====									

TABLE 11 ENERGY-THERMAL NUCLEIDE-CM-245									
Mass Elem	Ref	Yield	Error	N Res Type	wt.mean	Chi/df Estimates of Error			
135	XE(G)	808	1.7000E-01	12.0	0.00	FractInd 1.7000E-01	0.00	12.0(I)	0.0(E) 12.0(A)
=====									

TABLE 12 ENERGY-THERMAL NUCLIDES-CP-249									
Mass	Ref.	Yield	Error	N-Res	Type	wt. mean	Chi/df Estimates of Error		
96 NB	21604	2.6300E-03	14.0	0.00	Ind/Y(A)	2.6300E-03	0.00	14.0(I)	0.0(E) 14.0(A)
98 NB(M)	21604	6.4900E-02	20.2	0.00	Ind/Y(A)	6.4900E-02	0.00	20.2(I)	0.0(E) 20.2(A)
111 PD(M)	716	8.3000E-02	6.0	0.00	FractInd	8.3000E-02	0.00	6.0(I)	0.0(E) 6.0(A)
112 AG	716	3.5000E-02	23.0	0.00	FractInd	3.5000E-02	0.00	23.0(I)	0.0(E) 23.0(A)
130 I (G)	21604	2.0900E-02	13.6	0.00	Ind/Y(A)	2.0900E-02	0.00	13.6(I)	0.0(E) 13.6(A)
132 SB(M)	20878	2.6300E-01	18.9	0.00	Ind/Y(A)	2.6300E-01	0.00	13.5(I)	0.0(E) 13.5(A)

SB(T)	20878	3.8700E-01	18.6	0.00	Ind/Y(A)	3.8700E-01	0.00	18.6(I)	0.0(E) 18.6(A)
133 I (G)	13328	3.5000E-01	10.0	0.00	FractInd	3.5000E-01	0.00	10.0(I)	0.0(E) 10.0(A)
134 I	12710	7.2200E-01	18.3	0.00	Ind/Y(A)	7.2200E-01	0.00	18.3(I)	0.0(E) 18.3(A)
135 XE	12710	4.9700E-01	8.2	0.00	Ind/Y(A)	4.9700E-01	0.00	8.2(I)	0.0(E) 8.2(A)

XE(G)	809	3.6000E-01	12.0	0.00	FractInd	3.6000E-01	0.00	12.0(I)	0.0(E) 12.0(A)
138 CS	13318	3.7000E-01	8.0	0.00	FractInd	3.7000E-01	0.00	8.0(I)	0.0(E) 8.0(A)
139 BA	1142	1.4000E-01	20.0	0.00	FractInd	1.4000E-01	0.00	20.0(I)	0.0(E) 20.0(A)
140 CS	21604	6.5600E-02	6.1	0.00	Ind/Y(A)	6.5600E-02	0.00	6.1(I)	0.0(E) 6.1(A)

LA	674	3.5000E-02	5.0	0.00	FractInd	3.5000E-02	0.00	5.0(I)	0.0(E) 5.0(A)
142 LA	1142	2.9000E-01	10.0	0.00	FractInd	2.9000E-01	0.00	10.0(I)	0.0(E) 10.0(A)

TABLE 13 ENERGY-FAST NUCLIDES-FH-232									
Mass Elem.	Ref.	Yield	Error	N-Res	Type	wt. mean	Chi/df Estimates of Error		
85 BR	2068	4.7000E-02	10.0	0.00	FractInd	4.7000E-02	0.00	10.0(I)	0.0(E) 10.0(A)
86 BR	2068	1.8400E-01	20.0	0.00	FractInd	1.8400E-01	0.00	20.0(I)	0.0(E) 20.0(A)

BR	21805	6.3300E-05	22.4	0.00	Ind/Y(A)	6.3300E-05	0.00	22.4(I)	0.0(E) 22.4(A)
90 KR	30425	7.6200E-01	15.0	0.00	FractInd	7.6200E-01	0.00	15.0(I)	0.0(E) 15.0(A)
91 KR	30425	7.4000E-01	8.7	0.00	FractInd	7.4000E-01	0.00	8.6(I)	0.0(E) 8.6(A)
96 NB	13441	3.0000E-05	1000.0	0.00	FractInd	3.0000E-05	0.00	*****	0.0(E)*****
110 AG(M)	13441	1.0000E-04	15.0	0.00	FractInd	1.0000E-04	0.00	15.0(I)	0.0(E) 15.0(A)
131 SN	30425	7.1000E-01	28.5	0.00	FractInd	7.1000E-01	0.00	28.5(I)	0.0(E) 28.5(A)

TE	21805	1.8500E-02	29.1	0.00	Ind/Y(A)	1.8500E-02	0.00	29.1(I)	0.0(E) 29.1(A)
132 SN	30425	5.2900E-01	16.1	0.46	FractInd	5.5549E-01	0.21	11.2(I)	5.1(E) 11.2(A)
21805	5.8600E-01	15.6	0.46	Ind/Y(A)					

SB	30425	3.3000E-01	40.0	0.00	FractInd	3.3000E-01	0.00	40.0(I)	0.0(E) 40.0(A)
134 I	13430	7.7000E-02	52.0	0.00	FractInd	7.7000E-02	0.00	52.0(I)	0.0(E) 52.0(A)

I (G)	2068	8.4800E-03	30.0	0.00	FractInd	8.4800E-03	0.00	30.0(I)	0.0(E) 30.0(A)

I (M)	2068	7.5200E-03	30.0	0.00	FractInd	7.5200E-03	0.00	30.0(I)	0.0(E) 30.0(A)
135 I	2068	1.6200E-01	20.0	0.59	FractInd	1.4755E-01	0.34	14.3(I)	8.4(E) 14.3(A)
21805	1.3700E-01	20.2	-0.59	Ind/Y(A)					

136 I (G)	2068	9.6900E-02	25.0	0.00	FractInd	9.6900E-02	0.00	25.0(I)	0.0(E) 25.0(A)

I (M)	2068	2.3710E-01	25.0	0.00	FractInd	2.3710E-01	0.00	25.0(I)	0.0(E) 25.0(A)

CS	13430	6.3000E-04	5.0w	2.32	FractInd	8.8856E-05	3.71	62.9(I)	121.1(E) 121.1(A)
322x3	0.0400E-04	59.8	1.24	Ind/Y(A)					
21805	3.0500E-05	8.7w	-2.50	Ind/Y(A)					

139 XE	30425	7.5500E-01	10.3	0.00	FractInd	7.5500E-01	0.00	10.3(I)	0.0(E) 10.3(A)
140 XE	30425	7.7300E-01	7.2	0.00	FractInd	7.7300E-01	0.00	7.2(I)	0.0(E) 7.2(A)

TABLE 14 ENERGY-FAST NUCLEI-U -235									
Mass Elem	Ref.	Yield	Error	N-Res	Type	wt. mean	Chi/df	Estimates of Error	
86 BR	21743 4.3000E-01	5.7	0.00	Ind/Y(A)	4.3000E-01	0.00	5.7(I)	0.0(E)	5.7(A)
87 BR	21743 6.1500E-01	6.1	0.00	Ind/Y(A)	6.1500E-01	0.00	6.1(I)	0.0(E)	6.1(A)
88 BR	21743 1.6400E-01	19.3	0.00	Ind/Y(A)	1.6400E-01	0.00	19.3(I)	0.0(E)	19.3(A)
89 BR	21743 5.2000E-01	5.8	0.00	Ind/Y(A)	5.2000E-01	0.00	5.8(I)	0.0(E)	5.8(A)
90 BR	21743 1.2200E-01	6.7	0.00	Ind/Y(A)	1.2200E-01	0.00	6.7(I)	0.0(E)	6.7(A)
91 BR	21743 2.2400E-02	33.3	0.00	Ind/Y(A)	2.2400E-02	0.00	33.3(I)	0.0(E)	33.3(A)
92 BR	21743 6.2000E-01	4.9	0.00	Ind/Y(A)	6.2000E-01	0.00	4.9(I)	0.0(E)	4.9(A)
93 BR	21743 2.5300E-01	15.4	0.00	Ind/Y(A)	2.5300E-01	0.00	15.4(I)	0.0(E)	15.4(A)
94 BR	21743 5.7400E-03	33.4	0.00	Ind/Y(A)	5.7400E-03	0.00	33.4(I)	0.0(E)	33.4(A)
95 BR	21743 4.6000E-01	5.3	0.00	Ind/Y(A)	4.6000E-01	0.00	5.3(I)	0.0(E)	5.3(A)
96 BR	21743 4.2800E-02	8.9	0.00	Ind/Y(A)	4.2800E-02	0.00	8.9(I)	0.0(E)	8.9(A)
97 BR	21743 5.3000E-02	6.7	0.00	Ind/Y(A)	5.3000E-02	0.00	6.7(I)	0.0(E)	6.7(A)
98 BR	21743 5.6100E-01	5.3	0.00	Ind/Y(A)	5.6100E-01	0.00	5.3(I)	0.0(E)	5.3(A)
99 BR	21743 3.9000E-01	10.8	0.00	Ind/Y(A)	3.9000E-01	0.00	10.8(I)	0.0(E)	10.8(A)
100 BR	21743 3.5900E-02	95.2	0.00	Ind/Y(A)	3.5900E-02	0.00	95.2(I)	0.0(E)	95.2(A)
101 BR	21743 9.7200E-03	17.1	0.00	Ind/Y(A)	9.7200E-03	0.00	17.1(I)	0.0(E)	17.1(A)
102 BR	21743 2.9300E-01	9.0	0.00	Ind/Y(A)	2.9300E-01	0.00	9.0(I)	0.0(E)	9.0(A)
103 BR	21743 5.6500E-01	6.7	0.00	Ind/Y(A)	5.6500E-01	0.00	6.7(I)	0.0(E)	6.7(A)
104 BR	21743 7.9400E-02	30.8	0.00	Ind/Y(A)	7.9400E-02	0.00	30.8(I)	0.0(E)	30.8(A)
105 BR	21743 1.8800E-01	20.7	0.00	Ind/Y(A)	1.8800E-01	0.00	20.7(I)	0.0(E)	20.7(A)
106 BR	21743 5.9700E-01	7.3	0.00	Ind/Y(A)	5.9700E-01	0.00	7.3(I)	0.0(E)	7.3(A)
107 BR	21743 3.4700E-01	12.4	0.00	Ind/Y(A)	3.4700E-01	0.00	12.4(I)	0.0(E)	12.4(A)
108 BR	21743 5.8100E-01	5.5	0.00	Ind/Y(A)	5.8100E-01	0.00	5.5(I)	0.0(E)	5.5(A)
109 BR	21743 1.6400E-04	23.8	0.00	FractInd	1.6400E-04	0.00	23.8(I)	0.0(E)	23.8(A)
110 BR	21743 6.7400E-04	4.9	0.00	FractInd	6.7400E-04	0.00	4.9(I)	0.0(E)	4.9(A)
111 BR	21743 8.3700E-04	6.2	0.00	FractInd	8.3700E-04	0.00	6.2(I)	0.0(E)	6.2(A)
112 BR	21743 6.4500E-01	3.9	0.00	Ind/Y(A)	6.4500E-01	0.00	3.9(I)	0.0(E)	3.9(A)
113 BR	21743 2.7200E-01	5.1	0.00	Ind/Y(A)	2.7200E-01	0.00	5.1(I)	0.0(E)	5.1(A)
114 BR	21743 3.2000E-01	4.6	0.00	Ind/Y(A)	3.2000E-01	0.00	4.6(I)	0.0(E)	4.6(A)
115 BR	21743 6.1500E-01	7.6	0.00	Ind/Y(A)	6.1500E-01	0.00	7.6(I)	0.0(E)	7.6(A)
116 BR	21743 1.7500E-02	24.0	0.00	FractInd	1.7500E-02	0.00	24.0(I)	0.0(E)	24.0(A)
117 BR	21743 2.9800E-02	5.7	0.00	FractInd	2.9800E-02	0.00	5.7(I)	0.0(E)	5.7(A)
118 BR	21743 4.7500E-02	8.2	1.89	FractInd	5.1259E-02	3.56	6.5(I)	12.3(E)	12.3(A)
119 BR	21743 6.1900E-02	10.6	1.89	Ind/Y(A)					
120 BR	21743 1.3900E-01	6.7	0.00	Ind/Y(A)	1.3900E-01	0.00	6.7(I)	0.0(E)	6.7(A)
121 BR	21743 6.4300E-01	6.7	0.00	Ind/Y(A)	6.4300E-01	0.00	6.7(I)	0.0(E)	6.7(A)
122 BR	21743 2.2900E-01	11.6	0.00	Ind/Y(A)	2.2900E-01	0.00	11.6(I)	0.0(E)	11.6(A)
123 BR	21743 2.5000E-03	12.0	2.31	FractInd	1.8170E-03	4.15	2.7(I)	5.5(E)	5.5(A)
124 BR	963r1.7400E-03	8.5	-0.55	Ind/Y(A)					
125 BR	21743 3.9900E-01	6.4	0.00	Ind/Y(A)	3.9900E-01	0.00	6.4(I)	0.0(E)	6.4(A)
126 BR	21743 5.2000E-02	64.5	0.00	Ind/Y(A)	5.2000E-02	0.00	64.5(I)	0.0(E)	64.5(A)
127 BR	21743 1.9300E-01	5.8	0.00	Ind/Y(A)	1.9300E-01	0.00	5.8(I)	0.0(E)	5.8(A)
128 BR	21743 6.8500E-01	5.6	0.00	Ind/Y(A)	6.8500E-01	0.00	5.6(I)	0.0(E)	5.6(A)
129 BR	21743 1.2400E-01	18.8	0.00	Ind/Y(A)	1.2400E-01	0.00	18.8(I)	0.0(E)	18.8(A)
130 BR	21743 7.3600E-02	6.5	0.00	Ind/Y(A)	7.3600E-02	0.00	6.5(I)	0.0(E)	6.5(A)
131 BR	21743 5.8300E-01	6.1	0.00	Ind/Y(A)	5.8300E-01	0.00	6.1(I)	0.0(E)	6.1(A)
132 BR	21743 3.3500E-01	9.4	0.00	Ind/Y(A)	3.3500E-01	0.00	9.4(I)	0.0(E)	9.4(A)
133 BR	21743 4.3500E-01	5.1	0.00	Ind/Y(A)	4.3500E-01	0.00	5.1(I)	0.0(E)	5.1(A)
134 BR	21743 5.2300E-01	6.5	0.00	Ind/Y(A)	5.2300E-01	0.00	6.5(I)	0.0(E)	6.5(A)
135 BR	21743 1.0900E-01	21.1	0.00	Ind/Y(A)	1.0900E-01	0.00	21.1(I)	0.0(E)	21.1(A)
136 BR	21743 4.4500E-01	5.1	0.00	Ind/Y(A)	4.4500E-01	0.00	5.1(I)	0.0(E)	5.1(A)
137 BR	21743 5.2300E-01	5.4	0.00	Ind/Y(A)	5.2300E-01	0.00	5.4(I)	0.0(E)	5.4(A)
138 BR	21743 2.1600E-01	9.9	0.00	Ind/Y(A)	2.1600E-01	0.00	9.9(I)	0.0(E)	9.9(A)
139 BR	21743 6.3900E-01	4.3	0.00	Ind/Y(A)	6.3900E-01	0.00	4.3(I)	0.0(E)	4.3(A)
140 BR	21743 7.6800E-02	8.0	0.00	Ind/Y(A)	7.6800E-02	0.00	8.0(I)	0.0(E)	8.0(A)
141 BR	21743 6.0900E-01	6.8	0.00	Ind/Y(A)	6.0900E-01	0.00	6.8(I)	0.0(E)	6.8(A)
142 BR	21743 3.7400E-01	6.6	0.00	Ind/Y(A)	3.7400E-01	0.00	6.6(I)	0.0(E)	6.6(A)

TABLE 15 ENERGY-FAST NUCLEI:U -236									
Mass Elem.	Ref.	Yield	Error	N Res Type	wt.mean	Chi/df	Estimates of Error		
136 CS	989+6.9600E-04	22.4	0.00	Ind/Y(A)	6.9600E-04	0.00	22.4(I)	0.0(E)	22.4(A)

TABLE 16 ENERGY-FAST NUCLEI:U -238									
Mass Elem.	Ref.	Yield	Error	N Res Type	wt.mean	Chi/df	Estimates of Error		
89 RB	876 3.9000E-02	56.0	0.00	Ind/Y(A)	3.9000E-02	0.00	56.0(I)	0.0(E)	56.0(A)
91 RB	876 2.2300E-01	32.1	0.00	Ind/Y(A)	2.2300E-01	0.00	32.1(I)	0.0(E)	32.1(A)
92 RB	876 2.6100E-01	28.2	0.00	Ind/Y(A)	2.6100E-01	0.00	28.2(I)	0.0(E)	28.2(A)
93 RB	876 5.4400E-01	23.4	0.00	Ind/Y(A)	5.4400E-01	0.00	23.4(I)	0.0(E)	23.4(A)
94 RB	876 4.9800E-01	26.3	0.00	Ind/Y(A)	4.9800E-01	0.00	26.3(I)	0.0(E)	26.3(A)
95 RB	876 3.2200E-01	25.0	0.00	Ind/Y(A)	3.2200E-01	0.00	25.0(I)	0.0(E)	25.0(A)
97 RB	876 1.6300E-02	27.0	0.00	Ind/Y(A)	1.6300E-02	0.00	27.0(I)	0.0(E)	27.0(A)
133 XE(G)	12895 2.5000E-04	20.0	0.00	FractInd	2.5000E-04	0.00	20.0(I)	0.0(E)	20.0(A)
XE(M)	12895 1.5000E-03	20.0	0.00	FractInd	1.5000E-03	0.00	20.0(I)	0.0(E)	20.0(A)
XE(T)	12895 1.7000E-03	20.0	0.00	FractInd	1.7000E-03	0.00	20.0(I)	0.0(E)	20.0(A)
136 CS	13326 1.4100E-04	9.9w	-2.47	FractInd	2.5992E-04	6.15	8.5(I)	21.0(E)	21.0(A)
	1014+2.8400E-04	8.5	2.40	Ind/Y(A)					
	163 5.3700E-03	20.5w	2.50	Ind/Y(A)					
CS(G)	13473 9.4000E-04	5.0	0.00	FractInd	9.4000E-04	0.00	5.0(I)	0.0(E)	5.0(A)
138 CS	876 5.8600E-02	73.0	1.13	Ind/Y(A)	1.1078E-02	1.27	63.4(I)	71.4(E)	71.4(A)
	876 9.7600E-03	73.0	-1.13	Ind/Y(A)					
139 CS	875 5.8300E-02	26.2	0.00	Ind/Y(A)	5.8300E-02	0.00	26.2(I)	0.0(E)	26.2(A)
141 CS	876 3.0000E-01	22.3	0.00	Ind/Y(A)	3.0000E-01	0.00	22.3(I)	0.0(E)	22.3(A)
142 CS	876 4.0200E-01	23.2	0.00	Ind/Y(A)	4.0200E-01	0.00	23.2(I)	0.0(E)	23.2(A)
143 CS	876 3.8500E-01	25.0	0.00	Ind/Y(A)	3.8500E-01	0.00	25.0(I)	0.0(E)	25.0(A)
145 CS	876 1.3100E-01	22.2	0.00	Ind/Y(A)	1.3100E-01	0.00	22.2(I)	0.0(E)	22.2(A)
146 CS	876 3.1800E-02	33.2	0.00	Ind/Y(A)	3.1800E-02	0.00	33.2(I)	0.0(E)	33.2(A)

TABLE 17		ENERGY-FAST				NUCLIDE-NP-237			
Mass Elem.	Ref.	Yield	Error	N-Res	Type	wt. mean	Chi/df Estimates of Error		
134 I	40677	3.4000E-01	58.8	0.00	FractInd	3.4000E-01	0.00	58.8(I)	0.0(E) 58.8(A)
135 XE	40677	3.3000E-02	45.5	0.00	FractInd	3.3000E-02	0.00	45.5(I)	0.0(E) 45.5(A)
136 CS	991r9	8300E-03	16.8	0.00	Ind/Y(A)	9.8300E-03	0.00	16.8(I)	0.0(E) 16.8(A)

TABLE 18		ENERGY-FAST				NUCLIDE-PU-239			
Mass Elem.	Ref.	Yield	Error	N-Res	Type	wt. mean	Chi/df Estimates of Error		
136 CS	13326	1.9700E-02	10.2	0.54	FractInd	1.8728E-02	2.29	4.5(I)	6.9(E) 6.9(A)
	1029r1	5700E-02	11.5	-1.90	Ind/Y(A)				
	1035r1	9000E-02	11.5	0.14	Ind/Y(A)				
	1042r1	1580E-02	11.5	1.30	Ind/Y(A)				
	1041r2	1800E-02	11.5	1.30	Ind/Y(A)				
	1042r2	2600E-02	11.5	1.58	Ind/Y(A)				
	1030r1	2500E-02	11.5w	-2.50	Ind/Y(A)				
138 I	940	1.5600E-01	10.0	0.00	FractInd	1.5600E-01	0.00	10.0(I)	0.0(E) 10.0(A)
	940	6.2500E-01	10.0	0.00	FractInd	6.2500E-01	0.00	10.0(I)	0.0(E) 10.0(A)
CS	940	2.1100E-01	10.0	0.00	FractInd	2.1100E-01	0.00	10.0(I)	0.0(E) 10.0(A)

TABLE 19 ENERGY-FAST NUCLEIDS-PU-240			
Mass Elem.	Ref.	Yield	Chi/df Estimates of Error
96 NB	10821	4.7200E-04	3.4 0.00 FractInd 4.7200E-04 0.00 3.4(I) 0.0(E) 3.4(A)
136 CS	10821	8.7400E-03	3.0 0.00 FractInd 8.7400E-03 0.00 3.0(I) 0.0(E) 3.0(A)

TABLE 20 ENERGY-HIGH NUCLEIDS-PH-232			
Mass Elem.	Ref.	Yield	Chi/df Estimates of Error
88 KR	708	4.0900E-01	15.6 0.00 Ind/Y(A) 4.0900E-01 0.00 15.6(I) 0.0(E) 15.6(A)
89 KR	708	4.6500E-01	14.6 0.00 Ind/Y(A) 4.6500E-01 0.00 14.6(I) 0.0(E) 14.6(A)
90 KR	708	6.5300E-01	18.6 0.00 Ind/Y(A) 6.5300E-01 0.00 18.6(I) 0.0(E) 18.6(A)
91 KR	708	5.3200E-01	8.0 0.00 Ind/Y(A) 5.3200E-01 0.00 8.0(I) 0.0(E) 8.0(A)
92 KR	708	3.8100E-01	10.5 0.00 Ind/Y(A) 3.8100E-01 0.00 10.5(I) 0.0(E) 10.5(A)
93 KR	708	1.2700E-01	15.4 0.00 Ind/Y(A) 1.2700E-01 0.00 15.4(I) 0.0(E) 15.4(A)
95 NB	677	3.7700E-02	22.8 0.00 Ind/Y(A) 3.7700E-02 0.00 22.8(I) 0.0(E) 22.8(A)
99 TC	677	1.7400E-03	21.5 0.00 Ind/Y(A) 1.7400E-03 0.00 21.5(I) 0.0(E) 21.5(A)
106 RH	677	6.7100E-03	20.3 0.00 Ind/Y(A) 6.7100E-03 0.00 20.3(I) 0.0(E) 20.3(A)

RH(M)	30785	1.3400E-04	50.5 0.00 Ind/Y(A) 1.3400E-04 0.00 50.5(I) 0.0(E) 50.5(A)
112 AG	677	1.1600E-02	23.6 2.22 Ind/Y(A) 6.0712E-03 2.56 18.9(I) 30.3(E) 30.3(A)
	30695	4.3800E-03	40.3 -1.26 Ind/Y(A)
	30785	5.4500E-03	35.4 -0.46 Ind/Y(A)
132 I (G)	723	3.5800E-02	20.6 0.34 Ind/Y(A) 3.3898E-02 0.12 14.4(I) 5.0(E) 14.4(A)
	30695	3.2400E-02	20.2 -0.34 Ind/Y(A)
133 I	636	8.0000E-02	25.0 -0.84 FractInd 9.0462E-02 0.71 17.3(I) 14.5(E) 17.3(A)
	723	1.0700E-01	23.5 0.84 Ind/Y(A)
134 I	636	1.5200E-01	3.0 1.56 FractInd 1.5064E-01 1.36 3.0(I) 3.5(E) 3.5(A)
	724	1.0700E-01	25.7 -1.61 Ind/Y(A)
	30695	1.3500E-01	33.9 -0.34 Ind/Y(A)

CS (G)	677	7.0800E-03	11.7 0.00 Ind/Y(A) 7.0800E-03 0.00 11.7(I) 0.0(E) 11.7(A)
CS (M)	30695	5.3700E-05	52.0 0.00 Ind/Y(A) 5.3700E-05 0.00 52.0(I) 0.0(E) 52.0(A)
135 I	636	4.7000E-01	17.0 0.00 FractInd 4.7000E-01 0.00 17.0(I) 0.0(E) 17.0(A)

CS (G)	677	2.2100E-02	27.7 0.00 Ind/Y(A) 2.2100E-02 0.00 27.7(I) 0.0(E) 27.7(A)
CS (M)	30695	1.0600E-03	35.0 0.00 Ind/Y(A) 1.0600E-03 0.00 35.0(I) 0.0(E) 35.0(A)
136 CS	30695	1.5600E-03	20.6 -5.04 Ind/Y(A) 1.7508E-03 25.38 18.2(I) 91.8(E) 91.8(A)
	646	1.5300E-02	17.7 5.04 Ind/Y(A)
139 XB	708	5.9500E-01	15.8 0.00 Ind/Y(A) 5.9500E-01 0.00 15.8(I) 0.0(E) 15.8(A)
140 XB	708	5.4700E-01	13.5 0.00 Ind/Y(A) 5.4700E-01 0.00 13.5(I) 0.0(E) 13.5(A)

LA	30695	6.1300E-03	20.3 0.00 Ind/Y(A) 6.1300E-03 0.00 20.3(I) 0.0(E) 20.3(A)
141 XB	708	2.5200E-01	15.6 0.00 Ind/Y(A) 2.5200E-01 0.00 15.6(I) 0.0(E) 15.6(A)
142 XB	708	1.4400E-01	19.5 0.00 Ind/Y(A) 1.4400E-01 0.00 19.5(I) 0.0(E) 19.5(A)

TABLE 21 ENERGY-HIGH NUCLIDES-U -233									
Mass Elem.	Ref.	Yield	Error	N Res	Type	wt. mean	Chi/df	Estimates of Error	
87 KR	705 5.7400E-01	25.0	0.00	Ind/Y(A)	5.7400E-01	0.00	25.0(I)	0.0(E)	25.0(A)
88 KR	705 6.0500E-01	17.5	0.00	Ind/Y(A)	6.0500E-01	0.00	17.5(I)	0.0(E)	17.5(A)
89 KR	705 6.5800E-01	19.4	0.00	Ind/Y(A)	6.5800E-01	0.00	19.4(I)	0.0(E)	19.4(A)
91 KR	705 2.4000E-01	14.7	0.00	Ind/Y(A)	2.4000E-01	0.00	14.7(I)	0.0(E)	14.7(A)
92 KR	705 9.3700E-02	24.7	0.00	Ind/Y(A)	9.3700E-02	0.00	24.7(I)	0.0(E)	24.7(A)
93 KR	705 1.7300E-02	31.3	0.00	Ind/Y(A)	1.7300E-02	0.00	31.3(I)	0.0(E)	31.3(A)
136 CS	62 9.2100E-02	15.0	0.00	FractInd	9.2100E-02	0.00	15.0(I)	0.0(E)	15.0(A)
137 XE	705 6.3500E-01	6.9	0.00	Ind/Y(A)	6.3500E-01	0.00	6.9(I)	0.0(E)	6.9(A)
139 XE	705 1.6900E-01	12.1	0.00	Ind/Y(A)	1.6900E-01	0.00	12.1(I)	0.0(E)	12.1(A)
140 XE	705 8.3000E-02	13.0	0.00	Ind/Y(A)	8.3000E-02	0.00	13.0(I)	0.0(E)	13.0(A)
141 XE	705 2.0900E-02	22.3	0.00	Ind/Y(A)	2.0900E-02	0.00	22.3(I)	0.0(E)	22.3(A)
121 CD	12813 4.3700E-01	48.1	0.00	Ind/Y(A)	4.3700E-01	0.00	48.1(I)	0.0(E)	48.1(A)
IN	12813 3.9900E-01	27.1	0.00	Ind/Y(A)	3.9900E-01	0.00	27.1(I)	0.0(E)	27.1(A)
SN	12813 4.2900E-02	116.0	0.00	Ind/Y(A)	4.2900E-02	0.00	116.0(I)	0.0(E)	116.0(A)
131 TE(G)	396 3.0000E-01	15.0	0.00	FractInd	3.0000E-01	0.00	15.0(I)	0.0(E)	15.0(A)
TE(M)	396 3.5000E-01	15.0	0.00	FractInd	3.5000E-01	0.00	15.0(I)	0.0(E)	15.0(A)
I	396 8.0000E-02	15.0	0.00	FractInd	8.0000E-02	0.00	15.0(I)	0.0(E)	15.0(A)
132 I	396 1.6000E-01	7.0	0.00	FractInd	1.6000E-01	0.00	7.0(I)	0.0(E)	7.0(A)
133 TE	396 4.0000E-01	15.0	0.00	FractInd	4.0000E-01	0.00	15.0(I)	0.0(E)	15.0(A)
XE(G)	12895 5.1000E-03	10.8	0.00	FractInd	5.1000E-03	0.00	10.8(I)	0.0(E)	10.8(A)
XE(M)	717 2.2000E-02	32.0	0.54	FractInd	2.5772E-02	0.30	4.9(I)	2.7(E)	4.9(A)
12895 2.5900E-02	5.0	0.54	FractInd						
XE(T)	12895 3.1000E-02	5.0	0.00	FractInd	3.1000E-02	0.00	5.0(I)	0.0(E)	5.0(A)
134 I	181 4.0000E-01	15.0	-0.47	FractInd	4.2659E-01	0.22	4.7(I)	2.2(E)	4.7(A)
396 4.3000E-02	5.0	0.47	FractInd						
135 XE(G)	12895 8.3000E-02	13.3	0.00	FractInd	8.3000E-02	0.00	13.3(I)	0.0(E)	13.3(A)
XE(M)	12895 1.6000E-01	5.0	0.00	FractInd	1.6000E-01	0.00	5.0(I)	0.0(E)	5.0(A)
XE(T)	12895 2.4300E-01	5.0	-0.96	FractInd	2.5093E-01	0.91	3.5(I)	3.4(E)	3.5(A)
717 2.6000E-01	5.0	0.96	FractInd						
136 CS	713 4.0000E-02	12.0	-0.95	FractInd	4.4107E-02	2.75	4.7(I)	7.7(E)	7.7(A)
13347 4.8000E-02	6.2	1.78	FractInd						
162 2.8500E-02	14.9w	-2.50	Ind/Y(A)						
987r4.5900E-02	8.9	0.51	Ind/Y(A)						
137 XE	706 6.2900E-01	21.3	0.00	Ind/Y(A)	6.2900E-01	0.00	21.3(I)	0.0(E)	21.3(A)
138 I	941 9.7000E-02	10.0	0.00	FractInd	9.7000E-02	0.00	10.0(I)	0.0(E)	10.0(A)
XE	941 5.9000E-01	10.0	0.00	FractInd	5.9000E-01	0.00	10.0(I)	0.0(E)	10.0(A)
CS	941 3.0100E-01	10.0	0.00	FractInd	3.0100E-01	0.00	10.0(I)	0.0(E)	10.0(A)
139 XE	706 3.8300E-01	17.5	0.00	Ind/Y(A)	3.8300E-01	0.00	17.5(I)	0.0(E)	17.5(A)
140 XE	706 2.1600E-01	16.1	0.00	Ind/Y(A)	2.1600E-01	0.00	16.1(I)	0.0(E)	16.1(A)
LA	638 7.3500E-03	20.0	0.00	FractInd	7.3500E-03	0.00	20.0(I)	0.0(E)	20.0(A)
141 XE	706 5.6700E-02	16.5	0.00	Ind/Y(A)	5.6700E-02	0.00	16.5(I)	0.0(E)	16.5(A)
148 PM(G)	1183 1.0500E-06	12.4	0.00	FractInd	1.0500E-06	0.00	12.4(I)	0.0(E)	12.4(A)
PM(M)	1183 8.0000E-06	7.5	0.00	FractInd	8.0000E-06	0.00	7.5(I)	0.0(E)	7.5(A)
PM(T)	1183 9.1000E-06	6.6	0.00	FractInd	9.1000E-06	0.00	6.6(I)	0.0(E)	6.6(A)
150 PM	1183 1.7900E-03	8.4	0.00	FractInd	1.7900E-03	0.00	8.4(I)	0.0(E)	8.4(A)

TABLE 22 ENERGY-HIGH NUCLIDES-U -235									
Mass Elem.	Ref.	Yield	Error	N Res	Type	wt. mean	Chi/df	Estimates of Error	
82 BR	181 3.0000E-03	15.0	4.72	FractInd	9.4606E-04	22.31	12.3(I)	57.9(E)	57.9(A)
403 8.0000E-04	15.0	-4.72	FractInd						
77 KR	706 3.1500E-01	20.6	0.00	Ind/Y(A)	3.1500E-01	0.00	20.6(I)	0.0(E)	20.6(A)
88 KR	706 3.5600E-01	22.4	0.00	Ind/Y(A)	3.5600E-01	0.00	22.4(I)	0.0(E)	22.4(A)
89 KR	706 6.2200E-01	18.1	0.00	Ind/Y(A)	6.2200E-01	0.00	18.1(I)	0.0(E)	18.1(A)
90 KR	706 5.4100E-01	18.1	0.00	Ind/Y(A)	5.4100E-01	0.00	18.1(I)	0.0(E)	18.1(A)
91 KR	706 3.8100E-01	19.2	0.00	Ind/Y(A)	3.8100E-01	0.00	19.2(I)	0.0(E)	19.2(A)
92 Y	638 7.7000E-03	20.0	0.00	FractInd	7.7000E-03	0.00	20.0(I)	0.0(E)	20.0(A)
93 KR	706 3.4900E-02	22.4	0.00	Ind/Y(A)	3.4900E-02	0.00	22.4(I)	0.0(E)	22.4(A)
96 NB	638 8.0000E-04	10.0	0.00	FractInd	8.0000E-04	0.00	10.0(I)	0.0(E)	10.0(A)
97 NB	713 6.9000E-02	22.0	0.00	FractInd	6.9000E-02	0.00	22.0(I)	0.0(E)	22.0(A)
112 AG	713 5.1000E-02	12.0	0.00	FractInd	5.1000E-02	0.00	12.0(I)	0.0(E)	12.0(A)
121 CD	12813 4.3700E-01	48.1	0.00	Ind/Y(A)	4.3700E-01	0.00	48.1(I)	0.0(E)	48.1(A)
IN	12813 3.9900E-01	27.1	0.00	Ind/Y(A)	3.9900E-01	0.00	27.1(I)	0.0(E)	27.1(A)
SN	12813 4.2900E-02	116.0	0.00	Ind/Y(A)	4.2900E-02	0.00	116.0(I)	0.0(E)	116.0(A)
131 TE(G)	396 3.0000E-01	15.0	0.00	FractInd	3.0000E-01	0.00	15.0(I)	0.0(E)	15.0(A)
TE(M)	396 3.5000E-01	15.0	0.00	FractInd	3.5000E-01	0.00	15.0(I)	0.0(E)	15.0(A)
I	396 8.0000E-02	15.0	0.00	FractInd	8.0000E-02	0.00	15.0(I)	0.0(E)	15.0(A)
132 I	396 1.6000E-01	7.0	0.00	FractInd	1.6000E-01	0.00	7.0(I)	0.0(E)	7.0(A)
133 TE	396 4.0000E-01	15.0	0.00	FractInd	4.0000E-01	0.00	15.0(I)	0.0(E)	15.0(A)
XE(G)	12895 5.1000E-03	10.8	0.00	FractInd	5.1000E-03	0.00	10.8(I)	0.0(E)	10.8(A)
XE(M)	717 2.2000E-02	32.0	0.54	FractInd	2.5772E-02	0.30	4.9(I)	2.7(E)	4.9(A)
12895 2.5900E-02	5.0	0.54	FractInd						
XE(T)	12895 3.1000E-02	5.0	0.00	FractInd	3.1000E-02	0.00	5.0(I)	0.0(E)	5.0(A)
134 I	181 4.0000E-01	15.0	-0.47	FractInd	4.2659E-01	0.22	4.7(I)	2.2(E)	4.7(A)
396 4.3000E-02	5.0	0.47	FractInd						
135 XE(G)	12895 8.3000E-02	13.3	0.00	FractInd	8.3000E-02	0.00	13.3(I)	0.0(E)	13.3(A)
XE(M)	12895 1.6000E-01	5.0	0.00	FractInd	1.6000E-01	0.00	5.0(I)	0.0(E)	5.0(A)
XE(T)	12895 2.4300E-01	5.0	-0.96	FractInd	2.5093E-01	0.91	3.5(I)	3.4(E)	3.5(A)
717 2.6000E-01	5.0	0.96	FractInd						
136 CS	713 4.0000E-02	12.0	-0.95	FractInd	4.4107E-02	2.75	4.7(I)	7.7(E)	7.7(A)
13347 4.8000E-02	6.2	1.78	FractInd						
162 2.8500E-02	14.9w	-2.50	Ind/Y(A)						
987r4.5900E-02	8.9	0.51	Ind/Y(A)						
137 XE	706 6.2900E-01	21.3	0.00	Ind/Y(A)	6.2900E-01	0.00	21.3(I)	0.0(E)	21.3(A)
138 I	941 9.7000E-02	10.0	0.00	FractInd	9.7000E-02	0.00	10.0(I)	0.0(E)	10.0(A)
XE	941 5.9000E-01	10.0	0.00	FractInd	5.9000E-01	0.00	10.0(I)	0.0(E)	10.0(A)
CS	941 3.0100E-01	10.0	0.00	FractInd	3.0100E-01	0.00	10.0(I)	0.0(E)	10.0(A)
139 XE	706 3.8300E-01	17.5	0.00	Ind/Y(A)	3.8300E-01	0.00	17.5(I)	0.0(E)	17.5(A)
140 XE	706 2.1600E-01	16.1	0.00	Ind/Y(A)	2.1600E-01	0.00	16.1(I)	0.0(E)	16.1(A)
LA	638 7.3500E-03	20.0	0.00	FractInd	7.3500E-03	0.00	20.0(I)	0.0(E)	20.0(A)
141 XE	706 5.6700E-02	16.5	0.00	Ind/Y(A)	5.6700E-02	0.00	16.5(I)	0.0(E)	16.5(A)
148 PM(G)	1183 1.0500E-06	12.4	0.00	FractInd	1.0500E-06	0.00	12.4(I)	0.0(E)	12.4(A)
PM(M)	1183 8.0000E-06	7.5	0.00	FractInd	8.0000E-06	0.00	7.5(I)	0.0(E)	7.5(A)
PM(T)	1183 9.1000E-06	6.6	0.00	FractInd	9.1000E-06	0.00	6.6(I)	0.0(E)	6.6(A)
150 PM	1183 1.7900E-03	8.4	0.00	FractInd	1.7900E-03	0.00	8.4(I)	0.0(E)	8.4(A)

TABLE 23		ENERGY-HIGH		NUCLIDE-U -238		wt. mean		Chi/df Estimates of Error	
Mass Elem.	Ref.	Yield	N-Res	Type					
87 KR	707	4.3200E-01	6.2	0.00	Ind/Y(A)	4.3200E-01	0.00	6.2(I)	0.0(E) 6.2(A)
88 KR	707	2.9900E-01	13.2	0.00	Ind/Y(A)	2.9900E-01	0.00	13.2(I)	0.0(E) 13.2(A)
89 KR	707	5.0600E-01	14.4	0.00	Ind/Y(A)	5.0600E-01	0.00	14.4(I)	0.0(E) 14.4(A)
90 KR	707	5.7600E-01	11.2	0.00	Ind/Y(A)	5.7600E-01	0.00	11.2(I)	0.0(E) 11.2(A)
91 KR	707	5.5300E-01	11.2	0.00	Ind/Y(A)	5.5300E-01	0.00	11.2(I)	0.0(E) 11.2(A)
92 KR	707	4.3900E-01	12.1	0.00	Ind/Y(A)	4.3900E-01	0.00	12.1(I)	0.0(E) 12.1(A)
93 KR	707	1.6900E-01	13.3	0.00	Ind/Y(A)	1.6900E-01	0.00	13.3(I)	0.0(E) 13.3(A)
101 TC	795	4.6200E-02	2.1	0.00	Ind/Y(A)	4.6200E-02	0.00	2.1(I)	0.0(E) 2.1(A)
131 TE(G)	30639	3.8000E-01	15.5	0.58	Ind/Y(A)	4.1269E-01	0.34	10.4(I)	6.1(E) 10.4(A)
136 CS	13347	3.7000E-03	8.1w	-2.50	FractInd	5.1565E-03	1.96	3.5(I)	4.9(E) 4.9(A)
137 XE	707	3.0900E-01	9.5	0.00	Ind/Y(A)	3.0900E-01	0.00	9.5(I)	0.0(E) 9.5(A)
138 XE	707	5.1900E-01	8.4	0.00	Ind/Y(A)	5.1900E-01	0.00	8.4(I)	0.0(E) 8.4(A)
CS	788	8.3000E-02	6.0	0.23	FractInd	8.2954E-02	0.05	6.0(I)	1.4(E) 6.0(A)
139 I	789	1.8300E-01	1.0	0.00	FractInd	1.8300E-01	0.00	1.0(I)	0.0(E) 1.0(A)
XE	789	4.7500E-01	2.0	-1.34	FractInd	4.7763E-01	1.80	1.9(I)	2.6(E) 2.6(A)
CS	712	2.8600E-01	5.0	0.00	FractInd	2.8600E-01	0.00	5.0(I)	0.0(E) 5.0(A)
BA	712	5.6000E-02	23.0	0.00	FractInd	5.6000E-02	0.00	23.0(I)	0.0(E) 23.0(A)
140 XE	707	5.4000E-01	8.0	0.00	Ind/Y(A)	5.4000E-01	0.00	8.0(I)	0.0(E) 8.0(A)
LA	30639	9.8600E-03	109.0	0.00	Ind/Y(A)	9.8600E-03	0.00	109.0(I)	0.0(E) 109.0(A)
141 XE	707	2.9100E-01	9.1	0.00	Ind/Y(A)	2.9100E-01	0.00	9.1(I)	0.0(E) 9.1(A)
142 XE	707	1.6400E-01	13.2	0.00	Ind/Y(A)	1.6400E-01	0.00	13.2(I)	0.0(E) 13.2(A)
150 PM	1184	2.3000E-05	30.4	0.00	FractInd	2.3000E-05	0.00	30.4(I)	0.0(E) 30.4(A)

TABLE 24		ENERGY-HIGH		NUCLIDE-PU-239		wt. mean		Chi/df Estimates of Error	
Mass Elem.	Ref.	Yield	N-Res	Type					
133 XE(G)	12895	1.7000E-02	12.4	0.00	FractInd	1.7000E-02	0.00	12.4(I)	0.0(E) 12.4(A)
XE(M)	12895	5.7500E-02	14.1	0.00	FractInd	5.7500E-02	0.00	14.1(I)	0.0(E) 14.1(A)
XE(T)	719	1.2000E-01	9.0	3.27	FractInd	9.2240E-02	10.69	7.2(I)	23.6(E) 23.6(A)
135 XE(G)	12895	1.1700E-01	21.4	0.00	FractInd	1.1700E-01	0.00	21.4(I)	0.0(E) 21.4(A)
XE(M)	12895	3.1700E-01	6.6	0.00	FractInd	3.1700E-01	0.00	6.6(I)	0.0(E) 6.6(A)
XE(T)	12895	4.3400E-01	5.0	-0.67	FractInd	4.4212E-01	0.45	4.1(I)	2.7(E) 4.1(A)
136 CS	13347	1.5100E-01	5.3	-0.39	FractInd	1.5240E-01	0.15	4.7(I)	1.8(E) 4.7(A)
138 I	941	2.7000E-02	10.0	0.00	FractInd	2.7000E-02	0.00	10.0(I)	0.0(E) 10.0(A)
XE	941	4.1500E-01	10.0	0.00	FractInd	4.1500E-01	0.00	10.0(I)	0.0(E) 10.0(A)
CS	941	5.0700E-01	10.0	0.00	FractInd	5.0700E-01	0.00	10.0(I)	0.0(E) 10.0(A)

TABLE 25		ENERGY-HIGH		NUCLIDE-AM-241			
Mass Elem	Ref	Yield	Error	N Res Type	wt. mean	Chi/df	Estimates of Error
86 RB	1154	2.100E-03	100.0	0.00	FractInd 2.100E-03	0.00	100.0(I) 0.0(E)100.0(A)
96 NB	1154	4.740E-03	5.1	0.00	FractInd 4.740E-03	0.00	5.1(I) 0.0(E) 5.1(A)
110 AG(M)	1154	1.200E-03	100.0	0.00	FractInd 1.200E-03	0.00	100.0(I) 0.0(E)100.0(A)
126 SB(G)	1154	2.600E-01	45.0	0.00	FractInd 2.600E-01	0.00	45.0(I) 0.0(E) 45.0(A)
130 I	1154	1.700E-01	5.9	0.00	FractInd 1.700E-01	0.00	5.9(I) 0.0(E) 5.9(A)
132 CS	1154	1.700E-03	11.8	0.00	FractInd 1.700E-03	0.00	11.8(I) 0.0(E) 11.8(A)
134 CS	1154	4.470E-02	6.3	0.00	FractInd 4.470E-02	0.00	6.3(I) 0.0(E) 6.3(A)
136 CS	1154	2.560E-01	5.1	0.00	FractInd 2.560E-01	0.00	5.1(I) 0.0(E) 5.1(A)
160 TS	1154	3.520E-02	5.1	0.00	FractInd 3.520E-02	0.00	5.1(I) 0.0(E) 5.1(A)

TABLE 26		ENERGY-SPONT.		NUCLIDE-CM-244			
Mass Elem	Ref	Yield	Error	N Res Type	wt. mean	Chi/df	Estimates of Error
136 CS	720	1.710E-02	16.2	0.00	Ind/Y(A) 1.710E-02	0.00	16.2(I) 0.0(E) 16.2(A)

TABLE 27		ENERGY.SPONT.		NUCLIDE:CP-252		Chi/df		Estimates of Error	
Mass	Ref.	Yield	Error	N Res	Type	wt.	mean		
86	RB	347	3.4600E-05	23.3	0.00 Ind/Y(A)	3.4600E-05	0.00	23.3(I)	0.0(E) 23.3(A)
111	PD(M)	13357	3.3000E-02	3.0	0.00 FractInd	3.3000E-02	0.00	3.0(I)	0.0(E) 3.0(A)
112	AG	484	9.0000E-03	44.4	0.00 FractInd	9.0000E-03	0.00	44.4(I)	0.0(E) 44.4(A)
131	TE(G)	13301	1.5000E-01	20.0	-1.11 FractInd	1.7773E-01	1.23	9.3(I)	10.4(E) 10.4(A)
		632	1.9000E-01	10.5	1.11 FractInd				
136	TE(M)	632	1.9000E-01	39.5	0.00 FractInd	1.9000E-01	0.00	39.5(I)	0.0(E) 39.5(A)
134	I (G)	1080	1.5900E-01	7.3	0.00 Ind/Y(A)	1.5900E-01	0.00	7.3(I)	0.0(E) 7.3(A)
	I (M)	1080	9.4800E-02	12.2	0.00 Ind/Y(A)	9.4800E-02	0.00	12.2(I)	0.0(E) 12.2(A)
	I (T)	30684	2.6000E-01	11.5	-0.18 FractInd	2.6342E-01	0.02	8.9(I)	1.2(E) 8.9(A)
		21531	2.7000E-01	22.2	0.12 FractInd				
135	XE	30691	8.6000E-02	14.0	-0.06 FractInd	8.6592E-02	0.00	8.9(I)	0.6(E) 8.9(A)
		21531	8.7000E-02	11.5	0.06 FractInd				
136	S	389	8.0000E-02	20.0	0.00 FractInd	1.0000E-02	0.00	20.0(I)	0.0(E) 20.0(A)
138	CS	484	1.1000E-01	27.3	0.00 FractInd	1.1000E-01	0.00	27.3(I)	0.0(E) 27.3(A)
140	CS	40895	7.4000E-01	28.0	0.00 Ind/Y(A)	7.4000E-01	0.00	28.0(I)	0.0(E) 28.0(A)
144	CS	21559	8.9000E-02	10.1	0.00 FractInd	8.9000E-02	0.00	10.1(I)	0.0(E) 10.1(A)
	BA	21559	5.9900E-01	10.0	-0.43 FractInd	6.0962E-01	0.19	9.0(I)	3.9(E) 9.0(A)
		40895	6.6200E-01	20.1	0.43 Ind/Y(A)				
	LA	21559	3.0200E-01	9.9	1.89 FractInd	2.7865E-01	3.56	9.8(I)	18.5(E) 18.5(A)
		40895	1.6500E-01	40.1	-1.89 Ind/Y(A)				
	CE	1066	1.0000E-02	20.0	0.00 FractInd	1.0000E-02	0.00	20.0(I)	0.0(E) 20.0(A)

TABLE 28		ENERGY.SPONT.		NUCLIDE:PK-254		Chi/df		Estimates of Error	
Mass	Ref.	Yield	Error	N Res	Type	wt.	mean		
132	I	758	2.0000E-01	10.0	0.00 FractInd	2.0000E-01	0.00	10.0(I)	0.0(E) 10.0(A)
134	I	758	5.8000E-01	6.9	0.00 FractInd	5.8000E-01	0.00	6.9(I)	0.0(E) 6.9(A)
135	XE(M)	758	2.8000E-01	35.4	0.00 FractInd	2.8000E-01	0.00	35.4(I)	0.0(E) 35.4(A)

TABLE 7 ENERGY-THERMAL NUCLEIDS-Pu-239			
Mass Element	Chi/df	Chi	%probability number of points.
*****	*****	*****	*****
93 KR	8.198	8.198	0.419 2 < 1.5
93 RB	4.279	4.279	3.859 2 < 1.5
95 RB	9.109	9.109	0.254 2 < 1.5
100 TC	1.567	1.567	4.195 4
w104 TC	2.251	6.754	8.077 4
w105 TC	2.930	8.789	3.223 4
128 I	17.159	17.159	0.003 2 < 0.01
w132 SB(M)	3.442	6.884	3.201 3
135 XE(M)	3.707	3.707	5.420 2
135 XE(T)	4.450	4.450	4.950 2
w136 CS(T)	2.334	9.285	5.504 5
138 CS(M)	29.547	29.547	0.000 2 < 0.01
150 PM	37.484	37.484	0.000 2 < 0.01

TABLE 13 ENERGY-FAST NUCLEIDS-TH-232			
Mass Element	Chi/df	Chi	%probability number of points.
*****	*****	*****	*****
w136 CS	3.712	7.424	2.443 3

TABLE 14 ENERGY-FAST NUCLEIDS-U-235			
Mass Element	Chi/df	Chi	%probability number of points.
*****	*****	*****	*****
135 XE(T)	3.559	3.559	5.922 2
w136 CS	4.145	53.886	0.000 14 < 0.01

TABLE 16		ENERGY:FAST		NUCLIDE:U-238	
Mass Element	Chi/df	Chi	%probability number of points.		
w136 CS	6.145	12.291	0.214	3 < 1.5	

TABLE 18		ENERGY:FAST		NUCLIDE:PU-239	
Mass Element	Chi/df	Chi	%probability number of points.		
w136 CS	2.286	13.719	3.294	7	

TABLE 20		ENERGY:HCH		NUCLIDE:TH-232	
Mass Element	Chi/df	Chi	%probability number of points.		
112 AG	2.561	5.122	7.724	3	
136 CS	25.385	25.385	0.000	2 < 0.01	

TABLE 27 ENERGY SPONT. NUCLEI:CE-252
 Mass Element Chi/dt Chi %probability number of points.

 144 LA 3.557 3.557 5.931 2

278. H G PETROM, G ROCCO. (J.PR.96,1614,54)
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FISSION YIELD OF 135MO AND 135I.
279. A C PAPPAS, D R WILES. (J.JIN.2,69,56)
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280_282. A N PROTOPOV, G N TOJACHEV, ET AL. (J.JNEA,10,80,59)
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283. K S ELLAY, R J MEYER, B D LARSEN. (J.NUC.3,233,69)
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284. M W REED. (J.PR.98,1327,55)
285. M W REED, A TURKEVITCH. (J.PR.99,1473,53)
286. M KUMARASEN, H B ANKANA, L J GOLDIN, B V HERSCHER. (J.RAC-TR-2415,)
YIELDS OF VANADIOUS AND CE ISOTOPES IN THE FISSION OF 233U.
287. G R RUNNALLS, D E TROUTNER, R L FERGUSON. (J.PR.179,118,69)
"CHARGE DISTRIBUTION IN FISSION: FRACTIONAL CM. YIELDS OF ETC."
288_290. R B BRADY, M H BURGUS, R S THOMP. (J.PR.113,1569,69)
"RATIO OF ASYMMETRIC TO SYMMETRIC FISSION OF 233U AS A FUNCTION OF NEUTRON ETC."
Early results reported in 51-60.
291_296. R B BRIDGER, M H BURGUS, R L THOMP, B H SURENSEN. (J.PR.119,2017,60)
"RATIO OF ASYMMETRIC TO SYMMETRIC FISSION OF 239PU AND 241PU AS A FUNCTION ETC."
Early results reported in 51-60.
297. R D RICHARD, C F GORING, E I WATTS. (J.NSE.23,115,65) Exfor-13079
"MASS FISSION YIELD CURVE FOR 241AM."
298. N R RAO, P K KURODA. (J.PR.147,884,66)
"DECAY CONSTANT AND MASS YIELD CURVE FOR THE SPONTANEOUS FISSION OF 238U."
299. N R RAO. (J.RCA.8,12,67)
"RADIOCHEMICAL INVESTIGATION OF 238U SPONTANEOUS FISSION."
300. RAVINDRAN, K F FLAVIN, L E GLENDIN. (J.JIN.28,921,66)
"MASS DISTRIBUTION IN THE FISSION OF 239TH."
301. D C SANTRY, L YAFEE. (J.COC.38,464,60)
"THE YIELD OF 140BA IN THE THERMAL FISSION OF 235U."
302. A F STERNER, N STOKMAN. (J.PR.89,194,53)
"CHARACTERISTICS OF 97ER A DELAYED NEUTRON ACTIVITY."
303. N STOKMAN. (J.PR.89,570,53)
"GENETICS OF THE 78ER-78AS FISSION CHAIN."
304. J E SAVITZKIN, J D KNIGHT, M KARR. (J.JIN.12,206,60)
"SHORT LIVED BR AND BE NUCLEIDES FROM FISSION."
305. D C SANTRY, L YAFEE. (J.COC.38,421,60)
"ABSOLUTE THERMAL FISSION YIELDS OF 233U."
306. B SRINIVASAN, E C ALEXANDER, O K MANTEL, D E TROUTNER. (J.PR.179,1166,69)
"XE AND KR FROM SPONTANEOUS FISSION OF 252CF."
307. P O STROM, D L LOVE, A E GHENDALE, A DELUCCI, D SAM, N E BALLOU. (J.PR.144,984,66)
"NUCLEAR CHARGE DISTRIBUTION OF FISSION PRODUCT CHAINS OF MASS MEMBERS 131,133."
308. P O STROM, G R GRANT, A C PAPPAS. (J.COC.43,2493,65)
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309. R OHYOSHI, A OHKOSHI, M SHINGAMA. (J.PRC.3,1,1,70)
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310. R STELLA, L G MORITTO, V MAXIA, M DI OMS, V CRESPI, M A ROLLIER. (J.NUC.12,487,70)
"MASS DISTRIBUTION IN THE FISSION OF 237MP WITH REPLCD NEUTRONS."
311. G D THERON, J A MARINOV. (J.JIN.1129,64)
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312_321. J TERRELL, M E SOWTH, S GILMORE, C O MINKINEN. (J.PR.92,1091,53).
"YIELD OF 99MO FROM FISSION OF 235U AND 238U."
SEE ALSO (J.RAC-1463)
322. A TURKEVITCH, J B MIDAY. (J.PR.84,52,51)
"RADIOCHEMICAL STUDIES ON THE FISSION OF 232TH WITH FILE NEUTRONS."
323. S L TONS, K PRITZER. (J.RCA.12,179,69)
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324. D E TROUTNER, R D FERGUSON, G D O'KELLEY. (J.PR.130,1466,63)
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325_326. G W WETHERILL. (J.PR.92,907,53)
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327_330. D R WILES. (J.PR.96,696,54)
"FISSION YIELD FINE STRUCTURE IN THE MASS REGION 99,106."
331. A C WAHL, N A BONNER. (J.PR.85,570,52)
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332. FOR OTHER VALUES.
333. H V WEISS, N E BALLOU. (C.65SALZBERG,65)
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334. H KOSHIDA, Y PALSS, S AMEL. IA-1128
"DETERMINATION OF IND. YIELDS OF 131I AND 133I IN THERMAL NEUTRON ETC."
335_336. M F ROCHE. (R.TD-24500,)
"THE IND. YIELD OF 112AD AND THE CM. YIELD OF 115PD IN ETC."

337. L R RUNNEY, E M SCUDEN, J O ABRAIM, N E BALLOU. (C.SOVETNA,15,444,58)
"EXTENSION OF THE FISSION PRODUCT REGION AND YIELDS OF HEAVY PRODUCTS ETC."
338_346. C D CORVELL, M STOKMAN
RADIOCHEMICAL STUDIES: THE FISSION PRODUCTS. VOL. 2.
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347. H R GUNTEN, K F FLAVIN, E E GLENDIN. (J.JIN.31,3357,69)
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348_350. D R NETHAWAY, B MEMODA, T E VOISS. (J.PR.182,1251,69)
"LOW YIELD PRODUCTS FROM FISSION OF 237TH, 235U AND 238U WITH 14.8MEV NEUTRONS."
351. M THEIN, M N RAO, P K KURODA. (J.JIN.30,1145,68)
"MASS DISTRIBUTION IN 14.8MEV NEUTRON FISSION OF 232TH."
352. R H JAMES, G R MARTIN, D J SILVESTER. (J.RCA.3,76,64)
"RADIOCHEMICAL STUDIES OF THE FISSION BY 14.7MEV NEUTRONS: PART 1 U."
353. S J LYLE, G R MARTIN, J B WHEATLEY. (J.RCA.3,80,64)
"RADIOCHEMICAL STUDIES OF FISSION BY 14.7MEV NEUTRONS: PART 2 TH."
354. V A VLASOV, YU A YZVIN, I S KIRIN, A L LIOV, L I OSAVAYA, L I SELCHENOV. (J.RAC-TR-4665,)
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355. R GANAPATHY, P K KURODA. (J.JIN.38,2071,66) Also in 609.
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356. H FARAR, R H TOMLINSON. (J.NP.34,367,62)
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357_359. L H GEVARTY, R E JERVIS, H D SHARMA. (J.COC.48,641,70)
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360. M N RAO. (J.JIN.28,921,67)
"CM. YIELDS IN THE 14MEV NEUTRON FISSION OF 232TH AND 238U IN THE ETC."
361_362. M W REED, G BRIDGER, P BRADY, S MOKRZY. (J.JIN.118,69)
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363. D J GORDAN, M TONG, WERNER. (J.COC.66,1663,68)
"CM. YIELDS IN THE 14MEV FISSION OF 238U."
364. J HARVEY, B CLARKE, D GORDAN, R TOMLINSON. (J.COC.46,2911,68)
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365_373. N STOKMAN, S N DUBOVYKH, ET AL. (J.NSP.6,331,68)
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374_377. P RILDER, J P PETERSON, C RUIZ, P R SMITH. GRAP-5356.
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378. R S ONDRZECIN. (J.JIN.38,1763,66)
"THERMAL FISSION YIELD OF 137CS IN 233U."
379. B G YOUNG, H G THODE. (J.CIP.38,1,1,60)
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380. L YAFEE, A E DAY, B A GREER. (J.COC.31,48,53)
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381. L YAFEE, H G THODE, W F MERRITT, R C HAWKINS, P BROWN, AND R M BARFLOHOMEW. (J.COC.32,1077,54)
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382. H V WEISS, J L ELZIE, J M PRESCO. (J.PR.172,1269,68)
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383. L WISH. (J.PR.172,1262,68)
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384. A WITTENBACH, H R VON GUNTEN, H DUKAKAS. (J.RCA.3,118,64)
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385. H V WEISS, N E BALLOU. (J.JIN.27,1917,65)
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386. H V WEISS. (J.PR.139,8304,65)
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387. A C WAHL, D R NETHAWAY. (J.PR.131,830,63)
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388_391. A C WAHL, R L FERGUSON, D R NETHAWAY, D E TROUTNER, K WOLFSBERG.
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392. A C WAHL. (J.JIN.6,243,68)
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393. D M WEISS, J A KERRICK, R M TOMLINSON. (J.COC.44,229,64)
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394. K WOLFSBERG, D R NETHAWAY, B A KAHN, A C WAHL. (J.PR.13,091,60)
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395_397. A C WAHL, G D THERON, J L ELZIE. (J.NSE.23,115,65)
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398_400. D WITTENBACH, B H R VON GUNTEN, H G THOMP. (J.COC.31,419,53)
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401_402. R W. WAINWESS. (J.COC.33,441,55) DATA IN 2H 13389 AND 13391.
"THE FISSION YIELD OF ISOTOPES OF AR AND KR IN THE NEUTRON FISSION OF ETC."
403. D G VALLES, A O THOMAS. AWRB REPORT 0.59/6769
"LIGHT MASS YIELDS IN THE 14MEV NEUTRON FISSION OF 235U."
404. H V WEISS, N E BALLOU, J L ELZIE, J M PRESCO. (J.PR.188,1893,69)
"NUCLEAR CHARGE DISTRIBUTION IN SYMMETRIC FISSION OF 235U WITH THERMAL ETC."

405. S J LYLE, R WELLM. (J.RCA.13,167,70) DATA FROM (J.RCA.3,163,64)
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"SOME CM. MASS YIELDS FROM THE FISSION OF 238U BY 3MEV NEUTRONS."
406_407. L H NICE, D E TROUTNER, R L FERGUSON. (J.PR/C.11,312,70)
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"NUCLEAR CHARGE DISTRIBUTION IN FISSION IND. YIELDS OF 132I, ETC."
408. N R RUNNALLS, D E TROUTNER. (J.PR/C.11,316,70)
"THE ABSOLUTE YIELDS OF SELECTED FISSION ISOTOPES FROM FISSION OF 235U IN DPA."
409. B J KOWLES, H WILKIS, PRIVATE COMMUNICATION.
"THE ABSOLUTE YIELDS OF SELECTED FISSION ISOTOPES FROM FISSION OF 235U IN DPA."
410_411. J BLANCHET, L C CARBAZ, P CAVALLINI, A GAGELLE, A MOUSA. (C.69VIENNA,69)
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412. CHEN-CHANG LIN, A C WAHL. (J.JIN.32,2501,70)
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413_414. E A C CROUCH, M BROWNSHED, I C MCKEAN. PRIVATE COMMUNICATION.
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415_420. B L TRACY. (J.CIP.48,1708,70)
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421_483. A C OWAN, B P BATHURST, J S PRESTWOOD, J S GILMORE, G W KNOBLECH.
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484. D TROUTNER, M BURGUS, G PAGE. (J.PR/C.3,1044,70)
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485. A C WAHL, A R WARD, R A ROUSE, J C WILLIAMS. (C.69VIENNA,69)
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486_553. A C OWAN, B P BATHURST, R S PRESTWOOD, J S GILMORE, G W KNOBLECH.
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554. K BACHMANN. (J.RCA.9,27,68)
555_556. J P BAERG, R M BATHOLOGEN, R H BETTS. (J.COC.38,2147,60)
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557. D E TROUTNER, A C WAHL, R L FERGUSON. (J.PR.134,81027,64)
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558_559. J A MCHUGH. (J.JIN.28,1787,66)
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560. B PANDA, G E GORDON, A WENZEL. (J.JIN.31,585,69)
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561. L TOMLINSON, M H HINDUS. (J.JIN.30,1995,68)
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562_564. J P CHALL. (J.JIN.16,358,61)
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565. D R NETHAWAY, B MEMODA. (J.PR/C.2,2289,70)
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"FISSION OF 233U WITH 14.8MEV NEUTRONS"
566_567. S N QAIN, H O DINSCHLAG. (J.JIN.32,1767,70)
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568_569. K WOLFSBERG, G P FORD, LA-DC-12142 ALSO IN (J.PR/C.3,1333,71)
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570_573. K WOLFSBERG. (J.PR.137,8939,65)
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574_577. R M HARBOUR, D E TROUTNER. (J.JIN.33,1,71)
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578_579. J V KRAVZ, G HERMANN. (J.JIN.32,3713,70)
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580. J KEMNER, J I KIN, H J BORN. (J.RCA.13,181,70)
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581. K WOLFSBERG. (J.JIN.33,587,71)
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582_585. F L LISMAN, R M ABERNETHY, R E FOSTER, W J MARCK. (J.JIN.33,643,71)
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586_587. D L SWINDLE, R O WRIGHT, T E WARD, P K KURODA. (J.JIN.33,651,71)
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588. D L SWINDLE, R J WRIGHT, P K KURODA. (J.JIN.33,876,71)
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589. P K KURODA, M P MENON. (J.NSE.10,70,61) Exfor-13058
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590. P L PARKER, P K KURODA. (J.JIN.5,153,58) Deleted see 589.
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591. F T ASHIZAWA, P K KURODA. (J.JIN.5,12,57) Deleted see 589.
"THE OCCURRENCE OF THE SHORT LIVED I ISOTOPES IN NATURAL AND IN DEPLETED U."
592. H R HEDGECOCK, P K KURODA. (J.JIN.12,12,59) Deleted see 589.
"NATURAL OCCURRENCE OF THE SHORT LIVED BA AND SR ISOTOPES."
593_594. N V SKOVORODIN, ET AL. (J.SRA.12,458,70) TRANS. OF (J.RAC.12,492,70)
"RADIOCHEMICAL DETERMINATION OF THE YIELDS OF RARE EARTH ELEMENTS ETC."
595_596. N V SKOVORODIN, ET AL. (J.SRA.12,453,70) TRANS. OF (J.RAC.12,487,70)
"RADIOCHEMICAL DETERMINATION OF THE YIELDS OF RARE EARTH ELEMENTS ETC."
597. J KEMNER, J I KIN, H J BORN. (J.RCA.15,113,71)
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- 598_599. R. M. HARBOR, M. EICHOR, D. E. TROUTNER, (J. RCA. 35, 1446, 71)
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600. R. DIECKMANN, G. MARACCI, F. RUSTICHELLI, (J. JNE. 25, 85, 71)
"MEASUREMENT OF THE ^{140}La FISSION PRODUCT YIELD FOR FISSION IN ^{238}U ETC."
601. G. E. GORDON, J. M. HARVEY, H. NAKAMURA, (J. NUC. 24, 62, 66)
"REF. PAT. FROM KATCOFF (1960), AND PARFAR AND TOMLINSON (1962).
"MEASURING FISSION SPECTRA WITH SEMICONDUCTOR DETECTORS."
602. S. P. DANKE, H. C. GAIN ET AL., (G. 6VIERNA. 741, 69)
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603. J. FAHLAND, G. LANGE, G. HERMANN, (J. JIN. 32, 3149, 70)
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- 604_607. R. C. HAWKINS, M. J. EDWARDS, W. J. GUNSTEAD, (J. CIP. 49, 745, 71)
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608. M. EICHOR, D. E. TROUTNER, (J. JIN. 33, 1543, 71)
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- 609_610. R. GANNAPATHY, H. HOCHT, (J. JIN. 28, 3071, 66)
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613. R. E. STEINBERG, S. B. GLENNERIN, (J. PR. 95, 431, 64)
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614. T. WATKINSON, G. B. HAY, A. TOMPAINS, (J. PR. 99, 453, 63)
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615. R. G. GARDNER, B. R. JAMES, G. J. PERKIN, (J. JIN. 14, 8, 60)
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616. P. EISENBERG, R. NEW, M. KAMRA ET AL., (J. RCA. 7, 95, 67)
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- 617_618. "COLLECTIVE DETERMINATION OF THE AVERAGE TOTAL KINETIC ENERGY ETC."
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619. Z. KAMANT, G. GOLD, R. GARDNER, S. ROBERTS, (J. NUC. 23, 80, 70)
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- 621_622. S. J. LYLE, G. R. MARTIN, M. RAMANI, (J. RCA. 9, 90, 68)
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- 621_624. J. G. CHINGHANG, J. A. B. GORDALL, H. H. WILLIS, (R. ABER. 6-655, 5)
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- 625_627. J. G. CHINGHANG, J. A. B. GORDALL, H. H. WILLIS, (R. ABER. 6-646, 7, 205)
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628. T. P. MACHUGELIN, UNIV. ARIZONA, (J. NUC. 23, 145, 69)
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- 629_631. H. NAKAMURA, K. FUJIMURA, H. OKAMOTO, M. IMANISHI, T. NISHI, (J. JIN. 33, 2271, 71)
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632. D. E. TROUTNER, N. G. KUNZLIG, (J. JIN. 32, 3271, 71)
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633. DEL MARINO, D. C. BRIDGES, (J. JIN. 32, 704, 70)
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634. L. SPÄHLER, D. M. MOORE, J. N. NEW, D. K. KURODA, (J. JIN. 33, 3643, 71)
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- 635_636. H. O. BRUNSHLAG, S. M. OSM, (J. JIN. 33, 3649, 71)
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637. D. E. ROSE, G. V. SPANNEY, (J. ABER. 2551, 1)
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638. B. NETHANAY, H. B. LEVY, (J. PR. 130, 81505, 65)
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639. A. EISENBERG, V. B. TRIVANATHAN, M. G. PAN YAN, (J. SMO. 11, 654, 70)
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640. N. I. BOLESOVA ET AL., (J. SMO. 6, 404, 69)
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641. D. G. SARANTIDES, G. E. GORDON, C. D. CORVELL, (J. PR. 138, 8353, 65)
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- 642_643. A. V. BACHMANN, H. FRIEDRICH, (J. RCA. 5, 234, 66)
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- 644_645. M. G. BROWN, S. J. LYLE, G. R. MARTIN, (J. RCA. 6, 16, 66)
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- 646_647. A. S. PAO, M. M. BAO, P. K. KURODA, (J. JIN. 31, 591, 69)
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- 648_649. T. MO, P. K. KURODA, (J. JIN. 27, 503, 65)
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650. H. ARINO, P. K. KURODA, (J. JIN. 30, 677, 68)
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- 651_652. M. N. MAMCOWSKI ET AL., (J. JIN. 30, 2305, 68)
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653. L. TOMLINSON, M. H. HURDIS, (J. JIN. 33, 3609, 71)
- 723_724. S. A. BAO, P. K. KURODA, (J. JIN. 35, 1443, 73)
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726. R. C. KAVANATHA, D. K. BHATTACHARYA, (J. JIN. 35, 1794, 73)
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- 727_738. R. L. TRACY, J. P. KEVA, M. G. THORE, (J. JIN. 35, 2639, 73)
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- 739_740. S. L. TONG, K. WHITE, M. V. PRESHYON, (J. JIN. 35, 3079, 73)
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- 741_745. N. V. SKOVORODIN, G. E. LOHOMOV, ET AL., (J. AE. 34, 345, 73)
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- 746_754. M. DUBOVINA, ET AL., (J. PR. 17, 470, 73)
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756. L. R. BATTLES, D. M. CHITTENDEN, (J. JIN. 35, 1075, 73)
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757. K. DEBERTIN, (J. RCA. 18, 202, 72)
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- 758_759. M. HARBOR, K. W. MACHRO, D. E. TROUTNER, M. V. ROSEN, (J. PR. C. 8, 1489, 73)
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- 810_811. M. D. SLABERT, R. H. TOMLINSON, (J. RCA. 5, 223, 66)
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812. J. V. WATKE, ET AL., (J. JIN. 35, 1407, 73)
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- 813_820. M. J. PILES, N. D. JUDY, R. L. WALEWICKI, (J. PR. C. 6, 2252, 73)
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905. A C PAPAS. ((R,MIT-REP-63,53)=(R,AKU-2805,53))
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906. A C PAPAS, P O STROM, L WESTGAARD. (J.JIN,30,89,68)
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907. J BLANCHOT, P CAVALLINI, A FERREU, R LOUIS. (J.UIC,26,107,75)
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- 908_909. C EGGER, H R VONGHENTEN, A SCHMID, H S PRUYS. (J.RCA,21,200,74)
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- 912_913. S J LYLE, J SELLARS. (J.RCA,12,43,69)
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- 921_923. C WAGMANS, A J DERUYTER. (J.ZP/A,275,149,75)
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- 924_925. M RAZAOADAN, ET AL. (J.NSE,58,414,75)
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1080. H ERTEN, O BIRGUL, N K ARAS. (J.JIN,40,183,78)
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- 1081_1085. H GAGELER, H R VONGHENTEN. (J.PR/C,17,172,78)
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A NEW NUCLEIDE, XE-145: MEASUREMENT OF ITS FRACTIONAL	RIDER	73701
CUMULATIVE YIELD FROM THERMAL NEUTRON FISSION OF U-235	REFERENCE	(J JIN 35, 1079, 7309)
13297	AUTHOR	(S. L. YONG, K. PRITZE, M. V. PRESTWICH)
72AE19	TITLE	FISSION OF U-235 IN THE THERMAL AND EPITHERMAL
REFERENCE	ENTRY	13315
(J NE/F, 198, 228, 72)	RIDER	737PA1
(P. ALEXANDER)	REFERENCE	(J JIN 35, 11, 7301)
YIELDS OF 132, 135XE IN THE FISSION OF	AUTHOR	(B. L. TRACY, J. F. KLEVA, H. G. THODE)
235U, 238U, AND 239PU BY 14 MEV NEUTRONS	RIDER	727-738
13298	REFERENCE	(J JIN 35, 9639, 7049)
72AD1	TITLE	CUMULATIVE KRYPTON AND XENON YIELDS FROM THE NEUTRON-
ENTRY	ENTRY	13316
72AF1	RIDER	737B1
760-763.	REFERENCE	(J JIN 35, 11, 7301)
(D. G. ANDERSON)	TITLE	INDUCED FISSION OF 235P, 238P, 241AM, AND 242AM
No data in EXFOR as author feels unknown fractions of	ENTRY	13317
the volatile element yields.	RIDER	74BAL2
FISSION PRODUCT MASS-YIELD MEASUREMENTS FROM INTERMEDIATE	REFERENCE	(J PR/C, 10, 1872, 7411)
ENERGY NEUTRON FISSION OF PLUTONIUM-239 AND PLUTONIUM-241	AUTHOR	(S. J. BALESTRINI, L. PORMANI)
72B1	TITLE	INDUCED FISSION OF 235P, 238P, 241AM, AND 242AM
740.	ENTRY	13318
REFERENCE	RIDER	74B1C1
(T. BECKE, 72) UNIVERSITY OF MISSOURI	REFERENCE	(J PR/C, 10, 1872, 7411)
(L. A. BECKE)	AUTHOR	(S. J. BALESTRINI, L. PORMANI)
NUCLEAR CHARGE DISTRIBUTIONS FOR THE 131 AND 133 MASS CHAINS	TITLE	FISSION-SPECTRUM NEUTRONS
FROM THE THERMAL-NEUTRON INDUCED FISSION OF URANIUM-233.	ENTRY	13319
13301	RIDER	74COW1
(J ACS, (21), 7002) NUCLEAR SECTION 159TH NAT. MEETING	REFERENCE	(J JIN 36, 3880, 7412)
AMERICAN CHEMICAL SOC., HOUSTON, TEXAS	RIDER	74COW1
(K. F. PLYNN, B. SRINIVASAN, O. K. MANUEL, L. E. GLENDENIN)	REFERENCE	(J JIN 36, 3880, 7412)
FRACTIONAL INDEPENDENT AND CUMULATIVE YIELDS OF SOME	TITLE	THE INDEPENDENT YIELD OF 138CS FROM THERMAL-NEUTRON-
PRODUCTS OF SPONTANEOUS FISSION OF 252-CALIFORNIUM	ENTRY	13320
13302	RIDER	74COW1
72FEV2	REFERENCE	(J PR/C, 6, 2211, 7212)
REFERENCE	AUTHOR	(K. F. PLYNN, B. SRINIVASAN, O. K. MANUEL, L. E. GLENDENIN)
(J JIN 34, 1479, 72)	TITLE	SEPARATION OF MASS AND CHARGE IN SPONTANEOUS FISSION
OF 244CM	ENTRY	13307
72331	RIDER	72331
72331	REFERENCE	(J JIN 34, 1479, 72)
678-679.	TITLE	CHARGE DISTRIBUTION IN THE FISSION OF 242C
(J JIN 34, 1479, 72)	ENTRY	13305
72BA01	RIDER	72BA01
REFERENCE	AUTHOR	(S. A. RAO)
(J PR/C, 5, 171, 7201)	TITLE	CHARGE DISTRIBUTION IN THE FISSION OF 242C
13307	ENTRY	13307
72331	RIDER	72331
72331	REFERENCE	(J JIN 34, 801, 72)
674.	TITLE	NUCLEAR CHARGE DISTRIBUTION IN FISSION: FRACTIONAL INDEPENDENT
(J JIN 34, 801, 72)	ENTRY	13308
72MAH1	RIDER	72MAH1
REFERENCE	AUTHOR	(A. C. WAHL, R. DENIG)
(J JIN 34, 2413, 7208)	TITLE	INDUCED FISSION OF 235U
13309	ENTRY	13309
72BA01	RIDER	72BA01
756	REFERENCE	(J JIN 35, 3075, 7309)
(L. R. BATTLES, D. M. CHITTENDEN)	TITLE	YIELDS OF LOW MASS PRODUCTS IN THE FISSION OF 232TH BY
14.8 MEV NEUTRONS	ENTRY	13310
13310	RIDER	72331
72331	REFERENCE	(J JIN 35, 3075, 7309)
72331	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13311
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13312
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13313
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13314
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13315
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13316
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13317
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13318
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13319
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13320
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13321
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13322
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13323
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13324
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13325
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13326
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13327
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13328
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13329
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13330
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13331
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13332
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13333
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13334
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13335
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13336
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13337
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13338
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13339
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13340
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13341
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13342
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13343
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13344
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13345
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13346
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13347
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13348
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13349
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13350
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13351
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13352
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13353
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13354
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13355
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13356
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13357
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13358
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13359
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13360
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13361
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13362
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13363
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13364
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13365
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13366
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13367
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13368
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13369
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM	ENTRY	13370
73K1K1	RIDER	73K1K1
73K1K1	REFERENCE	(J JIN 35, 3075, 7309)
73K1K1	TITLE	MASS AND NUCLEAR CHARGE DISTRIBUTIONS FROM SPONTANEOUS
FISSION OF 254FM		

13429	ENTRY	13429	0	13429	REFERENCE	(J.P.R.C. 2, 615, 7008)
569111	RIDER	569111	0	569111	AUTHOR	(G.A. COWAN, B.P. BAYHURST, R.J. PRESTWOOD, J.S. GILMORE, G.M. KNEBELSCH)
13430	REFERENCE	(J.C.C. 34, 327, 5603)		13430	NOTE	MEASURED RELATIVE YIELD RATIOS AT DIFFERENT ENERGIES SEPARATED BY FEW -eV (IN RANGE 19 TO 86 eV)
13431	AUTHOR	(D.M. WILKES, J.A. PETRUSKA, R.H. TOMLINSON)		13431	TITLE	SYMMETRY OF NEUTRON-INDUCED 235U FISSION AT INDIVIDUAL RESONANCES
13432	AUTHOR	(S. KATCOFF, B. FINKLE, N. SUGARMAN)		13432	ENTRY	13452 0
13433	TITLE	FISSION YIELD OF 88M BA39		13433	AUTHOR	(J.D. KNIGHT, D.C. HOFFMAN, B.J. DROPSKY, D.L. PRASCO)
13434	REFERENCE	(B.R.C. 2, 944(131), 51)		13434	TITLE	RADIATIONS OF 93F AND 94F AND HALF-LIVES OF 93SR AND 94SR
13435	AUTHOR	(G.R. LEADER, W.H. SULLIVAN)		13435	ENTRY	13453 900220
13436	TITLE	STUDY OF LONG-LIVED ANTIMONY IN FISSION (II)		13436	REFERENCE	(J.P.R. 107, 325, 5707)
13437	REFERENCE	(B.R.C. 2, 905(128), 51)		13437	AUTHOR	(B.P. BAYHURST, C.I. BROWNE, G.P. FORD, J.S. GILMORE, R.P. METCALF)
13438	AUTHOR	(R.P. METCALF)		13438	TITLE	RESONANCE FISSION IN U235
13439	TITLE	CD117 AND 11117: HALF-LIVES, RADIATIONS, AND FISSION YIELD		13439	ENTRY	13454 0
13440	REFERENCE	(B.R.C. 2, 860(119), 51)		13440	AUTHOR	(J.P.R. 5, 1725, 7205)
13441	AUTHOR	(J.A. SELLER)		13441	TITLE	DISTRIBUTION OF MASS IN THE SPONTANEOUS FISSION OF 256PM
13442	TITLE	PALLADIUM - SILVER CHAINS IN FISSION		13442	AUTHOR	(K.K. SOLOMON, F.R. FIELDS, L.E. GLENDENIN)
13443	REFERENCE	(B.R.C. 2, 910(129), 51)		13443	ENTRY	13455 0
13444	AUTHOR	(J.A. SELLER)		13444	ENTRY	218 0
13445	TITLE	SN ISOTOPES (80MIN, 62H, AND 10D) IN FISSION		13445	REFERENCE	(J.P.R. 1, 45, 5583)
13446	REFERENCE	(B.R.C. 2, 549(51), 51)		13446	TITLE	FISSION YIELDS IN SPONTANEOUS FISSION OF CP252
13447	AUTHOR	(J.M. SIEGEL, E. GLENDENIN)		13447	ENTRY	918 0
13448	TITLE	ZINC AND GALLIUM ACTIVITIES IN FISSION		13448	REFERENCE	(J.P.R. 6, 12, 178, 7811)
13449	REFERENCE	(B.R.C. 2, 947(134), 51)		13449	AUTHOR	(K.F. PLANN, J.E. GIEGLER, L.E. GLENDENIN)
13450	AUTHOR	(C. MONTAGNOLI, E. GLENDENIN)		13450	TITLE	DISTRIBUTION OF MASS IN THERMAL-NEUTRON-INDUCED FISSION
13451	TITLE	A LONG-LIVED ANTIMONY ACTIVITY IN URANIUM FISSION		13451	ENTRY	13457 0
13452	REFERENCE	(B.R.C. 2, 566(94), 51)		13452	AUTHOR	(M.C. INGRAM, D.C. BESS, JR, J.H. REYNOLDS)
13453	AUTHOR	(P.C. FREEDMAN, J. ENKELMEIER)		13453	TITLE	ON THE RELATIVE YIELDS OF FISSION CESIUM ISOTOPES
13454	TITLE	SHORT-LIVED GERMANIUM AND ARSENIC FISSION ACTIVITIES		13454	ENTRY	13459 0
13455	REFERENCE	(W. STEINBERG, 51)		13455	REFERENCE	(J.P.R. 108, 1452, 5712)
13456	AUTHOR	(W. STEINBERG)		13456	TITLE	MASS DISTRIBUTION OF U235 BY RESONANCE NEUTRONS
13457	REFERENCE	(P.C. 2310, 201, 4501)		13457	ENTRY	13460 0
13458	TITLE	INDEPENDENT FISSION YIELD OF 40H LA140 IN FISSION		13458	REFERENCE	(J.P.R. 108, 1452, 5712)
13459	REFERENCE	(P.C. 2310, 201, 4501)		13459	AUTHOR	(G.A. COWAN, B.P. BAYHURST, R.J. PRESTWOOD, J.S. GILMORE, J.S. KNEBELSCH)
13460	AUTHOR	(N. SUGARMAN)		13460	TITLE	A NEW FISSION PRODUCT: 74GA
13461	TITLE	INDEPENDENT FISSION YIELD OF 40H LA140 IN FISSION		13461	ENTRY	53941 0
13462	REFERENCE	(R.C. 1493, 4403)		13462	RIDER	53941 0
13463	AUTHOR	(W.H. SULLIVAN, N. R. SLEIGHT, E.M. GLADRON)		13463	REFERENCE	(R.MIT-REP-63, 53)=(R. ACQU-2806, 53))
13464	TITLE	RADIOACTIVITIES OF ARSENIC AND RADIUM		13464	AUTHOR	(A.C. PAPAPAS)
13465	ENTRY	13422 0		13465	TITLE	STUDY OF FISSION YIELDS IN THE REGION OF SHELL PERTURBATIONS AND THE EFFECT OF CLOSED SHELLS IN FISSION
13466	REFERENCE	(L. WINBERG)		13466	ENTRY	13464 0
13467	AUTHOR	(L. WINBERG)		13467	REFERENCE	(R. LA-6129, 7602) DATA COMPILED
13468	TITLE	STUDY OF 25M SM155 IN FISSION		13468	AUTHOR	(G.P. FORD, A.E. NORRIS)
13469	REFERENCE	(B.R.C. 2, 1292(197), 51)		13469	TITLE	THE INDEPENDENT YIELD OF XE135 PRODUCED IN THE FISSION OF NATURAL URANIUM BY FIVE NEUTRONS
13470	AUTHOR	(L. WINBERG)		13470	ENTRY	13465 0
13471	TITLE	STUDY OF 60M EU156 AND 15.4H EU157 ACTIVITIES IN FISSION		13471	REFERENCE	(R.MIT-LNS-PR-38, 5508)
13472	REFERENCE	(L. WINBERG)		13472	TITLE	NOT GIVEN
13473	AUTHOR	(L. WINBERG)		13473	ENTRY	13467 0
13474	TITLE	STUDY OF THE FISSION CHAIN 10H SM156 - 15.4D EU156		13474	REFERENCE	(JACS, (211, 7404) NUCLEAR CHEM. AND TECHNOLOGY DIV. AMERICAN CHEM. SOC. NATIONAL MEETING, LOS ANGELES
13475	ENTRY	174-176		13475	AUTHOR	(H.R. HATVEGER, P.K. KURODA)
13476	REFERENCE	(S. KATCOFF, W. RUBINSON)		13476	TITLE	NATURAL OCCURRENCE OF THE SHORT-LIVED BARIUM AND STRONTIUM ISOTOPES
13477	AUTHOR	(D.M. ENKELMEIER, M.S. FREEDMAN, E.P. STEINBERG, J.A. SELLER, L. WINBERG)		13477	ENTRY	13471 0
13478	TITLE	DATA IN 13396		13478	REFERENCE	(J.P.R. 1, 45, 5583)
13479	REFERENCE	(B.R.C. 1997, 5602)		13479	AUTHOR	(J.P.R. 107, 325, 5707)
13480	AUTHOR	(R. LA-6129, 7602) DATA COMPILED		13480	TITLE	MASS YIELDS FROM SPONTANEOUS FISSION OF 254CF
13481	TITLE	MASS YIELDS FROM FISSION BY NEUTRONS BETWEEN THERMAL AND 14.7 MEV		13481	ENTRY	59891 0
13482	REFERENCE	(S. KATCOFF, W. RUBINSON)		13482	REFERENCE	(J.P.R. 5, 1725, 7205)
13483	AUTHOR	(G.P. FORD, J.S. GILMORE)		13483	TITLE	DISTRIBUTION OF MASS IN THE SPONTANEOUS FISSION OF 256PM
13484	TITLE	MASS YIELDS FROM FISSION BY NEUTRONS BETWEEN THERMAL AND 14.7 MEV		13484	ENTRY	59891 0
13485	REFERENCE	(S. KATCOFF, W. RUBINSON)		13485	REFERENCE	(J.P.R. 5, 1725, 7205)
13486	AUTHOR	(G.P. FORD, J.S. GILMORE)		13486	TITLE	DISTRIBUTION OF MASS IN THE SPONTANEOUS FISSION OF 256PM
13487	TITLE	MASS YIELDS FROM FISSION BY NEUTRONS BETWEEN THERMAL AND 14.7 MEV		13487	ENTRY	59891 0
13488	REFERENCE	(S. KATCOFF, W. RUBINSON)		13488	REFERENCE	(J.P.R. 5, 1725, 7205)
13489	AUTHOR	(G.P. FORD, J.S. GILMORE)		13489	TITLE	DISTRIBUTION OF MASS IN THE SPONTANEOUS FISSION OF 256PM
13490	TITLE	MASS YIELDS FROM FISSION BY NEUTRONS BETWEEN THERMAL AND 14.7 MEV		13490	ENTRY	59891 0
13491	REFERENCE	(S. KATCOFF, W. RUBINSON)		13491	REFERENCE	(J.P.R. 5, 1725, 7205)
13492	AUTHOR	(G.P. FORD, J.S. GILMORE)		13492	TITLE	DISTRIBUTION OF MASS IN THE SPONTANEOUS FISSION OF 256PM
13493	TITLE	MASS YIELDS FROM FISSION BY NEUTRONS BETWEEN THERMAL AND 14.7 MEV		13493	ENTRY	59891 0
13494	REFERENCE	(S. KATCOFF, W. RUBINSON)		13494	REFERENCE	(J.P.R. 5, 1725, 7205)
13495	AUTHOR	(G.P. FORD, J.S. GILMORE)		13495	TITLE	DISTRIBUTION OF MASS IN THE SPONTANEOUS FISSION OF 256PM
13496	TITLE	MASS YIELDS FROM FISSION BY NEUTRONS BETWEEN THERMAL AND 14.7 MEV		13496	ENTRY	59891 0
13497	REFERENCE	(S. KATCOFF, W. RUBINSON)		13497	REFERENCE	(J.P.R. 5, 1725, 7205)
13498	AUTHOR	(G.P. FORD, J.S. GILMORE)		13498	TITLE	DISTRIBUTION OF MASS IN THE SPONTANEOUS FISSION OF 256PM
13499	TITLE	MASS YIELDS FROM FISSION BY NEUTRONS BETWEEN THERMAL AND 14.7 MEV		13499	ENTRY	59891 0
13500	REFERENCE	(S. KATCOFF, W. RUBINSON)		13500	REFERENCE	(J.P.R. 5, 1725, 7205)
13501	AUTHOR	(G.P. FORD, J.S. GILMORE)		13501	TITLE	DISTRIBUTION OF MASS IN THE SPONTANEOUS FISSION OF 256PM
13502	TITLE	MASS YIELDS FROM FISSION BY NEUTRONS BETWEEN THERMAL AND 14.7 MEV		13502	ENTRY	59891 0
13503	REFERENCE	(S. KATCOFF, W. RUBINSON)		13503	REFERENCE	(J.P.R. 5, 1725, 7205)
13504	AUTHOR	(G.P. FORD, J.S. GILMORE)		13504	TITLE	DISTRIBUTION OF MASS IN THE SPONTANEOUS FISSION OF 256PM
13505	TITLE	MASS YIELDS FROM FISSION BY NEUTRONS BETWEEN THERMAL AND 14.7 MEV		13505	ENTRY	59891 0
13506	REFERENCE	(S. KATCOFF, W. RUBINSON)		13506	REFERENCE	(J.P.R. 5, 1725, 7205)
13507	AUTHOR	(G.P. FORD, J.S. GILMORE)		13507	TITLE	DISTRIBUTION OF MASS IN THE SPONTANEOUS FISSION OF 256PM
13508	TITLE	MASS YIELDS FROM FISSION BY NEUTRONS BETWEEN THERMAL AND 14.7 MEV		13508	ENTRY	59891 0
13509	REFERENCE	(S. KATCOFF, W. RUBINSON)		13509	REFERENCE	(J.P.R. 5, 1725, 7205)
13510	AUTHOR	(G.P. FORD, J.S. GILMORE)		13510	TITLE	DISTRIBUTION OF MASS IN THE SPONTANEOUS FISSION OF 256PM
13511	TITLE	MASS YIELDS FROM FISSION BY NEUTRONS BETWEEN THERMAL AND 14.7 MEV		13511	ENTRY	59891 0
13512	REFERENCE	(S. KATCOFF, W. RUBINSON)		13512	REFERENCE	(J.P.R. 5, 1725, 7205)
13513	AUTHOR	(G.P. FORD, J.S. GILMORE)		13513	TITLE	DISTRIBUTION OF MASS IN THE SPONTANEOUS FISSION OF 256PM
13514	TITLE	MASS YIELDS FROM FISSION BY NEUTRONS BETWEEN THERMAL AND 14.7 MEV		13514	ENTRY	59891 0
13515	REFERENCE	(S. KATCOFF, W. RUBINSON)		13515	REFERENCE	(J.P.R. 5, 1725, 7205)
13516	AUTHOR	(G.P. FORD, J.S. GILMORE)		13516	TITLE	DISTRIBUTION OF MASS IN THE SPONTANEOUS FISSION OF 256PM
13517	TITLE	MASS YIELDS FROM FISSION BY NEUTRONS BETWEEN THERMAL AND 14.7 MEV		13517	ENTRY	59891 0
13518	REFERENCE	(S. KATCOFF, W. RUBINSON)		13518	REFERENCE	(J.P.R. 5, 1725, 7205)
13519	AUTHOR	(G.P. FORD, J.S. GILMORE)		13519	TITLE	DISTRIBUTION OF MASS IN THE SPONTANEOUS FISSION OF 256PM
13520	TITLE	MASS YIELDS FROM FISSION BY NEUTRONS BETWEEN THERMAL AND 14.7 MEV		13520	ENTRY	59891 0
13521	REFERENCE	(S. KATCOFF, W. RUBINSON)		13521	REFERENCE	(J.P.R. 5, 1725, 7205)
13522	AUTHOR	(G.P. FORD, J.S. GILMORE)		13522	TITLE	DISTRIBUTION OF MASS IN THE SPONTANEOUS FISSION OF 256PM
13523	TITLE	MASS YIELDS FROM FISSION BY NEUTRONS BETWEEN THERMAL AND 14.7 MEV		13523	ENTRY	59891 0
13524	REFERENCE	(S. KATCOFF, W. RUBINSON)		13524	REFERENCE	(J.P.R. 5, 1725, 7205)
13525	AUTHOR	(G.P. FORD, J.S. GILMORE)		13525	TITLE	DISTRIBUTION OF MASS IN THE SPONTANEOUS FISSION OF 256PM
13526	TITLE	MASS YIELDS FROM FISSION BY NEUTRONS BETWEEN THERMAL AND 14.7 MEV		13526	ENTRY	59891 0
13527	REFERENCE	(S. KATCOFF, W. RUBINSON)		13527	REFERENCE	(J.P.R. 5, 1725, 7205)
13528	AUTHOR	(G.P. FORD, J.S. GILMORE)		13528	TITLE	DISTRIBUTION OF MASS IN THE SPONTANEOUS FISSION OF 256PM
13529	TITLE	MASS YIELDS FROM FISSION BY NEUTRONS BETWEEN THERMAL AND 14.7 MEV		13529	ENTRY	59891 0
13530	REFERENCE	(S. KATCOFF, W. RUBINSON)		13530	REFERENCE	(J.P.R. 5, 1725, 7205)
13531	AUTHOR	(G.P. FORD, J.S. GILMORE)		13531	TITLE	DISTRIBUTION OF MASS IN THE SPONTANEOUS FISSION OF 256PM
13532	TITLE	MASS YIELDS FROM FISSION BY NEUTRONS BETWEEN THERMAL AND 14.7 MEV		13532	ENTRY	59891 0
13533	REFERENCE	(S. KATCOFF, W. RUBINSON)		13533	REFERENCE	(J.P.R. 5, 1725, 7205)
13534	AUTHOR	(G.P. FORD, J.S. GILMORE)		13534	TITLE	DISTRIBUTION OF MASS IN THE SPONTANEOUS FISSION OF 256PM
13535	TITLE	MASS YIELDS FROM FISSION BY NEUTRONS BETWEEN THERMAL AND 14.7 MEV		13535	ENTRY	59891 0
13536	REFERENCE	(S. KATCOFF, W. RUBINSON)		13536	REFERENCE	(J.P.R. 5, 1725, 7205)
13537	AUTHOR	(G.P. FORD, J.S. GILMORE)		13537	TITLE	DISTRIBUTION OF MASS IN THE SPONTANEOUS FISSION OF 256PM
13538	TITLE	MASS YIELDS FROM FISSION BY NEUTRONS BETWEEN THERMAL AND 14.7 MEV		13538	ENTRY	59891 0
13539	REFERENCE	(S. KATCOFF, W. RUBINSON)		13539	REFERENCE	(J.P.R. 5, 1725, 7205)
13540	AUTHOR	(G.P. FORD, J.S. GILMORE)		13540	TITLE	DISTRIBUTION OF MASS IN THE SPONTANEOUS FISSION OF 256PM
13541	TITLE	MASS YIELDS FROM FISSION BY NEUTRONS BETWEEN THERMAL AND 14.7 MEV		13541	ENTRY	59891 0
13542	REFERENCE	(S. KATCOFF, W. RUBINSON)		13542	REFERENCE	(J.P.R. 5, 1725, 7205)
13543	AUTHOR	(G.P. FORD, J.S. GILMORE)		13543	TITLE	DISTRIBUTION OF MASS IN THE SPONTANEOUS FISSION OF 256PM
13544	TITLE	MASS YIELDS FROM FISSION BY NEUTRONS BETWEEN THERMAL AND 14.7 MEV		13544	ENTRY	59891 0
13545	REFERENCE	(S. KATCOFF, W. RUBINSON)		13545	REFERENCE	(J.P.R. 5, 1725, 7205)
13546	AUTHOR	(G.P. FORD, J.S. GILMORE)		13546	TITLE	DISTRIBUTION OF MASS IN THE SPONTANEOUS FISSION OF 256PM
13547	TITLE	MASS YIELDS FROM FISSION BY NEUTRONS BETWEEN THERMAL AND 14.7 MEV		13547	ENTRY	59891 0
13548	REFERENCE	(S. KATCOFF, W. RUBINSON)		13548	REFERENCE	(J.P.R. 5, 1725, 7205)
13549	AUTHOR	(G.P. FORD, J.S. GILMORE)		13549	TITLE	DISTRIBUTION OF MASS IN THE SPONTANEOUS FISSION OF 256PM
13550	TITLE	MASS YIELDS FROM FISSION BY NEUTRONS BETWEEN THERMAL AND 14.7 MEV		13550	ENTRY	59891 0
13551	REFERENCE	(S. KATCOFF, W. RUBINSON)		13551	REFERENCE	(J.P.R. 5, 1725, 7205)
13552	AUTHOR	(G.P. FORD, J.S. GILMORE)		13552	TITLE	DISTRIBUTION OF MASS IN THE SPONTANEOUS FISSION OF 256PM
13553	TITLE	MASS YIELDS FROM FISSION BY NEUTRONS BETWEEN THERMAL AND 14.7 MEV		13553	ENTRY	59891 0
13554	REFERENCE	(S. KATCOFF, W. RUBINSON)		13554	REFERENCE	(J.P.R. 5, 1725, 7205)
13555	AUTHOR	(G.P. FORD, J.S. GILMORE)		13555	TITLE	DISTRIBUTION OF MASS IN THE SPONTANEOUS FISSION OF 256PM
13556	TITLE	MASS YIELDS FROM FISSION BY NEUTRONS BETWEEN THERMAL AND 14.7 MEV		13556	ENTRY	59891 0
13557	REFERENCE	(S. KATCOFF, W. RUBINSON)		13557	REFERENCE	(J.P.R. 5, 1725, 7205)
13558	AUTHOR	(G.P. FORD, J.S. GILMORE)		13558	TITLE	DISTRIBUTION OF MASS IN THE SPONTANEOUS FISSION OF 256PM
13559	TITLE	MASS YIELDS FROM FISSION BY NEUTRONS BETWEEN THERMAL AND 14.7 MEV		13559	ENTRY	59891 0
13560	REFERENCE	(S. KATCOFF, W. RUBINSON)		13560	REFERENCE	(J.P.R. 5, 1725, 7205)
13561	AUTHOR	(G.P. FORD, J.S. GILMORE)		13561	TITLE	DISTRIBUTION OF MASS IN THE SPONTANEOUS FISSION OF 256PM
13562	TITLE	MASS YIELDS FROM FISSION BY NEUTRONS BETWEEN THERMAL AND 14.7 MEV		13562	ENTRY	59891 0
13563	REFERENCE	(S. KATCOFF, W. RUBINSON)		13563	REFERENCE	(J.P.R. 5, 1725, 7205)
13564	AUTHOR	(G.P. FORD, J.S. GILMORE)		13564	TITLE	DISTRIBUTION OF MASS IN THE SPONTANEOUS FISSION OF 256PM
13565	TITLE	MASS YIELDS FROM FISSION BY NEUTRONS BETWEEN THERMAL AND 14.7 MEV		13565	ENTRY	59891 0
13566	REFERENCE	(S. KATCOFF, W. RUBINSON)		13566	REFERENCE	(J.P.R. 5, 1725, 7205)
13567	AUTHOR	(G.P. FORD, J.S. GILMORE)		13567	TITLE	DISTRIBUTION OF MASS IN THE SPONTANEOUS FISSION OF 256PM
13568	TITLE	MASS YIELDS FROM FISSION BY NEUTRONS BETWEEN THERMAL AND 14.7 MEV		13568	ENTRY	59891 0
13569	REFERENCE	(S. KATCOFF, W. RUBINSON)		13569	REFERENCE	(J.P.R. 5, 1725, 7205)
13570	AUTHOR	(G.P. FORD, J.S. GILMORE)		13570	TITLE	DISTRIBUTION OF MASS IN THE SPONTANEOUS FISSION OF 256PM
13571	TITLE	MASS YIELDS FROM FISSION BY NEUTRONS BETWEEN THERMAL AND 14.7 MEV		13571	ENTRY	59891 0
13572	REFERENCE	(S. KATCOFF, W. RUBINSON)		13572	REFERENCE	(J.P.R. 5, 1725, 7205)
13573	AUTHOR	(G.P. FORD, J.S. GILMORE)		13573	TITLE	DISTRIBUTION OF MASS IN THE SPONTANEOUS FISSION OF 256PM
13574	TITLE	MASS YIELDS FROM FISSION BY NEUTRONS BETWEEN THERMAL AND 14.7 MEV		13574	ENTRY	59891 0
13575	REFERENCE	(S. KATCOFF, W. RUBINSON)		13575	REFERENCE	(J.P.R. 5, 1725, 7205)

[illegible]

REFERENCE TITLE	(J.YF.13.(1).484.71) EFFECT OF EXCITATION ENERGY ON YIELDS AND KINETIC ENERGIES OF FRAGMENTS AT THE FISSION OF PU-239 BY NEUTRONS.	TITLE	MASS YIELDS AND KINETIC ENERGY OF FRAGMENTS FOR FISSION OF PLUTONIUM ISOTOPES	REFERENCE TITLE	(J.YF.1.150.48.8303) DETERMINATION OF NP-237 FISSION YIELDS BY NEUTRONS OF FAST REACTOR CORE SPECTRUM USING GAMMA-SPECTROMETRIC METHOD
ENTRY AUTHOR	40145 (J.YF.11.(2).297.7002) V.A.PCHELIN,L.V.CHESTIAKOV,V.I.MYCHOMOTSEVA,	ENTRY AUTHOR	40293 (V.A.KOROSTYLEV,D.K.KUZANOV,V.A.SAFONOV)	ENTRY AUTHOR	40178 (J.YF.10.(1).64.8031) A.B.KOLODINSKI,JU.F.KOLODNOV,V.M.KOLODASHKIN,
REFERENCE TITLE	(J.YF.14.(5).7443.71) THE FISSION PRODUCTS FROM CP-249 EXPOSED TO SLOW NEUTRONS	REFERENCE TITLE	40163 (J.YF.3.(7).11.5707) I.A.KONSHAKOV,B.O.IVANKO,S.M.KUKAVAZIDE, I.A.KONSHAKOV	REFERENCE TITLE	40179 (J.YF.10.(1).64.8031) A.B.KOLODINSKI,JU.F.KOLODNOV,V.M.KOLODASHKIN,
ENTRY AUTHOR	40172 (B.D.KUZ'MINOV,A.I.SERGACHEV,L.D.SNIEKINA)	ENTRY AUTHOR	40172 (B.D.KUZ'MINOV,A.I.SERGACHEV,L.D.SNIEKINA)	ENTRY AUTHOR	40180 (J.YF.10.(1).64.8031) A.B.KOLODINSKI,JU.F.KOLODNOV,V.M.KOLODASHKIN,
REFERENCE TITLE	(J.YF.11.(2).297.7002) FISSION OF FRAGMENTS AT THE FISSION OF NP-237 BY NEUTRONS	REFERENCE TITLE	40173 (A.I.SERGACHEV,V.G.VOROB'YEV,B.D.KUZ'MINOV, V.B.MITROPOV,M.Z.TARASKO)	REFERENCE TITLE	40181 (J.YF.10.(1).64.8031) A.B.KOLODINSKI,JU.F.KOLODNOV,V.M.KOLODASHKIN,
ENTRY AUTHOR	40173 (A.I.SERGACHEV,V.G.VOROB'YEV,B.D.KUZ'MINOV, V.B.MITROPOV,M.Z.TARASKO)	ENTRY AUTHOR	40173 (A.I.SERGACHEV,V.G.VOROB'YEV,B.D.KUZ'MINOV, V.B.MITROPOV,M.Z.TARASKO)	REFERENCE TITLE	40182 (J.YF.10.(1).64.8031) A.B.KOLODINSKI,JU.F.KOLODNOV,V.M.KOLODASHKIN,
REFERENCE TITLE	NUCLEI TH-232 ON MASS AND KINETIC ENERGY DISTRIBUTIONS OF FRAGMENTS	REFERENCE TITLE	40176 (J.YF.15.(1).22.7201) L.Z.MALKIN,K.A.PETZHAH,V.I.SHEKOV	REFERENCE TITLE	40183 (J.YF.10.(1).64.8031) A.B.KOLODINSKI,JU.F.KOLODNOV,V.M.KOLODASHKIN,
ENTRY AUTHOR	40176 (J.YF.15.(1).22.7201) L.Z.MALKIN,K.A.PETZHAH,V.I.SHEKOV	ENTRY AUTHOR	40176 (J.YF.15.(1).22.7201) L.Z.MALKIN,K.A.PETZHAH,V.I.SHEKOV	REFERENCE TITLE	40184 (J.YF.10.(1).64.8031) A.B.KOLODINSKI,JU.F.KOLODNOV,V.M.KOLODASHKIN,
REFERENCE TITLE	FRAGMENT YIELDS AND KINETIC ENERGY OF FISSION OF URANIUM-235	REFERENCE TITLE	40177 (J.YF.11.(2).297.7002) V.A.PCHELIN,L.V.CHESTIAKOV,V.I.MYCHOMOTSEVA,	REFERENCE TITLE	40185 (J.YF.10.(1).64.8031) A.B.KOLODINSKI,JU.F.KOLODNOV,V.M.KOLODASHKIN,
ENTRY AUTHOR	40177 (J.YF.11.(2).297.7002) V.A.PCHELIN,L.V.CHESTIAKOV,V.I.MYCHOMOTSEVA,	ENTRY AUTHOR	40177 (J.YF.11.(2).297.7002) V.A.PCHELIN,L.V.CHESTIAKOV,V.I.MYCHOMOTSEVA,	REFERENCE TITLE	40186 (J.YF.10.(1).64.8031) A.B.KOLODINSKI,JU.F.KOLODNOV,V.M.KOLODASHKIN,
REFERENCE TITLE	ONLY STATISTICAL ERRORS GIVEN 3-16%, THEREFORE YIELDS AND KINETIC ENERGIES OF FISSION FRAGMENTS BY SPONTANEOUS AND INDUCED FISSION OF PU-242	REFERENCE TITLE	40178 (J.YF.11.(2).297.7002) V.A.PCHELIN,L.V.CHESTIAKOV,V.I.MYCHOMOTSEVA,	REFERENCE TITLE	40187 (J.YF.10.(1).64.8031) A.B.KOLODINSKI,JU.F.KOLODNOV,V.M.KOLODASHKIN,
ENTRY AUTHOR	40200 (J.YF.16.(4).649.72) V.F.ZARAROVA,D.K.KUZANOV,B.G.BASOVA,A.D.RABINOVICH,	ENTRY AUTHOR	40178 (J.YF.11.(2).297.7002) V.A.PCHELIN,L.V.CHESTIAKOV,V.I.MYCHOMOTSEVA,	REFERENCE TITLE	40188 (J.YF.10.(1).64.8031) A.B.KOLODINSKI,JU.F.KOLODNOV,V.M.KOLODASHKIN,
REFERENCE TITLE	INVESTIGATION OF URANIUM-235 FISSION BY THE THERMAL NEUTRONS	REFERENCE TITLE	40179 (J.YF.11.(2).297.7002) V.A.PCHELIN,L.V.CHESTIAKOV,V.I.MYCHOMOTSEVA,	REFERENCE TITLE	40189 (J.YF.10.(1).64.8031) A.B.KOLODINSKI,JU.F.KOLODNOV,V.M.KOLODASHKIN,
ENTRY AUTHOR	40205 (M.V.SHOVOROKIN,G.E.LOZHOMOEY,K.A.PETZHAH, V.F.ZARAROVA,D.K.KUZANOV,B.G.BASOVA,A.D.RABINOVICH)	ENTRY AUTHOR	40179 (J.YF.11.(2).297.7002) V.A.PCHELIN,L.V.CHESTIAKOV,V.I.MYCHOMOTSEVA,	REFERENCE TITLE	40190 (J.YF.10.(1).64.8031) A.B.KOLODINSKI,JU.F.KOLODNOV,V.M.KOLODASHKIN,
REFERENCE TITLE	FRAGMENTS YIELDS OF CP-252 SPONTANEOUS FISSION	REFERENCE TITLE	40180 (J.YF.11.(2).297.7002) V.A.PCHELIN,L.V.CHESTIAKOV,V.I.MYCHOMOTSEVA,	REFERENCE TITLE	40191 (J.YF.10.(1).64.8031) A.B.KOLODINSKI,JU.F.KOLODNOV,V.M.KOLODASHKIN,
ENTRY AUTHOR	40206 (L.N.JUROVA,A.V.BUSHUEV,V.O.OZERKIN,V.I.KOZIN)	ENTRY AUTHOR	40180 (J.YF.11.(2).297.7002) V.A.PCHELIN,L.V.CHESTIAKOV,V.I.MYCHOMOTSEVA,	REFERENCE TITLE	40192 (J.YF.10.(1).64.8031) A.B.KOLODINSKI,JU.F.KOLODNOV,V.M.KOLODASHKIN,
REFERENCE TITLE	YIELD DEPENDENT OF SOME FRAGMENTS IN U-238 FISSION BY NEUTRONS OF REACTOR SPECTRUM	REFERENCE TITLE	40181 (J.YF.11.(2).297.7002) V.A.PCHELIN,L.V.CHESTIAKOV,V.I.MYCHOMOTSEVA,	REFERENCE TITLE	40193 (J.YF.10.(1).64.8031) A.B.KOLODINSKI,JU.F.KOLODNOV,V.M.KOLODASHKIN,
ENTRY AUTHOR	40232 (L.N.JUROVA,A.V.BUSHUEV,V.O.OZERKIN,V.I.KOZIN)	ENTRY AUTHOR	40181 (J.YF.11.(2).297.7002) V.A.PCHELIN,L.V.CHESTIAKOV,V.I.MYCHOMOTSEVA,	REFERENCE TITLE	40194 (J.YF.10.(1).64.8031) A.B.KOLODINSKI,JU.F.KOLODNOV,V.M.KOLODASHKIN,
REFERENCE TITLE	STUDY OF SPONTANEOUS FISSION OF CP-252	REFERENCE TITLE	40182 (J.YF.11.(2).297.7002) V.A.PCHELIN,L.V.CHESTIAKOV,V.I.MYCHOMOTSEVA,	REFERENCE TITLE	40195 (J.YF.10.(1).64.8031) A.B.KOLODINSKI,JU.F.KOLODNOV,V.M.KOLODASHKIN,
ENTRY AUTHOR	40234 (L.N.JUROVA,A.V.BUSHUEV,V.O.OZERKIN,V.I.KOZIN)	ENTRY AUTHOR	40182 (J.YF.11.(2).297.7002) V.A.PCHELIN,L.V.CHESTIAKOV,V.I.MYCHOMOTSEVA,	REFERENCE TITLE	40196 (J.YF.10.(1).64.8031) A.B.KOLODINSKI,JU.F.KOLODNOV,V.M.KOLODASHKIN,
REFERENCE TITLE	ANGULAR ANISOTROPY AND ASYMMETRY OF FRAGMENT MASSES BY FISSION OF U-235 AND U-238	REFERENCE TITLE	40183 (J.YF.11.(2).297.7002) V.A.PCHELIN,L.V.CHESTIAKOV,V.I.MYCHOMOTSEVA,	REFERENCE TITLE	40197 (J.YF.10.(1).64.8031) A.B.KOLODINSKI,JU.F.KOLODNOV,V.M.KOLODASHKIN,
ENTRY AUTHOR	40240 (V.G.VOROB'YEV,A.I.GENTOSH,B.D.KUZ'MINOV, A.I.SERGACHEV,V.M.SURIN)	ENTRY AUTHOR	40183 (J.YF.11.(2).297.7002) V.A.PCHELIN,L.V.CHESTIAKOV,V.I.MYCHOMOTSEVA,	REFERENCE TITLE	40198 (J.YF.10.(1).64.8031) A.B.KOLODINSKI,JU.F.KOLODNOV,V.M.KOLODASHKIN,
REFERENCE TITLE	ANGULAR ANISOTROPY AND ASYMMETRY OF FRAGMENT MASSES BY FISSION OF U-235 AND U-238	REFERENCE TITLE	40184 (J.YF.11.(2).297.7002) V.A.PCHELIN,L.V.CHESTIAKOV,V.I.MYCHOMOTSEVA,	REFERENCE TITLE	40199 (J.YF.10.(1).64.8031) A.B.KOLODINSKI,JU.F.KOLODNOV,V.M.KOLODASHKIN,
ENTRY AUTHOR	40243 (A.M.KONDOV,P.V.KOROV'YEV,V.A.KOROSTYLEV, A.M.NIKITIN,V.M.SEREBRENNY)	ENTRY AUTHOR	40184 (J.YF.11.(2).297.7002) V.A.PCHELIN,L.V.CHESTIAKOV,V.I.MYCHOMOTSEVA,	REFERENCE TITLE	40200 (J.YF.10.(1).64.8031) A.B.KOLODINSKI,JU.F.KOLODNOV,V.M.KOLODASHKIN,
REFERENCE TITLE	THEORETICAL CALCULATION OF THE DISTRIBUTION OF THE PU-241 NUCLEI INDUCED BY FAST NEUTRONS	REFERENCE TITLE	40185 (J.YF.11.(2).297.7002) V.A.PCHELIN,L.V.CHESTIAKOV,V.I.MYCHOMOTSEVA,	REFERENCE TITLE	40201 (J.YF.10.(1).64.8031) A.B.KOLODINSKI,JU.F.KOLODNOV,V.M.KOLODASHKIN,
ENTRY AUTHOR	40284 (V.G.VOROB'YEV,A.I.GENTOSH,B.D.KUZ'MINOV, A.I.SERGACHEV,V.M.SURIN)	ENTRY AUTHOR	40185 (J.YF.11.(2).297.7002) V.A.PCHELIN,L.V.CHESTIAKOV,V.I.MYCHOMOTSEVA,	REFERENCE TITLE	40202 (J.YF.10.(1).64.8031) A.B.KOLODINSKI,JU.F.KOLODNOV,V.M.KOLODASHKIN,
REFERENCE TITLE	THEORETICAL CALCULATION OF THE DISTRIBUTION OF THE PU-241 NUCLEI INDUCED BY FAST NEUTRONS	REFERENCE TITLE	40186 (J.YF.11.(2).297.7002) V.A.PCHELIN,L.V.CHESTIAKOV,V.I.MYCHOMOTSEVA,	REFERENCE TITLE	40203 (J.YF.10.(1).64.8031) A.B.KOLODINSKI,JU.F.KOLODNOV,V.M.KOLODASHKIN,

WARNINGS ON DATA 9000+

Reference numbers of 9000+ and above give warning that the data is highly discrepant, predicted or converted into a usable form by possibly inaccurate methods. Descriptions follow:

90000. Model estimates for the THERMAL 242M high mass peak were unrealistic. When model calculations renormalised by sparse experimental data, the model estimates were found to be before extrapolated from log(CHAIN YIELD) vs Af-mul-bar graphs,10% standard deviation assumed, for 140Ba to produce more realistic result in the absence of complete experimental data.

[Database record: B 0.000E+00 95242140 56 U 0.590E+01 3.000E+0190000Y]

91199. FAST H-1,H-3 and He-4 estimated from reference 1199 monenergetic data, assumed fast == 400kev.

91204. FAST H-3 yields for Th-232 and U-233. Measurements about 5-10 times expected, see 91205, and large uncertainties. Measurements of other data are included in the model. Other data requires more experimental measurements to resolve uncertainty. From reference 1204.

91205. FAST H-3 yields for U-238,U-235 and Th-232, Th-232 and U-238 are about 10 times larger than expected, paper suggests tritium measurements are needed. Measurements of other data are included in UNFV2 libraries. U235 uncertainty increased to 10%. From reference 1205.

92043. U-238 DATA is not in form convertible to absolute yield. Therefore, shows energy dependence only. For Pu-239 and U-235, the model estimates for yields are 10% higher than experimental, thus assigned errors of 15% from reference 2043.